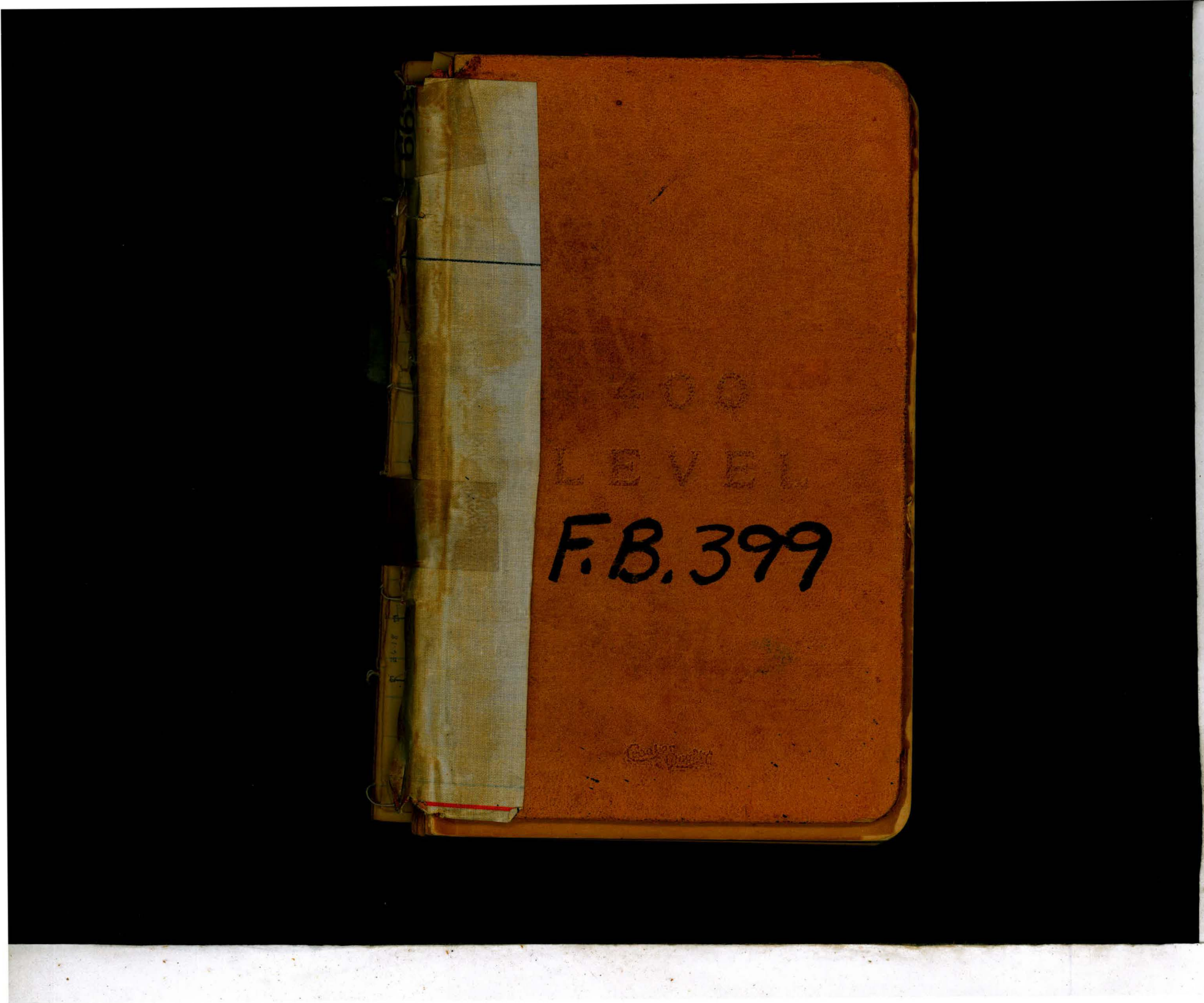

400
LEVEL
F.B.399

Published by H. S. CROCKER COMPANY, Stationers, Drawing Materials, and Mathematical Instruments, San Francisco.

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1	2⅓	21	49	41	95⅔
2	4⅔	22	51⅓	42	98
3	7	23	53⅔	43	100⅓
4	9⅓	24	56	44	102⅔
5	11⅔	25	58⅓	45	105
6	14	26	60⅔	46	107⅓
7	16⅓	27	63	47	109⅔
8	18⅔	28	65⅓	48	112
9	21	29	67⅔	49	114⅓
10	23⅓	30	70	50	116⅔
11	25⅔	31	72⅓	51	119
12	28	32	74⅔	52	121⅓
13	30⅓	33	77	53	123⅔
14	32⅔	34	79⅓	54	126
15	35	35	81⅔	55	128⅓
16	37⅓	36	84	56	130⅓
17	39⅔	37	86⅓	57	133
18	42	38	88⅔	58	135⅓
19	44⅓	39	91	59	137⅔
20	46⅔	40	93⅓	60	140

MICROFILMED OCT 1 0 1964

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

Crocker Quality

LEVEL BOOK

No. 400

Return to City Engineer's Office
City Hall, San Diego, Cal.

COMMUNI CONSENSU MADE PRIMO MADE

MANUFACTURED BY
A. S. Crocker Co.
SAN FRANCISCO
and
SACRAMENTO

X-section Fort Stockton Boulevard from center line of Chestnut st to Jackson & Chestnut.
sections taken for 30' on each side of center line R= right & L= left from ℄ as survey runs from Chestnut
sections taken at right angles from ℄

3 Dunkle
1/16 Shaw
40 ½ [illegible]

B.M. Brass cap Mon Conde & Whitman 215.07

B.M.	12.17	227.24		
T.P.	12.69	238.45	1.48	225.76

0+0 = center Mon Chestnut & Arist3 ½

0+0 Center Chestnut. 50' wide

R.

		6.4	232.0
+5=N.L. Arista 50' wide		5.7	232.7
crb		3.7	234.7 ✓
$^{1}/_{4}$		3.2	235.2
M	238.45	2.4	236.0
$^{1}/_{4}$		1.3	237.1
crb		1.1	237.3
S.L. Arista		0.2	238.2
+5=L		+0.4	238.8

N $^{1}/_{4}$

L

+5=S.L.	0.5	237.9
	0.9	237.5
Crb	1.4	237.0
$^{1}/_{4}$	1.7	236.7
M	2.9	235.5
$^{1}/_{4}$	4.6	233.8
crb	4.9	233.5
N.L.	6.0	232.4
+5=R.	6.8	231.6

	W. Curb		
R	238.45	7.4	231.0
+5 = W.L.		6.7	231.7
Crb		5.4	233.0
1/4		4.6	233.8
M		3.1	235.3
1/4		1.9	236.5
Crb		1.6	236.8
S.L.		0.9	237.5
+5 = L.		0.6	237.8
	0+25 = W.L. Chestnut		
L		1.3	237.1
+5 = S.L.		1.7	236.7
Crb		2.3	236.1
1/4		2.5	235.9
M		3.8	234.6
1/4		5.3	233.1
Crb		6.1	232.3
W.L.		7.5	230.9
+5 = R		8.3	230.1

	0+50		
R	238.45	9.0	229.4
+5 = W.L.		8.5	229.9
Crb		7.1	231.3
1/4		6.5	231.9
M		5.2	233.2
1/4		3.8	234.6
Crb		3.4	235.0
S.L.		2.8	235.6
+5 = L.		2.5	235.9
	0+75		
L		3.8	234.6
+5 = S.L.		4.2	234.2
Crb		5.0	233.4
1/4		5.2	233.2
M		6.7	231.7
1/4		8.1	230.3
Crb		8.6	229.8
W.L.		9.6	228.8
+5 = R		10.2	228.2

1+00

R.	238.45	11.7	226.7
+5 = N.L.		11.1	227.3
Crk		10.1	228.3
1/4		9.7	228.7
M		8.8	229.6
1/4		7.6	230.8
Crk		7.2	231.2
S.L.		6.2	232.2
+5 = L.		5.4	233.0

1+25

L		6.6	231.8
+5 = S.L.		7.3	231.1
Crk		8.8	229.6
1/4		9.1	229.3
M		10.2	228.2
1/4		11.3	227.1
Crk		11.9	226.5
N.L.		13.5	224.9
+5 = R		14.4	224.0

1+50

R	238.45	15.6	226.8
+5 = N.L.		15.0	223.4
Crk		13.5	224.9
1/4		12.8	225.6
M		11.5	226.9
1/4		10.1	228.3
Crk		9.8	228.6
S.L.		8.8	229.6
+5 = L		8.0	230.4

1+75

L.		10.2	228.2
+5 = S.L.		10.7	227.7
Crk		11.8	226.6
1/4		12.2	226.2
M		13.5	224.9
1/4		13.8	224.6
Crk		12.3	226.1
N.L.		15.5	222.9
+5 = R		16.2	222.2

238.45

2+0

R	238.45	17.4	221.0	
+5 = N.L.		16.3	222.1	
crk		15.2	223.2	
"		15.0	223.4	
M		14.5	223.9	
"		13.4	225.0	
crk		12.9	225.6	
S.L.		12.0	226.4	
+5 = L		11.6	226.8	
T.P.	0.54	226.58	12.41	226.04

2+25 = P.C. Blvd leaves drive 25'

	226.58	0.1	226.5	
+5 = S.L.		0.4	226.2	
crk		2.0	224.6	
"		2.4	224.2	
M		3.4	223.2	
"		3.6	223.0	
crk		3.8	222.8	
N.L.		5.0	221.6	
+5 = R		5.7	220.9	

2+50

R	226.6	6.5	220.1	
+10		5.5	221.1	
+16		4.3	222.3	
+20		4.1	222.5	
℄		3.7	222.9	
+10		2.7	223.9	224.0
+20		2.5	224.1	
+30 = L		2.0	224.6	

2+75

L	226.6	3.5	223.1	
+10		3.7	222.9	222.8
+20		3.8	222.8	
℄		4.2	222.4	
+8		4.5	222.1	
+10		4.9	221.7	221.1
+20		6.1	220.5	
R		7.2	219.4	

	3+00			
R	226.6	6.5	220.1	
+10		6.0	220.6	
+20		5.5	221.1	220.8
℄		4.9	221.7	
+10		4.4	222.2	
+20		4.3	222.3	222.3
L		4.2	222.4	
	3+25			
L		4.4	222.2	
+10		4.6	222.0	
+20		4.6	222.0	222.0
℄		5.0	221.6	
+10		5.4	221.2	
+20		5.7	220.9	221.0
R		6.3	220.3	

	3+50			
R	226.6	8.4	218.2	
+10		6.3	220.3	
+20		5.5	221.1	220.7
℄		5.0	221.6	
+10		5.0	221.6	
+20		4.8	221.8	221.7
L		4.7	221.9	
	3+75			
L		4.2	222.4	
+10		5.0	221.6	
+20		6.0	220.6	221.1
℄		7.1	219.5	
+10		8.2	218.4	
+20		9.3	217.3	217.8
R		11.3	215.3	

		226.58			
		4+0			
R		226.6	14.9	211.7	
+10			13.5	213.1	
					213.9
+20			11.8	214.8	
℄			10.4	216.2	
+10			9.0	217.6	
					218.1
+20			8.0	218.6	
+22			7.5	219.1	
+23			6.6	220.0	
L			6.1	220.5	
T.P.	0.94	217.01	10.51	216.07	
	4+21 35 = P.T.				
L			1.4	215.6	
+10			2.9	214.6	213.9
+20			3.9	213.1	
℄			4.8	212.2	
+10			5.9	211.1	
					210.9
+20			6.2	210.8	
R			6.2	210.8	

4+33 64 = P.C.				
R	217.0	7.3	209.7	
+10		7.4	209.6	
				209.5
+20		7.6	209.4	
℄		6.8	210.2	
+10		6.7	210.3	
				210.6
+20		6.0	211.0	
L		5.4	211.6	
4+75				
L		11.7	205.3	
+10		12.1	204.9	
				204.9
+20		12.1	204.9	
℄		12.3	204.7	
+10		11.3	205.7	
				205.6
+20		11.4	205.6	
R		11.5	205.5	

		217.01			
		4+90			
R.		217.0	12.0	205.0	
+10			12.9	204.1	
+20			13.2	203.8	203.9
℄			14.2	202.8	
+10			13.9	203.1	
+20			13.8	203.2	203.1
L			13.7	203.3	
T.P.	1.39	206.36	12.54	209.47	
		5+0			
L			4.5	201.9	
+10			4.7	202.0	
+15			4.5	201.9	201.9
+20			7.1	199.3	
℄			7.8	198.6	
+10			9.9	196.8	
+20			9.3	197.1	196.8
R			8.8	197.6	

	5+10			
R.	206.4	1.9	204.5	
+10		7.3	199.1	
+20		10.4	196.0	197.5
℄		13.0	193.4	
+10		10.5	195.9	
+20		7.9	198.5 (26)	187.2
L		5.5	200.9	
	5+25			
L		13.0	193.4	
+5		16.3	190.1	
+10		13.6	192.8	
+20		10.8	195.6 (28)	194.2
℄		5.4	201.0	
+10		3.6	202.8	
+20		2.2	204.2 (31)	203.5
R		1.5	204.9	

5+50

R	206.4	2.3	204.1	
+10		3.4	203.0	
+20		4.2	202.2	202.6
℄		5.1	201.3	
+10		6.2	200.2	
+20		15.1	191.3	195.7
+25		18.5	187.9	
L		18.5	187.9	

5+75

L		13.3	193.1	
+8		7.4	199.0	
+10		7.2	199.2	
+20		6.4	200.0	199.6
℄		5.6	200.8	
+10		4.7	201.7	
+20		4.1	202.3	202.0
R		3.2	203.2	

6+05.99 = P.T.

R	206.4	3.5	202.9	
+10		4.4	202.0	
+20		5.0	201.4	201.7
℄		5.8	200.6	
+10		7.1	199.3	
+20		7.9	198.5	198.9
L		9.0	197.4	

6+25

L		10.3	196.1	
+3		9.1	197.3	
+10		8.1	198.3	
+20		7.2	199.2	198.7
℄		6.1	200.3	
+10		5.1	201.3	
+20		4.0	202.4	201.8
R		2.6	203.8	

	6+50			
R	206.4	1.2	205.2	
+10		2.3	204.1	
+20		3.4	203.0	203.5
℄		4.7	201.7	
+10		6.3	200.1	
+20		7.7	198.7	199.4
+25		8.4	198.0	
L		11.1	195.3	
	6+75			
L		13.4	193.0	
+10		7.9	198.5	
+20		5.5	200.9	199.7
℄		4.1	202.3	
+10		2.7	203.7	
+20		1.3	205.1	204.4
R		0.3	205.1	

	7+0			
R	206.4	0.9	205.5	
+10		2.2	204.2	
+20		3.7	202.7	203.4
℄		5.0	201.4	
+10		6.4	200.0	
+20		8.4	198.0	199.0
+25		9.8	196.6	
L		12.2	194.2	
	7+35 28 = P.C.			
L		14.2	192.2	
+10		12.3	194.1	
+20		10.9	195.5	194.8
℄		9.3	197.1	
+12		7.6	198.8	
+20		5.4	201.0	199.9
R		4.1	202.3	

		206.36			
		7+75			
R		206.4	6.7	199.7	
+10			7.3	199.1	197.9
+20			9.6	196.8	
℄			11.7	194.7	
+10			14.8	191.6	
+20			17.1	189.3	190.4
L			19.9	186.5	
T.P	6.52	200.33	12.55	193.81	
		8+0			
L		200.3	15.7	184.6	
+10			12.5	187.8	
+20			9.7	190.6	189.2
℄			6.7	193.6	
+10			9.3	196.0	
+20			2.7	197.6	196.8
R			1.7	198.6	

	8+25			
R	200.3	4.5	195.8	
+10		4.6	195.7	195.5
+20		5.0	195.3	
℄		6.7	193.6	
+10		10.2	190.1	
+20		13.3	187.0	188.5
L		15.4	184.9	
	8+50			
L		18.7	181.6	
+10		15.5	184.8	
+20		12.4	187.9	186.3
℄		10.6	189.7	
+10		8.9	191.4	
+20		7.5	192.8	192.1
R		6.5	193.8	

200.33

8+88.88 = R.T.

R		200.3	9.6	190.7	
+10			10.6	189.7	
+20			12.1	188.2	188.9
℄			14.0	186.3	
+10			17.4	182.9	
+20			20.9	179.4	184.6
L.			25.5	174.8	
		9+25			
L			29.3	171.0	
+10			24.8	175.5	
+20			20.2	179.6	177.6
℄			17.2	183.1	
+10			14.1	186.2	
+20			12.4	187.9	187.0
R.			12.0	188.3	
T.P.	0.97	188.78	12.52	187.81	

188.78

9+46.88 = P.C.

P	188.8	2.2	186.6		
+10		3.0	185.8		
				184.4	
+20		4.8	184.0		
℄		7.3	181.5		
+10		10.8	178.0		
+20		14.6	174.2	176.1	
			19		
L,		18.5	170.3		
	9+75				
L		16.6	172.2		
+10		12.9	175.9		
			13		
+20		10.3	178.5	177.4	
			16		
℄		7.6	181.2		
+10		5.6	183.2		
				183.7	
+20		4.7	184.1		
R,		4.0	184.8		

10+00

R,	188.8	4.6	184.2		
+10		6.0	182.8		
				182.0	
+20		7.6	181.2		
℄		10.3	178.5		
+10		13.3	175.5		
				173.6	
+20		17.0	171.8		
			3.8		
L		20.7	168.1		
	10+25				
L		25.3	163.5		
+10		21.1	167.7		
				170.1	
+20		16.2	172.6		
			2.9		
℄		12.1	176.7		
+10		8.9	179.9		
				181.0	
+20		6.6	182.2		
P		5.2	183.6		

188.78

10+45.27 = P.T.

R.	188.8	6.1	182.7	
+10		7.1	181.7	
+20		8.7	180.1	180.9
℄		11.8	177.0	
+10		15.1	173.7	
+20		19.0	169.8	171.8
L.		23.5	165.3	

10+56.72 = P.C.

L		21.7	167.1	
+10		18.0	170.8	
+20		14.2	174.6	176.7
℄		10.8	178.0	
+10		8.9	179.9	
+20		8.1	180.7	180.3
R.		7.3	181.5	

Quinec — 23.98 — 54

10+75

R	188.8	7.7	181.1	
+10		8.2	180.6	
+20		8.9	179.9	180.2
℄		10.1	178.7	
+10		11.9	176.9	
+20		12.2	176.6	176.7
L.		18.8	170.0	

11+0

L		15.5	173.3	
+10		13.7	175.1	
+20		12.6	176.2	175.6
℄		11.4	177.4	
+10		10.3	178.5	
+20		10.0	178.8	178.6
R		10.0	178.8	
T.P.	0.38	177.43	11.63	177.15

11+25

R	177.4	0.4	177.0	
+10		0.5	176.9	
+20		1.7	175.7	176.3
℄		3.0	174.4	
+10		3.9	173.5	
+20		5.1	172.3	172.9
L		6.0	171.4	

11+55? = P.T.

L		10.5	166.9	
+10		9.0	168.4	
+20		7.5	169.9	169.2
℄		5.9	171.5	
+10		4.0	173.4	
+20		3.2	174.2	173.8
R		2.4	175.0	

11+98? = P.C.

R	177.4	4.2	173.2	
+10		6.0	171.4	
+20		7.3	170.1	170.7
℄		8.8	168.6	
+10		10.7	166.7	
+20		12.7	164.7	165.7
L		14.0	163.4	

12+25

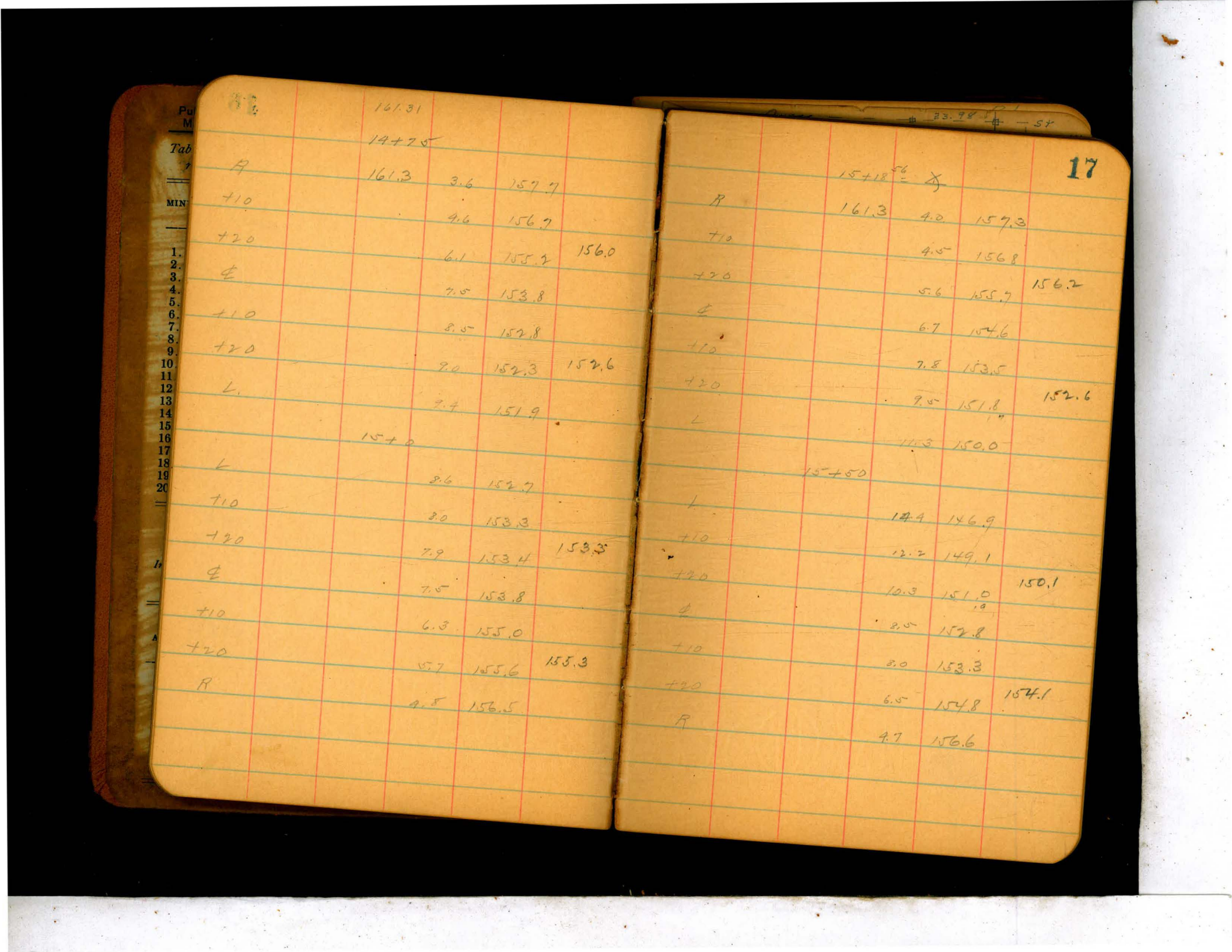
L		15.1	162.3	
+10		13.7	163.7	
+20		11.8	165.6	164.6
℄		10.8	166.6	
+10		9.5	167.9	
+20		7.8	169.6	168.7
R		6.2	171.2	

	177.43				
	12+50				
R	177.4	8.8	168.8		
+10		9.5	167.9		
+20		11.0	166.4	167.7	
℄		12.4	165.0		
+10		13.9	163.5		
+20		14.5	162.9	163.7	
L		16.2	161.2		
	12+75				
L		18.5	158.9		
+10		16.6	160.8		
+20		14.8	162.6	161.7	
℄		13.5	163.9		
+10		12.2	165.2		
+20		10.8	166.6	165.9	
R		9.6	167.8		
T.P	2.23	170.61	9.05	168.38	

	13+0				
R	170.6	2.6	168.0		
+10		3.1	167.5		
+20		5.1	165.5	166.5	
℄		6.3	164.3		
+10		7.8	162.8		
+20		9.5	161.1	162.0	
L		11.3	159.3		
	13+25				
L		10.9	159.5		
+10		9.3	161.3		
+20		7.7	162.9	162.1	
℄		6.0	164.6		
+10		4.1	166.5		
+20		2.1	168.5	167.5	
R		1.3	169.3		

	170.61				
	13+50				
R	170.6	1.0	169.6		
+10		2.6	168.0		
+20				167.7	
+26		3.2	167.4		
℄		2.7	167.9		
+5		5.5	165.1		
+10		8.7	161.7		
		7.8	162.8		
+20		9.4	161.2	162.0	
L		11.5	159.1		
	13+86.66 = P.T.				
L		13.5	157.1		
+10		11.1	159.5		
+20		9.9	161.2	160.3	
℄		8.4	162.2		
+10		6.8	163.8		
+20		5.8	164.8	164.3	
+24		4.0	166.6		
R		3.7	166.9		

	14+25				
R	170.6	8.4	162.2		
+6		8.6	162.0		
+10		9.9	160.7		
+20		10.5	160.1	160.4	
℄		12.3	158.3		
+10		13.7	156.9		
+20		14.7	155.9	156.4	
L		16.8	153.8		
	14+50				
L		17.6	153.0		
+10		16.3	154.3		
+20		15.7	154.9	154.6	
℄		14.7	155.9		
+10		13.8	156.8		
+20		12.4	158.2	157.5	
R		11.4	159.2		
T.P.	2.69	161.31	11.99	158.62	



161.31

14+75

R			
161.3	3.6	157.7	
+10	4.6	156.7	
+20	6.1	155.2	156.0
℄	7.5	153.8	
+10	8.5	152.8	
+20	9.0	152.3	152.6
L	9.7	151.9	
15+00			
L	8.6	152.7	
+10	8.0	153.3	
+20	7.9	153.4	153.3
℄	7.5	153.8	
+10	6.3	155.0	
+20	5.7	155.6	155.3
R	4.5	156.5	

17

15+18 56 = 4

R			
161.3	4.0	157.3	
+10	4.5	156.8	
+20	5.6	155.7	156.2
℄	6.7	154.6	
+10	7.8	153.5	
+20	9.5	151.8	152.6
L	11.3	150.0	
15+50			
L	14.4	146.9	
+10	12.2	149.1	
+20	10.3	151.0	150.1
℄	8.5	152.8	
+10	8.0	153.3	
+20	6.5	154.8	154.1
R	4.7	156.6	

15+75

R	161.3	6.4	154.9	
+10		7.6	153.7	
+20		8.5	152.8	153.3
℄		9.7	151.6	
+10		11.8	149.5	
+20		13.3	148.0	148.7
L		13.9	147.4	

16+0

L	161.3	16.5	144.8	
+6		17.5	143.8	
+10		15.9	145.4	
+20		15.6	145.7	145.6
℄		11.0	150.3	
+10		9.7	151.6	
+20		8.7	152.6	152.1
R		7.8	153.5	

16+75

R	161.3	6.8	154.5	
+10		7.8	153.5	
+20		9.2	152.1	152.8
℄		10.5	150.8	
+10		12.9	148.4	
+15		13.9	147.4	147.4
+20		17.8	143.5	
+22		18.4	142.9	
+25		16.1	145.2	
L		17.1	144.2	

16+50

L		21.0	140.3	
+10		17.3	144.0	
+20		13.8	147.5	145.2
℄		11.1	150.2	
+10		10.1	151.2	
+20		8.2	153.1	152.1
R		6.0	155.3	

Quintec — — 23.98 — 54

	161.31			
	16+75			
R	161.3	6.3	155.0	
+10		8.6	152.7	151.6
+20		10.9	150.4	
℄		13.3	148.0	
+10		15.4	145.9	
+20		18.5	142.8	144.4
L		22.5	138.8	
	17+0			
L		26.1	135.2	
+10		22.8	138.5	
+20		19.4	141.9	140.2
℄		15.8	145.5	
+10		11.5	149.8	
+20		9.0	152.3	151.1
R		6.5	154.8	

	17+25			
R	161.3	8.2	153.1	
+10		11.2	150.1	148.6
+20		14.2	147.1	
℄		18.8	142.5	
+10		21.3	140.0	
+20		23.6	137.7	138.8
L		27.9	133.4	
	17+68 56 = .7			
L		29.2	131.6	
+10		26.3	135.0	
+20		23.4	137.9	136.5
℄		19.7	141.6	
+10		16.4	144.9	
+20		14.2	147.1	146.0
R		10.8	150.5	
T.R	4.64	153.19	12.76	148.55

	153.19			
	18+00			
R	153.2	2.5	150.7	
+10		4.9	148.3	
+20		8.3	144.9	146.6
℄		11.5	141.7	
+10		15.5	137.7	
+20		19.3	133.9	135.8
			89	
L		22.9	130.3	
	18+25			
L		24.8	128.4	
+10		24.1	132.1	
			23	
+20		16.4	136.8	134.4
℄		12.7	140.5	
+10		9.1	144.1	
+20		4.5	149.2	146.7
R		1.0	153.2	

	18+50			
R	153.2	1.1	152.1	
+10		5.0	148.2	
+20		9.0	144.2	146.2
℄		13.4	139.8	
+10		18.0	135.2	
+20		22.0	131.2	133.2
L		26.9	126.3	
	18+75			
L	153.2	29.9	123.3	
+10		24.7	128.5	
+20		19.6	133.6	131.0
			49	
℄		14.6	138.6	
+10		10.5	142.7	
+20		6.1	147.1	145.5
R		2.1	151.1	

153.19

19+18 56 = P.C.

R		153.2	4.8	148.4	
+7			8.5	144.7	
+10			11.0	142.2	
+20			13.3	139.9	141.0
℄			18.8	134.4	
+10			23.7	129.5	
+20			28.0	125.2	127.3
L			32.5	120.7	
		19+50			
L			33.4	119.8	
+10			28.2	125.0	
+20			23.8	129.4	127.2
℄			18.5	134.7	
+10			14.1	139.1	
+20			10.3	142.9	141.0
R			7.1	146.1	
T.P.	5.33	147.36	11.4	142.03	

19+75 59 = P.C.

R	147.4	2.9	144.5	
+10		6.1	141.3	138.7
+20		11.2	136.2	
℄		16.0	131.4	
+10		20.9	126.5	
+20		25.4	122.0	124.2
L		31.0	116.4	
	20+00			
L		30.7	116.7	
+10		25.4	122.0	
+20		20.9	126.5	124.2
℄		16.4	131.0	
+10		11.1	136.3	
+20		7.4	140.0	138.1
R		2.6	144.8	

	147.36				
	20+25				
R	147.4	2.8	144.6		
+10		7.2	140.2		
+20		11.5	135.9	138.0	
			4B		
℄		15.7	131.7		
+10		20.3	127.1		
+20		24.9	122.5	124.8	
			2.3		
L		29.6	117.8		
	20+50				
L		28.0	119.4		
+10		23.2	124.2		
+20		19.1	128.3	126.3	
℄		15.2	132.2		
+10		11.4	136.0		
+20		7.3	140.1	138.0	
R		3.5	143.9		

	20+75				
R	147.4	4.1	143.3		
+10		6.7	140.7		
+20		10.5	136.9	138.8	
℄		14.5	132.9		
+10		18.5	128.9		
+20		22.6	124.8	126.8	
			4.1		
L		26.7	120.7		
	21+00				
L		25.3	122.1		
+10		21.5	125.9		
			1.8		
+20		17.8	129.6	127.7	
			3.7		
℄		13.9	133.5		
+10		9.9	137.5		
+20		7.7	139.7	138.6	
R		4.2	143.2		

		147.36			
		21+25			
R		147.4	5.7	141.7	
+10			7.6	139.8	
+20			10.6	136.8	138.3
℄			14.5	132.9	
+10			17.9	129.5	
+20			21.6	125.8	127.6
				P8	
L			24.5	122.9	
		21+50			
L			23.8	123.6	
+10			20.9	126.5	
				15	
+20			17.8	129.6	128.0
℄			14.4	133.0	
+10			11.8	135.6	
+20			9.9	137.5	136.6
R			8.6	138.8	
T.P.	1.50	138.91	9.95	137.41	

		21+75			
R		138.91	1.6	137.3	
+10			3.9	135.0	
+20			6.3	132.6	133.8
℄			8.8	130.1	
+10			11.5	127.4	
+20			14.9	124.0	125.7
				17	
L			17.8	121.1	
		22+00			
L			20.5	118.4	
+10			17.7	121.2	
				17	
+20			14.4	124.5	122.9
℄			12.1	126.8	
+10			9.4	129.5	
+20			7.4	131.5	130.5
R			5.5	133.4	

		138.91			
		22+38 65 =	P.T.		
R		138.9	9.2	129.7	
+10			11.8	127.1	
+20			13.9	125.0	126.0
℄			16.4	122.5	
+10			19.5	119.4	
+20			21.3	117.6 (9)	118.7
L.			23.9	115.0	
		22+75			
L			27.8	111.1	
+10			26.0	112.9 (14)	
+20			22.6	116.3	114.6
℄			19.0	119.9	
+10			17.1	121.8	
+20			15.0	123.9	122.9
R.			12.8	126.1	
T.P.	1.26	127.76	12.41	126.50	[illegible]

3/25/10 Quirk Evans

		23+00			
R		127.8	3.9	123.9	
+10			6.6	121.2	
+20			8.8	119.0	120.1
℄			11.3	116.5	
+10			14.6	113.2	
+20			17.6	110.2	111.7
L.			20.0	107.8	
		23+25			
L.			22.7	105.1	
+10			19.2	108.6 (12)	
+20			16.8	111.0	109.8
℄			14.4	113.4	
+10			11.8	116.0	
+20			8.5	119.3	117.7
R			5.9	121.9	

		127.76			
		23+50			
R		127.8	7.6	120.2	
+10			10.3	117.5	
+20			12.8	115.0	116.3
℄			15.5	112.3	
+10			19.2	108.6	
+20			22.1	105.7 (1.5)	107.2
L.			25.1	102.7	
		23+75			
L			27.9	99.9	
+10			25.0	102.8	
+20			22.0	105.8	104.3
℄			18.4	109.4	
+10			14.9	112.9	
+20			12.4	115.4	114.2
R.			9.9	117.9	
T.P.	1.76	118.24	11.78	116.48	

		24+00			
R		118.2	2.2	116.0	116.3 (1.3)
+10			4.6	113.6	
+20			7.2	111.0	112.3
℄			10.4	107.8	
+10			13.7	104.5	
+20			16.5	101.7 (1.5)	103.1
L.			18.2	100.0	
		24+25			
L			20.3	97.9	
+10			17.2	101.0 (1.2)	
+20			14.8	103.4	102.2
℄			12.3	105.9	
+10			9.5	108.7	
+20			7.1	111.1	109.9
R			4.5	113.7	

		118.29			
		29+50			
R		118.2	7.2	111.0	
+10			9.5	108.7	
+20			12.0	106.2	107.5
T.P.	5.04	112.27	11.01	107.23	
℄			8.3	104.0	
+10			10.6	101.7	
+20			13.2	99.1	100.4
L			14.9	97.4	
		29+75			
L			17.5	94.8	
+10			15.0	97.3	
+20			13.9	98.9	98.1
℄			11.9	100.9	
+10			8.8	103.5	
+20			7.3	105.0	104.2
R			5.5	106.8	

	112.27			
	29+87			
R	112.3	9.3	103.0	
+10		12.1	100.2	
+20		13.6	98.7	99.4
℄		15.2	97.1	
+10		16.7	95.6	
+20		19.2	93.1	95.3
L		21.6	90.7	
	25+00			
L		18.4	93.9	
+10		18.4	93.9	
+20		15.0	97.3	95.6
℄		13.0	99.3	
+10		12.2	100.1	
+20		8.3	104.0	102.0
R		5.8	106.5	

112.27

25+25

R	112.3	3.3	109.0
+10		5.0	107.3
+20		6.2	106.1
			106.7
℄		8.6	103.7
+10		10.9	101.4
+20		12.7	99.6
			100.5
L		15.0	97.3

25+50

L		12.7	99.6
+10		11.3	101.0
+20		8.6	103.7
			102.3
℄		6.8	105.5
+10		5.1	107.2
+20		3.4	109.9
			108.5
R		1.0	111.3

25+75

26

R	112.27	+0.8	113.1
+10		1.9	110.4
+20		3.9	108.4
			109.4
℄		6.1	106.2
+10		8.4	103.9
+20		9.9	102.4
			103.1
L		12.3	100.0

26+0

L		11.6	100.7
+10		10.7	101.6
+20		8.0	104.3
			102.9
℄		6.7	105.6
+10		3.3	108.5
+20		1.3	111.0
			109.7
R		+0.3	112.6

23.98 — 57

T 5.40

		112.27			
		26+25			
R		112.3	+0.6	112.9	
+10			2.3	110.0	
+20			4.3	108.0	109.0
℄			7.1	105.2	
+10			9.6	102.7	
+20			11.0	101.3	102.0
L			13.5	98.8	
T.P.	12.83	112.80	12.20	100.07	
		26+50			
L			15.9	97.0	
+10			14.8	98.1	
+20			12.6	100.3	99.2
℄			10.1	102.8	
+10			7.2	105.7	
+20			4.4	108.5	107.1
R			2.0	110.9	

	112.90			
	26+75			
R	112.9	3.5	109.4	
+10		6.0	106.9	
+20		9.2	103.7	105.3
℄		12.1	100.8	
+10		14.5	98.4	
+20		16.7	96.2	98.3
L		17.6	95.3	
	27+00			
L		19.3	93.6	
+10		17.6	95.3	
+20		16.7	96.8	96.0
℄		14.1	99.8	
+10		11.3	101.6	
+20		8.4	104.5	103.1
R		5.8	107.1	

		112.90				
		27+25				
R		112.9	7.9	105.0		
+10			10.7	102.2		
+20			12.8	100.1	101.1	
℄			15.1	97.8		
+10			17.1	95.8		
+20			18.4	94.5	95.1	
L			19.4	93.5		
		27+50				
L			19.5	93.4		
+10			18.5	94.1		
+20			18.0	94.9	94.5	
℄			16.9	96.0		
+10			14.9	98.0		
+20			12.5	100.4	99.2	
R			9.9	103.0		
T.P.	0.67	102.19	11.38	101.52		

ST 27+92.83 = PC					28
R	102.2	3.1	99.1		
+10		4.7	97.5		
+20		5.8	96.4	96.9	
℄		7.0	95.2		
+10		7.8	94.4		
+20		8.8	93.4	93.9	
L		9.4	92.8		
	28+25				
L		9.9	92.3		
+10		9.4	92.8		
+20		8.8	93.4	93.1	
℄		8.2	94.0		
+10		7.5	94.7		
+20		6.6	95.6	95.2	
R		5.5	96.7		

Quimoc — — — 23.98 — — ST

ST 75.40

28+50

R	102.2	6.0	96.2	
+10		6.6	95.6	
+20		7.3	94.9	95.3
℄		8.2	94.0	
+10		8.7	93.5	
+20		9.1	93.1	93.3
L		9.8	92.4	

28+91.27 = P.T

L		10.6	91.6	
+10		9.8	92.4	
+20		8.9	93.3	92.9
℄		7.8	94.4	
+10		6.3	95.9	
+20		5.6	96.6	96.2
R		5.4	96.8	

29+25

R	102.2	3.6	98.6	
+10		4.0	98.2	
+20		5.4	96.8	97.5
℄		7.0	95.2	
+10		9.0	93.2	
+20		10.3	91.9	92.5
L		11.2	91.0	

29+91.27 = angle

L		12.1	90.1	
+10		11.2	91.0	
+20		10.2	92.0	91.5
℄		8.3	93.9	
+10		7.2	95.0	
+20		5.7	96.5	95.8
R		4.7	97.5	

	102.19				
	29+75				
R	102.2	9.3	92.9		
+10		11.1	91.1		
+20		12.5	89.7	90.4	
℄		13.9	88.3		
+10		15.1	87.1		
+20		15.5	86.7	86.9	
L		15.9	86.3		
T.P.	1.05	90.26	12.98	89.21	
	29+96 22 = P.C.				
L		3.0	87.3		
+10		5.0	85.3		
+20		5.1	85.2	85.2	
℄		4.4	85.9		
+10		3.5	86.8		
+20		2.6	87.7	87.2	
R		1.5	88.8		

	90.26				
	30+25				
R	90.3	7.2	83.1		
+10		7.3	83.0		
+20		7.2	83.1	83.0	
+25		6.2	84.1		
℄		4.6	85.7		
+5		3.3	87.0		
+10		5.3	85.0		
+16		7.4	82.9	82.9	
+20		7.7	82.6		
L		7.9	82.4		
	30+50				
L		9.2	81.1		
+10		8.5	81.8		
+20		8.2	82.1	81.9	
℄		6.2	84.1		
+5		6.3	84.0		
+10		8.8	81.5		
+20		12.3	78.0	79.7	
+25		14.2	76.1		
+26		17.6	72.7		
R		19.9	70.4		

30+75

R	90.3	21.9	68.4	
+10		16.6	73.7	
+20		9.4	80.9	77.3
℄		10.5	79.8	
+10		10.5	79.8	
+20		9.7	80.6	80.2
L		8.2	82.1	

30+93.22 = P.T.

L	9.0	81.3	
+10	8.1	82.2	
+20	9.7	80.6	81.4
℄	9.7	80.6	
+10	11.6	78.7	
+20	14.9	75.4	77.1
R	17.1	73.2	

31+18.22 = P.C

R	90.3	17.5	72.8
+10		15.5	74.8
+20		13.9	76.4	75.6
℄		10.0	80.3
+10		10.6	79.7
+20		11.0	79.3	79.5
L		11.9	78.4

31+50

L	12.1	78.2	
+10	10.9	79.4	
+20	9.7	80.6	80.0
+25 ℄	9.4	80.9	
	10.8	79.5	
+10	12.6	77.7	
+20	13.5	76.8	77.3
R	14.9	75.4	

	90.26			
	31+75			
R	90.3	21.5	68.8	
+10		17.6	72.7	
+15		14.6	75.7	75.7
+20		13.9	76.4	
℄		13.3	77.0	
+4		13.1	77.2	
+10		11.3	79.0	
				78.9
+20		11.6	78.7	
L		12.0	78.3	
T.P.	1.39	79.42	12.23	78.03
	32+16.15 = P.T.			
L	79.4	1.7	77.7	
+10		2.0	77.4	
+15		2.0	77.4	77.4
+20		4.9	74.5	
℄		5.7	73.7	
+10		6.3	73.1	
+16		7.6	71.8	71.8
+20		9.2	70.2	
R		12.8	66.6	

	32+50			
R	79.4	14.2	65.2	
+7		11.0	68.4	
+10		10.7	68.7	
				69.2
+20		9.8	69.6	
℄		7.4	72.0	
+3		6.5	72.9	
+10		7.0	72.4	
				72.7
+20		6.4	73.0	
L		7.5	71.9	
	32+63.20 = P.C.			
L		8.9	70.5	
+7		5.6	73.8	
+10		5.6	73.8	
+15		7.3	72.1	72.1
+20		7.3	72.1	
℄		8.2	71.2	
+5		10.1	69.3	
+10		10.7	68.7	
				68.3
+20		11.5	67.9	
R		14.2	65.2	

		79.42			
		33+00			
R		49.4	15.6	63.8	
+10			14.5	64.9	
+20			13.8	65.6	65.3
Q			12.4	67.0	
+10			5.5	70.9	
+20			9.5	69.9	70.4
L			10.1	69.3	
		33+25			
L			11.4	68.0	
+10			10.8	68.6	
+20			11.3	68.1	68.3
Q			10.1	69.3	
+10			15.2	64.2	
+20			17.3	62.1	63.1
R			21.0	58.4	
T.P.	1.27	69.07	11.62	67.80	

	69.07			
	33+50			
R	69.1	5.8	63.3	
+10		4.9	64.2	
+15		2.4	66.7	66.7
+20		4.2	64.9	
L		2.1	67.0	
+10		3.3	65.8	
+20		1.7	67.2	66.5
L		2.8	663	
	33+75			
L		5.4	63.7	
+10		5.1	640	
+20		4.4	64.7	64.3
R		5.4	63.7	
+10		5.7	63.4	
+20		4.3	64.8	64.1
+28=R	about end of 30'	5.3	63.8	

68.07

34+00

R	—		
+10 = edge of cliff	69.1	6.3	63.8
+20		6.1	63.0
℄		5.9	63.2
+10		6.0	63.1
+20		6.2	62.9
L		6.6	62.5

63.4

63.0

34+25

L		6.2	62.9
+5		4.2	64.9
+10		5.2	63.9
+20		1.5	67.6
℄		2.8	64.3
+10		3.1	66.0
+20		7.0	62.1
+25		7.4	61.7
R		9.2	59.9

65.7

64.1

34+50

R	69.1	13.2	55.9
+10		10.6	58.5
+20		9.0	60.1
℄		7.6	61.5
+10		5.4	63.7
+15		3.2	65.9
+20		4.9	64.2
L		5.2	63.9

59.3

65.9

34+75

L		7.2	61.9
+5		6.9	62.2
+10		4.9	64.2
+20		8.1	61.0
℄		9.3	59.8
+10		10.6	58.5
+20		14.2	54.9
P		15.1	54.0

62.6

56.7

ST

75.40

		69.07			
		35+0			
R		69.1	12.7	50.4	
+10			17.3	51.8	
+20			15.6	53.5	52.6
C			14.2	54.9	
+10			12.0	57.1	
+20			8.5	60.6	58.9
P L			8.3	60.8	
T.P.	0.49	61.56	8.00	61.07	
		35+25			
L		61.6	1.4	60.2	5
+10			4.2	60.4	
+20			5.6	55.0	57.7
C			8.7	51.9	
+10			10.6	51.0	
+20			10.7	50.9	50.9
R			11.0	50.6	

		35+50		
L	61.6	14.5	47.1	
+10		14.2	47.4	
+20		13.5	48.1	47.7
C		9.8	51.8	
+10		5.0	56.6	
+20		3.2	58.4	57.5
L		4.1	57.5	
	35+75			
L		6.8	54.8	
+10		6.3	55.3	
+20		5.5	56.1	55.7
C		9.6	57.0	
+10		12.3	49.3	
+20		16.1	45.5	47.4
R		19.2	42.4	

	$36+01^{10}$ = P.T.			
R	61.6	14.6	47.0	
+10		11.8	49.8	
+20		9.4	52.2	51.0
℄		8.6	53.0	
+10		8.2	53.4	
+20		7.9	53.7	53.6
L		7.6	54.0	
	$36+28^{67}$ = P.C.			
L		7.0	54.6	
+10		7.3	54.3	
+20		7.7	53.9	54.1
℄		8.4	53.2	
+10		9.1	52.5	
+20		9.6	52.0	52.2
R		11.9	49.7	

	36+50			
R	61.6	11.7	49.9	
+10		10.0	51.6	
+20		8.6	53.0	52.3
℄		7.6	54.0	
+10		6.8	54.8	
+20		6.1	55.5	55.1
L		5.5	56.1	
	36+75			
L		4.8	56.8	
+10		6.1	55.5	
+20		7.4	54.2	54.9
℄		8.7	52.9	
+10		10.1	51.5	
+20		11.3	50.3	50.9
R		12.4	49.2	

		61.56			
		37+00			
R		61.6	17.8	43.8	
+10			17.7	43.9	
+20			15.0	46.6	45.3
℄			13.5	48.1	
+10			11.1	50.5	
+20			8.3	53.3	51.9
L			5.7	55.7	
		37+75			
L			10.5	51.1	
+10			13.1	48.5	
+20			13.8	47.8	48.1
T.P.	5.75	54.85	17.46	49.10	
℄			17.0	47.8	
+10			14.0	40.8	
+20			17.5	37.3	39.1
R			20.1	34.7	

		37+50			
R		54.8	20.3	34.5	
+10			17.1	37.7	
+20			14.9	40.4	39.0
℄			10.7	44.1	
+10			7.8	47.0	
+20			4.1	50.7	48.8
L			1.6	53.2	
		37+83.20 = P.C.C.			
L			0.3	54.5	
+10			2.8	52.0	
+20			5.7	49.1	50.6
℄			10.1	44.7	
+10			14.6	40.2	
+20			16.3	38.5	39.3
R			17.6	37.2	

		54.85			
		38+00			
R		54.8	16.5	38.3	
+10			15.2	39.6	
+20			13.5	41.3 (1.7)	40.4
¢			9.2	45.6	
+4			5.3	49.5	
+10			4.0	50.8	
+20			2.0	52.8	51.8
L			0.0	54.8	
		38+25			
L			3.8	51.0	
+10			7.6	47.2	
+20			10.5	44.3 (1.5)	45.8
¢			12.6	42.2	
+10			19.4	40.4	
+20			15.6	39.2	39.8
R			19.3	35.5	
T.P	4.56	46.69	12.72	42.13	

		38+50			
R		46.7	14.3	32.4	
+10			13.0	33.7	
+20			10.6	36.1	34.9
¢			8.0	38.7	
+10			4.9	41.8 (1.3)	
+20			2.3	44.4	43.1
L			+2.7	49.4	
		38+75			
L		46.7	3.7	43.0	
+10			5.7	41.0	
+20			8.3	38.4 (1.3)	39.7
¢			11.9	34.8	
+10			14.9	31.8	
+20			16.9	29.8	30.8
R			18.6	28.1	

47 Quince 23.98 54

75'40

	46.69				
	38+90				
R	46.7	21.2	25.5		
+10		19.3	27.4		
+20		17.0	29.7	28.5	
℄		15.0	31.7		
+10		12.7	34.0		
+20		6.7	40.0	37.0	
L		6.1	40.6		
	39+06.58 = P.T.				
L		4.6	42.1		
+10		5.7	41.0		
+18		5.8	40.9	40.9?	
+20		8.5	38.2		
℄		12.5	34.2		
+6		16.9	29.8		
+10		17.9	28.8		
+20		19.3	27.4	28.1	
R		21.2	25.5		

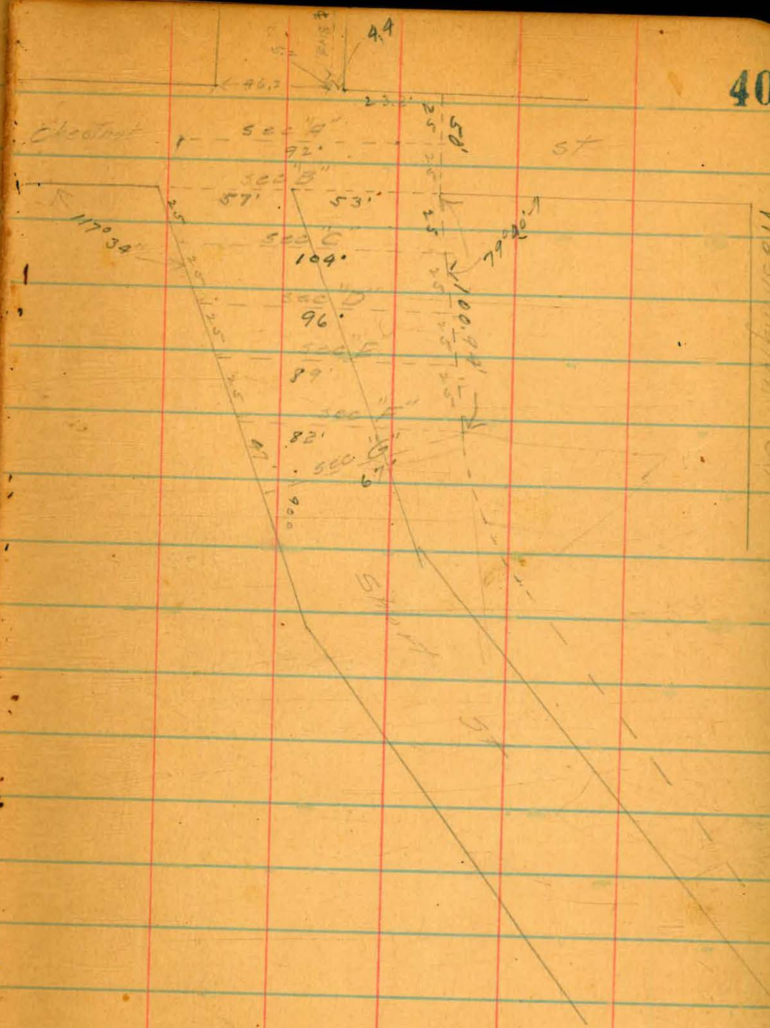
	39+25				
R	46.7	18.7	28.0		
+10		17.7	29.0		
+20		14.8	31.9	30.5	
℄		10.9	35.8		
+9		8.3	36.4		
+10		6.1	40.6		
+20		5.4	41.3	40.9	
L		4.5	42.2		
	39+59.28 = N.L. Chestnut St 50' wide				
L		5.8	40.9		
+10		7.1	39.6		
+20		8.3	38.4	39.0	
+28		12.3	36.4		
T.P.	2.99	36.25	12.88	33.81	
℄		3.4	37.8		
+10		7.6	28.8		
+20		10.7	25.7	27.2	
R		12.8	23.4		

X-sec "A"

R		36.5	22.8	13.4
+10			21.8	14.4
+20			20.5	15.4
+30			16.9	19.3
+40			15.1	21.1
+50			12.6	23.6
+60			8.4	27.8
+70			5.8	30.4
+80			3.9	32.3
+92 = L			+1.1	37.3

X-sec "B"

L		36.2	4.9	31.8
+10			6.8	29.4
+20			10.0	26.2
+30			12.5	23.7
+40			16.4	19.8
+50			18.3	17.9
+60			20.2	16.0
+70			21.9	14.3
+80			23.9	12.3
+90			24.2	12.0
+109.6 = R			25.0	11.2



36.25

1-sec "C"

R	36.2	25.5	10.7
+8		25.8	10.4
+14		22.3	13.9
+30		23.6	12.6
+40		21.2	15.0
+65		17.2	19.0
+80		11.6	24.6
+90		7.8	28.4
10 A=L		2.5	33.7
T.P.	0.36	34.68 1.93	34.32

1-sec "D"

L	34.7	0.7	34.0
+10		4.3	30.4
+20		6.2	28.5
+30		8.7	26.0
+40		12.3	22.4
+44		13.3	21.4
+52		18.7	16.0
+62		20.3	14.4
+77		20.7	14.0
+90		24.9	10.3
+96=R		25.1	9.6

34.78

1-sec "E"

L	34.7	26.0	8.7
+3		26.0	8.7
+20		19.7	15.0
+30		19.3	15.4
+45		18.0	16.7
+50		13.7	21.0
+53		11.0	23.7
+60		9.5	25.2
+70		6.8	27.9
+80		4.7	30.0
+89=R		1.4	33.4

1-sec "F"

L	34.7	4.0	30.7
+10		6.8	27.9
+20		9.6	25.1
+23		9.3	25.4
+37		17.5	17.2
+45		18.4	16.3
+60		18.6	16.1
+82=R		25.5	8.9

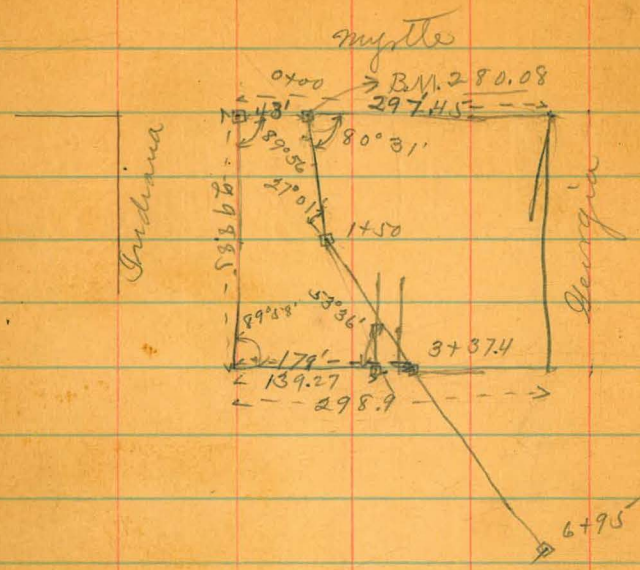
3168

1-3cc G

R	34.7	24.9	9.8
+2		24.7	10.0
+5		22.1	12.6
+17		18.2	16.5
+30		18.2	16.5
+40		16.8	17.9
+44		12.7	22.0
+50		10.3	24.4
+60		6.7	28.0
+67 = L		4.1	30.6

Road down canyon back of Country Club.

July 20/10 Childs Barber Taylor



		H.I.		
T.P.	2.40	304.95		302.55 BM
T.S.			12.34	292.61
		0.54	293.15	
T.P.			13.07	280.08

July 29/10 Childs Barber Taylor

Quittoc — — 23.98 — 57

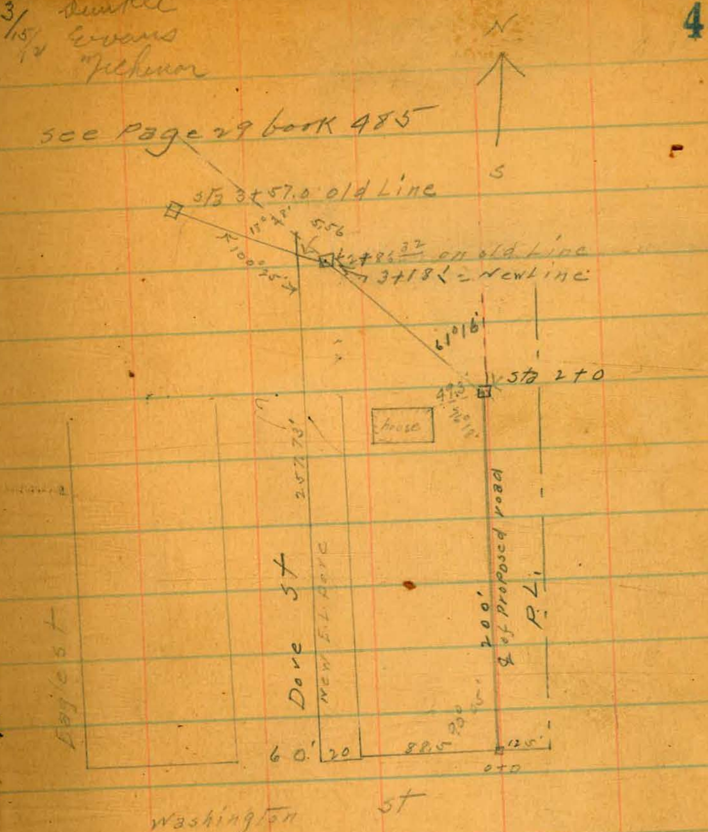
75.40

Re-survey of Dove St Canyon road from point on N.L. Washington St 88.5 E of Dove (20.80 wide) or 12.5 W. of P.L. to S/a 7+27.17 in book 485 P 28 & 29 see opp page

B.M. 6+253 P/g Dove & Wash				264.46
B.M.	1.42	265.88		
0+0			2.3	263.6
0+25			4.8	261.1
+50			7.7	258.2
+75			10.8	255.1
T.P.	0.34	253.40	12.82	253.06
1+0			3.6	249.8
1+25			6.8	246.6
T.P.	1.09	241.87	12.62	240.78
+50			2.8	239.1
+75			7.4	234.5
2+0 △			17.9	224.0
+25			8.9	233.0
+50			6.5	235.4
+75			4.3	237.6
3+0			2.5	239.4
T.P.	1.68	239.67	3.88	237.99
3+18 (2+56.32 old line) △ New Line			2.0	239.7
3+25			2.0	237.7

3/15/18 Dunkle Evans McKeever

see Page 29 book 485



		239.67		
3+50			6.2	233.5
T.P	0.94	228.51	12.10	227.57
+75			1.1	227.4
3+57 old				
3+88.25 new			3.8	224.7
4+0			5.7	222.8
+25			14.0	214.5
4+21.37 old				
4+53.5 new			14.7	213.8
+75			15.8	212.7
5+0			12.9	215.6
+25			12.6	215.9
T.P.	0.33	216.48	12.36	216.15
+50			1.5	215.0
5+44.77 old.				
5+76.5 New			4.9	211.6
6+0			8.9	208.1
+75			13.3	203.2
T.P.	1.27	204.90	12.85	203.63
+50			5.9	199.0
+75			9.0	195.9
7+0			10.3	194.6
+25			10.2	194.7
7+27.27 old.				
7+59.05 New			10.3	194.6

32nd & Nutmeg St X Sec 4-23-26 miller

60' wd Palm St X Sec from E line 32nd W.

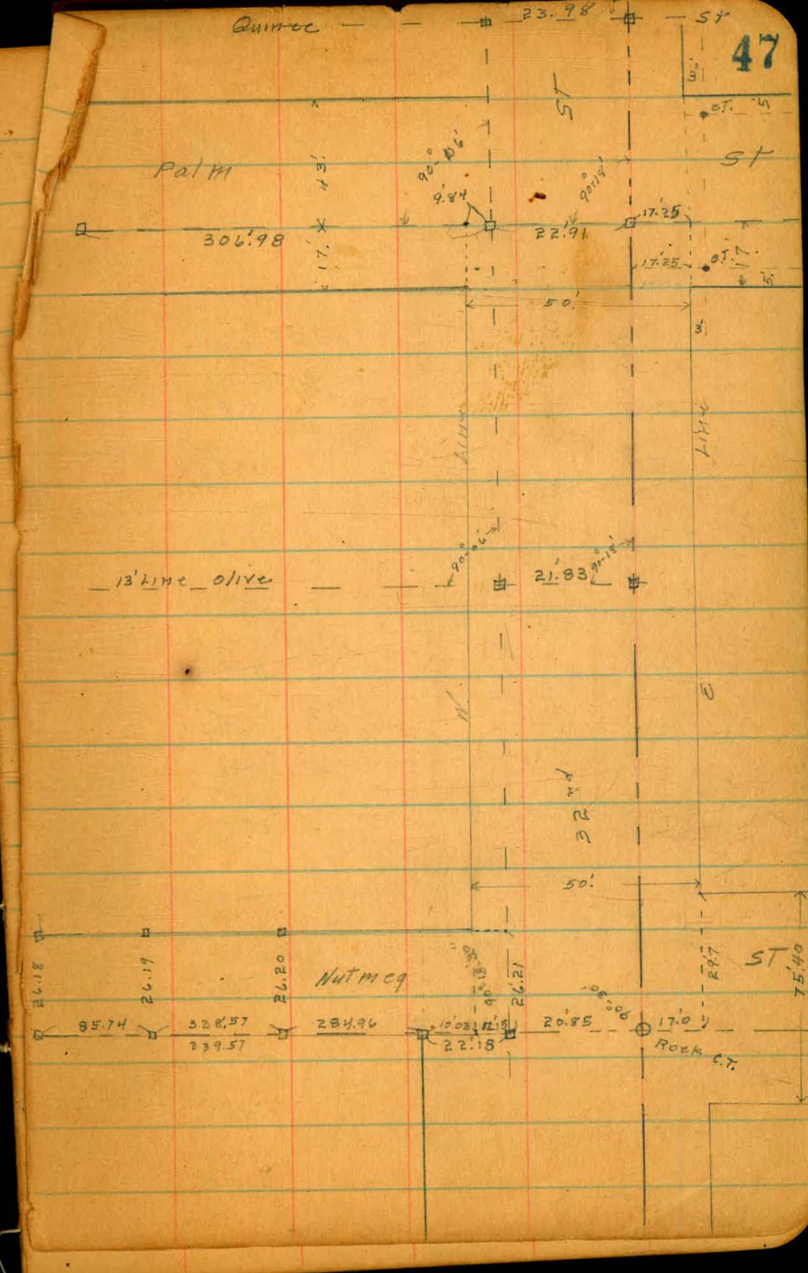
BM		12.63	306.71		294.08 N.E Bancroft & Nutmeg
T.P.	B.M.B.P.	3.64	308.68	1.67	305.04 N.E Bancroft & Palm

E. Line 32nd St 50' wide 10' clr 75'

		308.7	
N	4.4	304.3	
cl	4.68	304.0	W end cmt cl
+1	5.3	303.4	
1/4	4.9	303.8	
e	4.7	304.0	
3/4	4.8	303.9	
cl	5.13	303.6	W end cmt cl
+9	4.8	303.9	
S	2.4	306.3	

E. cl

S	2.6	306.1	
+3	3.8	304.9	
cl	4.0	304.7	
1/4	4.3	304.4	
e	3.8	304.9	
3/4	4.2	304.5	



308.68

			308.7
+8	E. el (corn)	5.5	303.2
el		4.8	303.9
N		4.0	304.7
	E. ¼		
N		3.9	304.8
el		4.7	304.0
+2		5.4	303.3
¼		3.9	304.8
C		3.7	305.0
¼		3.8	304.9
el		3.4	305.3
S		2.7	306.0
	E 32nd		
S		2.4	306.3
el		3.2	305.5
¼		3.4	305.3
C		3.6	305.1
¼		3.4	305.3

308.68 Palm

			308.7
+5		4.1	304.6
+6		5.3	303.4
el		5.4	303.3
+1		4.4	304.3
N		4.2	304.5
	W. ¼		
N		4.2	304.5
+		4.4	304.3
el		5.6	303.1
+4		5.7	303.0
+5		4.0	304.7
¼		3.3	305.4
C		3.4	305.3
¼		3.3	305.4
el		3.0	305.7
S		2.0	306.7
	W. el		
S		1.9	306.8

Palm

W. el (con)

		308.68	308.2
el		3.0	305.7
½		3.3	305.4
c		3.4	305.3
½		3.3	305.4
+5		4.0	304.7
+6		5.6	303.1
el		5.7	303.0
+1		4.4	304.3
N		4.3	304.4
00 = W Line 32nd St.			
N		4.5	304.2
+9		4.4	304.3
el		5.5	303.2
+4		5.7	303.0
+5		3.8	304.9
½		3.1	305.6
c		3.3	305.4
½		3.1	305.6

		308.68	308.2
el		2.9	305.8
5		2.0	306.7
25' W			
5		1.9	306.8
el		2.6	306.1
½		2.9	305.8
c		3.9	304.8
½		4.2	304.5
+5		4.5	304.2
+6		5.9	302.8
el		6.1	302.6
+1		4.8	303.9
N		5.3	303.4
50' W.			
N		6.9	301.8
+7		6.0	302.7
+8		7.6	301.1
el		7.6	301.1

	308.68		308.2
el+1	50'w	7.4	301.1
+2		5.5	303.2
1/4		4.9	303.8
c		4.0	304.7
1/4		3.2	305.5
el		2.6	306.1
E		2.7	306.0
	75'w		
S		4.0	304.7
el		4.0	304.7
1/4		5.0	303.7
c		5.2	303.5
1/4		6.4	302.3
+8		7.0	301.7
el		8.4	300.3
+3		9.3	299.4
+4		8.1	300.6
N		8.5	300.2
+5		8.7	300.0

	308.68		308.7
	100'w		
-5		9.8	298.9
N		10.6	298.1
el		9.0	299.7
1/4		8.4	300.3
c		7.6	301.1
1/4		7.3	301.4
el		6.6	302.1
S		6.3	302.4
	125'w		
S		7.8	300.9
el		8.1	300.6
1/4		8.8	~~299.9~~
c		9.3	~~299.4~~
1/4		10.0	298.7
el		10.4	298.3
N		11.5	297.2
+10		12.4	296.1

308.68

150' W

-10		12.6	308.2 / 296.1
N		11.8	296.9
el		11.1	297.6
114		10.6	298.2
C		9.4	298.9
114		9.2	299.5
el		8.4	299.9
S		8.3	300.4

175' W

S		8.6	300.1
el		8.9	299.8
114		9.3	299.4
C		9.6	299.1
114		10.1	298.6
el		10.4	298.3
N		10.8	297.9
+5		11.0	297.7

308.68

Palm

200' W

N		10.0	308.2 / 298.7
el		9.7	299.0
114		9.5	299.2
C		9.2	299.5
114		8.9	299.8
el		8.6	300.1
S		8.6	300.1

225' W

S		8.9	299.8
el		8.9	299.8
114		9.0	299.7
C		9.2	299.5
114		9.4	299.3
el		9.7	299.0
N		9.9	298.8

250' W

N		11.5	297.2
el		10.8	297.9

	308.68			
	250' W (com)		308.7	
1/4		10.5	298.2	
e		10.2	298.5	
1/4		10.0	298.7	
el		9.7	299.0	
S		9.6	299.1	
	R70' W			
S		10.6	298.1	
el		10.9	297.8	
1/4		11.4	297.3	
e		12.1	296.6	
1/4		12.7	296.0	
el		13.3	295.4	
T.P.	0.65 296.53	12.80	295.88	
			296.5	
N		8.8	293.7	
	R95' W		✓	
N		13.6	282.9	
el		7.6	288.9	
1/4		4.1	292.4	

	296.53		Palm	
			296.5	
1/4		3.6	292.9	
e		2.5	294.0	
1/4		1.8	294.7	
el		0.9	295.6	
S		0.2	296.3	
	330' W			
S		5.4	291.1	
el		6.0	290.5	
1/4		7.1	289.4	
e		8.4	288.1	
1/4		10.7	285.8	
el		12.8	283.7	
N		18.8	277.7	

50' wide
10' cl
7.5 1/43

32nd St & Sec

From S. line Palm to N. line Nulmeg

4-24-26
mills

B.M.	8.40	312.40	304.00	N.E. Palm + 32nd

00 = S line Palm 312.4

E	6.1	306.3
cl	6.3	306.1
1/4	6.4	306.0
C	6.1	306.3
1/4	5.7	306.7
cl	5.6	306.8
W	5.7	306.7

25' S.

W	3.6	308.8
cl	4.1	308.3
1/4	4.4	308.0
C	5.2	307.2
1/4	5.5	306.9
cl	5.6	306.8
E	5.8	306.6

312.40

50' S

		312.4
E	5.8	306.6
cl	5.5	306.9
1/4	5.2	307.2
C	4.8	307.6
1/4	3.9	308.5
cl	3.0	309.4
W	1.9	310.5

75' S

W	0.5	311.9
cl	2.2	310.2
1/4	3.4	309.0
4 6	4.1	308.3
C	5.0	307.4
1/4	5.6	306.8
cl	5.9	306.5
E	6.4	306.0

100' S

E	7.3	305.1

312.40

100' S eor

el		7.2	312.4 / 305.2
1/4		6.9	305.5
c		6.6	305.8
+1.5		5.5	306.9
1/4		4.9	307.5
el		4.~	308.2
w		3.1	309.3
	125' S		
w		4.0	306.4
el		6.9	305.5
1/4		7.2	305.2
+4		7.5	304.9
c		8.1	304.3
1/4		8.3	304.1
el		8.3	304.1
E		8.4	304.0
	150' S		
E		9.7	302.7

312.40

el		9.7	312.4 / 302.7
1/4		9.5	302.9
c		9.3	303.1
1/4		8.9	303.5
el		8.8	303.6
w		8.7	303.7
	175' S		
w		11.0	301.4
el		11.0	301.4
1/4		10.5	301.9
c		10.6	301.8
1/4		10.7	301.7
el		10.6	301.8
E		10.6	301.8
	200' S		
E		11.5	300.9
el		11.7	300.7
1/4		11.5	300.9

312.40

200's (con't)

			312.4
E		11.7	300.7
1/4		11.8	300.6
el		11.8	300.6
W		12.0	300.4

250' S

W		13.9	298.5
el		13.8	298.6
1/4		13.5	298.9
E		13.6	298.8
1/4		13.3	299.1
el		13.4	299.0
E		13.1	299.3
T.P.	0.05	299.51	12.94	299.46

300' S

299.5

E		2.2	297.3
el		2.3	297.1
1/4		2.2	297.3
E		2.2	297.3

299.51

3rd

299.5

1/4		2.2	297.3
el		2.3	297.2
W		2.4	297.1

350' S

W	3.7	295.8
el	3.8	295.7
1/4	4.1	295.4
E	4.2	295.3
1/4	4.2	295.3
el	4.4	295.1
E	4.3	295.2
+5	4.3	295.2

375' S

E-5	5.4	294.1
E	5.4	294.1
el	5.0	294.5
1/4	4.9	294.6
E	4.6	294.9

312.40

299.51

	375' S (cont)		299.5
1/4		4.2	295.3
cl		3.7	295.8
W		3.4	296.1
	400' S		
W		2.6	296.9
cl		2.8	296.7
1/4		3.5	296.0
+6		3.7	295.8
E		4.3	295.2
1/4		4.5	295.0
cl		5.0	294.5
E		5.5	294.0
+5		5.7	293.8
	425' S		
-5		5.5	294.0
E		5.1	294.4
cl		4.5	295.0
1/4		4.1	295.4
E		3.8	295.7

299.51

32 ft

			299.5
+1.5		3.2	296.3
1/4		2.9	296.6
cl		2.6	296.9
W		2.4	297.1
	450' S		
W		2.6	296.9
cl		2.7	296.8
1/4		3.0	296.5
+6		3.2	296.3
E		3.6	295.9
1/4		3.8	295.7
cl		4.0	295.5
E		4.6	294.9
	475' S		
E		4.8	294.7
cl		4.5	295.0
1/4		4.4	295.1
E		4.3	295.2

	299.51		
	475.5 (EOH)		299.5
+4		3.3	296.2
1/4		3.3	296.2
cl		3.4	296.1
W		3.2	296.3
	500.5		
W		4.5	295.0
cl		4.6	294.9
1/4		5.0	294.5
C		5.5	294.0
1/4		5.6	293.9
cl		5.4	294.1
E		5.5	294.0
	525.5		
E		6.7	292.8
cl		6.7	292.8
1/4		7.2	292.3
C		7.1	292.4
1/4		7.0	292.5

	299.51		32 ft
			299.5
cl		6.4	293.1
W		6.4	293.1
	550.5		
W		9.0	290.5
cl		8.6	290.9
1/4		9.1	290.4
C		9.7	289.8
1/4		9.9	289.6
+5		10.1	289.4
cl		8.8	290.7
E		8.6	290.9
	575.5		
E		11.8	287.7
+8		11.5	288.0
cl		13.1	286.4
1/4		13.2	286.3
C		13.0	286.5
1/4		13.3	286.2

299.51
575'S con

			11.8	299.5 / 287.7
1/4+2				
d			12.0	287.5
W			12.2	287.3
T.P.	3.46	290.27	12.70	286.81

595.5 5.= q Line 29.7 N. of P.L. = produced from E. N. Line Nut mg

				290.3
W			5.6	284.7
d			5.2	285.1
+6			5.3	285.0
1/4			6.5	283.8
E			6.5	283.8
1/4			6.7	283.6
+5			6.8	283.5
d			5.4	284.9
E			5.5	284.8
chk B.M.			4.56	285.71 = 285.72 B.M. S.W. San Marcos 4 3rd

75.4 wide
10' of N
13' 11¼ S
13.4 ch. S

Nutmeg St & Sec

4/29/N
shutin

B.M.	4.24	298.32	294.08	N.E. Nutmeg & Bancroft
			298.3	

00 = E. Line 33rd on N.

N		5.7	292.6
el		5.6	292.7
¼		5.4	292.9
c		4.7	293.6
+1		3.5	294.8
¼		3.0	295.3
el		2.7	295.6
S		2.6	295.7
	25' E		
S		5.2	293.1
el		5.3	293.0
¼		5.7	292.6
c		6.2	292.1
¼		7.1	291.2
el		7.3	291.0

298.32

298.3

N		7.1	291.2
	50' E		
N		8.5	289.8
+4		9.1	289.2
+5		8.5	289.8
el		8.5	289.8
¼		9.1	289.2
c		9.6	288.7
¼		9.6	288.7
el		9.2	289.1
S		8.8	289.5
	58' E		
S		10.0	288.3
el		10.3	288.0
¼		10.7	287.6
c		10.8	287.5
¼		9.8	288.5
el		9.2	289.1

	298.32		
	58' E (con)		298.3
+6		9.8	288.5
+7		13.0	285.3
N		13.0	285.3
+5		10.7	287.6
	65' E		
-5		14.7	283.6
N		12.8	285.5
el		10.7	287.6
1/4		10.5	287.8
+7		10.8	287.5
e		12.6	285.7
1/4		12.1	286.2
el		11.4	286.9
S		10.9	287.4
	75' E		
S		12.5	285.8
el		13.1	285.2
1/4		14.1	284.2

				Nutmeg
	298.32			298.3
e			15.0	283.3
1/4			14.6	283.7
el			16.1	282.2
N			17.2	281.1
+5			16.8	281.5
	80' E			
-7			18.5	279.8
N			18.4	279.9
el			17.2	281.1
1/4			16.2	282.1
e			16.4	281.9
1/4			15.5	282.8
el			14.3	284.0
S			13.4	284.9
T.P.	0.38	285.76	12.94	285.38
	100' E			285.8
S			5.2	280.6
el			4.2	279.6

285.76 (285.8)

100' E (con)

10	1/4	6.6	279.2
	C	7.3	278.5
	+4	8.4	277.4
	+6	7.6	278.2
	1/4	8.0	277.8
	cl	8.5	277.3
	N	9.3	276.5
	+10	10.1	275.7
	118' E = W Line Alley		
	-12	14.5	271.3
	N	12.8	273.0
	cl	12.0	273.8
	1/4	11.6	274.2
	+6	11.0	274.8
	+8	11.8	274.0
	C	10.6	275.2
	1/4	9.8	276.0
	cl	9.1	276.7

285.76 Nutmeg (285.8)

	S	8.6	277.2
	+5	8.4	277.4
	133' E = E. Line Alley		
	-5	11.2	274.6
	S	11.4	274.4
	cl	11.8	274.0
	1/4	12.4	273.4
	C	13.3	272.5
	+5	14.3	271.5
	+8	13.8	272.0
	1/4	14.0	271.8
	cl	14.5	271.3
	N	15.4	270.4
	+15	16.9	268.9
	148' E		
	N-25	25.7	260.1 Ewash
	-13	22.2	263.6
	N	19.9	265.9

285.76 148'E eob

		285.8	
el	18.0	267.8	
+4	16.8	269.0	
1/4	16.6	269.2	
+6	16.7	269.1	
+8	16.4	267.4	
+10	16.6	269.2	
e	15.9	269.9	
1/4	15.2	270.6	
d	14.6	271.2	
s	14.0	271.8	
+5	14.1	271.7	
	158'E		
-10	15.5	270.3	
s	15.6	270.2	
el	16.4	269.4	
1/4	17.1	268.7	
+9	18.3	267.5	
e	19.9	265.9	

285.76 Nutmeg

62

		285.8	
+4	21.1	264.7	
+5	20.0	265.8	
1/4	19.1	266.7	
el	21.8	264.0	
1	22.5	263.3	
+11	25.6	260.2	
+16	25.4	260.2	& wash
+19	25.3	260.5	
+26	22.3	263.5	
	164'E		
-20	22.5	263.3	
-14	25.4	260.4	
-7	26.0	259.8	& wash
1	26.1	259.7	
d	24.2	261.6	
1/4	22.2	263.6	
+8	21.3	264.5	
+9	24.4	261.4	

285.76

164' E (con)

E	24.3	261.5	285.8
+2	22.1	263.7	
1/4	20.5	265.3	
el	18.7	267.1	
S	17.7	268.1	
+10	17.1	268.7	

174' E

-10	19.9	265.9	
S	20.8	265.0	
+4	20.9	264.9	
el	23.7	262.1	
1/4	25.0	260.8	
E	27.2	258.7	
+3	27.3	258.5	
+4	26.0	259.8	
1/4	26.6	259.2	
el	28.0	257.8	¢ wash
N	26.4	259.4	
+20	19.0	266.8	

285.76

Nut mcy

181' E

-20	17.7	268.1	285.8
N	22.6	263.2	
el	26.0	259.8	
1/4	28.2	257.6	
+2	28.2	257.6	¢ wash
+11	28.7	257.1	
+12	30.5	255.3	
C	30.5	255.3	
+3	31.2	254.6	
+4	29.0	256.8	
1/4	29.0	256.8	
el	26.3	259.5	
S	23.6	262.2	
+10	22.2	263.6	

194' E

-15	26.5	259.3	
S	28.5	257.3	
+3	30.2	255.6	

285.76

194' E

		285.8	
+9	32.3	253.5	℄ Wash
cl	31.5	254.3	
1/4	28.4	257.4	
+9	25.5	260.3	
C	25.8	260.0	
+5	25.9	259.9	
+6	24.7	261.1	
1/4	23.1	262.7	
cl	21.4	264.4	
N	20.4	265.4	
+10	17.8	268.0	
	204.		
-10	15.9	269.9	
N	18.0	267.8	
cl	20.3	265.5	
1/4	21.5	264.3	
C	23.2	262.6	
1/4	25.0	260.8	

285.76 Nutmeg

64

		285.8	
cl	27.2	258.6	
S	32.8	253.0	℄ wash
+6	32.8	253.0	
+15	30.0	255.8	
+25	27.3	258.5	
215' E			
-25	31.4	254.4	
-11	33.8	252.0	℄ wash
S	28.4	257.4	
cl	24.5	261.3	
1/4	23.0	262.8	
C	21.5	264.3	
1/4	19.4	266.4	
cl	17.4	268.4	
N	16.0	269.8	
+7	14.8	271.0	

285.76

	225' E		285.8
-7		13.5	272.3
N		14.5	271.3
el		14.5	269.3
1/4		17.7	268.1
C		20.0	265.8
1/4		21.8	264.0
el		22.8	263.0
S		26.1	259.7
+22		34.4	251.4
+25		34.4	251.4 ℄ Wash
+32		34.6	251.2
			50' wide 10' clr 25' left
	250' E - W Line Felton		
-15		25.0	260.8
S		20.9	264.9
el		18.8	267.0
1/4		17.0	268.8
C		15.4	270.4
1/4		13.8	272.0

285.76

el	12.4	285.8 / 273.4
N	10.8	275.0
	W. el	
N	9.3	276.5
el	10.5	275.3
1/4	12.6	273.2
C	13.7	272.1
1/4	15.3	270.5
el	17.2	268.6
S	18.8	267.0
+12	21.3	264.5
	W. 1/4	
-10	18.8	267.0
S	17.6	268.2
el	14.1	269.7
1/4	14.4	271.4
C	12.0	273.8
1/4	10.8	275.0

285.76
N. 1/4

cl	9.6	285.8 / 276.2
N	8.7	277.1

& Felton

N	7.7	278.1
cl	8.8	277.0
1/4	9.9	275.9
C	10.8	275.0
1/4	11.9	273.9
+8	12.5	273.3
cl	14.6	271.2
S	16.3	269.5
+10	17.7	268.1

E. 1/4

-10	16.5	269.3
S	15.1	270.7
cl	12.6	273.2
1/4	11.2	274.6
C	10.0	275.8

285.76
Nutmeg

1/4	9.1	285.8 / 276.7
cl	7.7	278.1
N	6.8	279.0

E. cl

N	6.1	279.7
cl	6.9	278.9
1/4	8.2	277.6
C	9.3	276.5
1/4	10.5	275.3
cl	11.8	274.0
S	13.4	272.4
+10	14.6	271.2

E. Line Felton

-10	13.2	272.6
S	12.2	273.6
cl	10.6	275.2
1/4	9.5	276.3
C	8.6	277.2

280 ¼	285.76	7.0	285.8 / 278.8
d		5.7	280.1
V		4.6	281.2

LONG BRANCH Cross Section 50 wide 10' cls

ABBOTT ST. West 1/40'

N WIRE	16.4	11.77	10.13	Bright of Abbott
W.L. Abbott = 00			11.8	
S		8.1	3.7	
cb to b cen cb		8.0n	3.8	
1/4		8.6	3.7	
e		8.6	3.7	
1/4		8.9	7.9	
cb to b cen cb		9.07	7.7	
N		8.8	3.0	
	0+10			
N		9.2	7.6	
cb		9.2	7.6	
1/4		9.2	7.6	
e		9.2	7.6	
1/4		9.1	7.7	
cb		9.0	7.8	
S		8.7	3.1	

Abbott 12/2/26 11.77

	0+50	11.8
-S	9.6	7.7
S	9.5	7.3
cb	9.5	7.0
1/4	10.1	1.7
e	9.6	7.7
1/4	9.5	7.3
cb	9.7	7.1
N	9.6	7.7
+S	9.6	7.7
	0+79	
-S	9.8	7.0
N	9.7	7.1
cb	10.0	1.8
1/4	9.8	7.0
e	9.7	7.1
1/4	10.1	1.7
cb	10.0	1.8

	11.77	11.8
S	9.7	1.1
+S	9.5	1.3
0+8S		
-S	9.7	1.3
S	9.6	1.4
cb	10.0	1.8
1/S	10.1	1.7
c	9.7	1.1
1/4	9.8	1.0
cb	10.1	1.7
N	in yard	8.8 3.0
1+1S		
N	" "	9.0 2.8
cb	10.0	1.8
1/S	10.0	1.8
c	10.0	1.8
1/4	10.1	1.1
cb	10.5	1.3

	11.77	Long Branch 11.8
S	10.0	1.8
+S	9.9	1.9
1+20		
-S	10.3	1.5
S	10.2	1.6
cb	10.2	1.3
1/4	10.2	1.3
c	10.0	1.8
1/4	9.9	1.9
cb	9.9	1.9
N	10.0	1.8
+S	10.0	1.8
1+10		
-S	10.3	1.5
N	10.2	1.6
cb	10.1	1.7
1/1	10.1	1.7
c	10.1	1.1

11.77

		11.8
1/4	10.9	0.9
cb	11.1	0.7
S	10.8	1.0
+S	10.9	0.9
1+80 = ℄ col. bungalows 18' wide 0.4' WEST on North bdy.		
2+00		
- S -	10.0	1.8
S	10.2	1.6
cb	10.8	1.0
1/4	10.5	1.3
c	10.4	1.4
1/4	9.8	2.0
cb	9.7	2.1
2/	9.8	2.0
+S	10.0	1.8
2+06		
2/ EAST ℄ stairway to Apt house 4' wide	8.27	3.5 on cement on line
cb	9.4	2.4

11.77

Longbranch

	11.8	
1/4	9.8	2.0
e	10.3	1.5
1/4	10.3	1.5
cb	10.9	0.9
S	10.9	0.9
+S	10.9	0.9
2+35 ℄ WEST stairway to above Apt house		S inside
" " "	8.31	3.5 ON CEMENT
2+70		
S	8.6	3.2
cb	8.8	3.0
1/4	8.4	3.4
c	8.5	3.3
1/4	8.5	3.3
cb	8.8	3.0
2/	8.9	2.9
2+45		
2/	9.1	2.7

11.77

		11.8
cb	8.3	3.5
1/4	8.3	3.5
c	8.4	3.4
1/4	8.4	3.4
cb	8.6	3.4
s	8.3	3.5
2+J⁻J⁻		
s	7.6	4.4
+J⁻	8.J⁻	3.3
cb	8.J⁻	3.3
1/s	8.4	3.6
c	8.0	3.8
1/4	7.9	3.9
⊥J⁻	7.7	4.1
cb	7.0	4.8
N	6.4	5.6
4+75		
N	4.5	7.3

11.77

Long Branch

		11.8
cb	J⁻.8	6.0
1/4	7.J⁻	4.3
c.	8.4	3.4
1/4	8.J⁻	3.3
cb	8.0	3.8
s	7.1	4.7
2+87		
s	4.0	7.8
cb	7.6	4.4
1/4	8.6	3.4
+J⁻	8.6	3.4
c.	8.0	3.8
1/4	8.1	3.7
cb	7.0	4.8
+5	6.6	5.4
N	J⁻.6	6.4
3+00		
N	5.7	6.1

11.77

		11.8 / 4.8
H S	7.0	
cb	7.6	4.r
1/4	8.0	3.8
c	8.7	3.1
1/4	8.7	3.1
cb	7.7	4.1
S	7.0	4.8
3+rS		
S	6.8	5.0
cb	7.5	4.3
1/S	8.4	3.4
c	8.5	3.3
1/4	8.1	3.7
cb	6.9	4.9
N	6.0	5.8
3+50		
N	6.0	5.8
+S	5.8	6.0

11.77

Long Branch

11.8 / 4.r

cb	7.6	
1/4	8.0	3.8
c	9.9	1.9
+S	9.7	r.1
1/4	9.0	r.8
cb	7.0	4.8
S	7.r	4.6
3+7S		
S	8.1	3.7
cb	8.r	3.7
1/4	8.8	3.0
c	9.7	r.1
1/1	9.1	r.3
cb	9.0	r.8
N	7.9	3.9
4+00		
N	8.1	3.7
cb	9.1	r.4

11.77

		11.8 / 1.6
1/4	10.2	
e	10.0	1.8
1/4	9.7	2.1
eb	9.2	2.6
S	9.1	2.7
4+15		
S	9.1	2.7
eb	10.0	1.8
1/4	9.9	1.9
e	10.3	1.5
1/4	10.3	1.5
eb	10.3	1.5
N	8.2	3.6
4+25		
N	10.0	1.8
eb	10.4	1.4
1/4	10.6	1.2
e	10.5	1.3

11.77

Long Branch

	11.8 / 2.0
1/4	9.8
eb	10.0 / 1.8
S	10.1 / 1.7
4+4b	
S	10.5 / 1.3
eb	10.7 / 1.1
1/4	10.7 / 1.1
e	10.8 / 1.4
1/4	10.8 / 1.4
eb	10.6 / 1.2
N	10.6 / 1.2

Sewer levels 2 alley
14 Frary Hrs

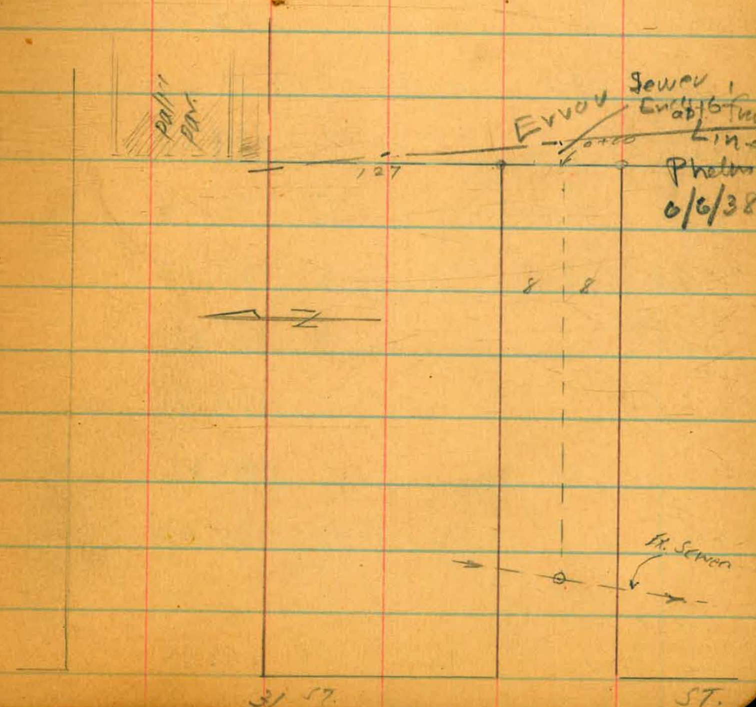
indexed
c.s.k.

NEBP	0.12	304.15		304.03	Palm 32nd
S. side Palm & Pueblo lane			8.09	296.06	Top 26 B.M.
N. side alley	"	"	7.92	296.23	" Pipe
0+00 - Ely end alley Error.			8.2	295.95	
0+25.			10.0	294.15	
0+25			12.3	291.85	
0+50			13.5	290.65	
T.P.	0.46	291.55	13.06	291.09	
0+60			7.0	284.55	
0+75			14.6	276.95	
T.P.	0.23	279.08	12.70	278.85	
0+90			9.9	268.18	
T.P.	0.07	266.22	12.93	266.15	
1+05			5.3	260.92	
1+20			12.7	253.52	
T.P.	0.29	253.61	12.90	253.32	
1+40			8.2	245.41	

253.61

5-17-38

1+60			15.2	238.41	
1+70			16.8	236.81	
T.P.	0.33	242.50	11.44	242.17	
1+84	M.H. Rim		8.40	234.10	
"	" " F.L.		13.10	229.40	



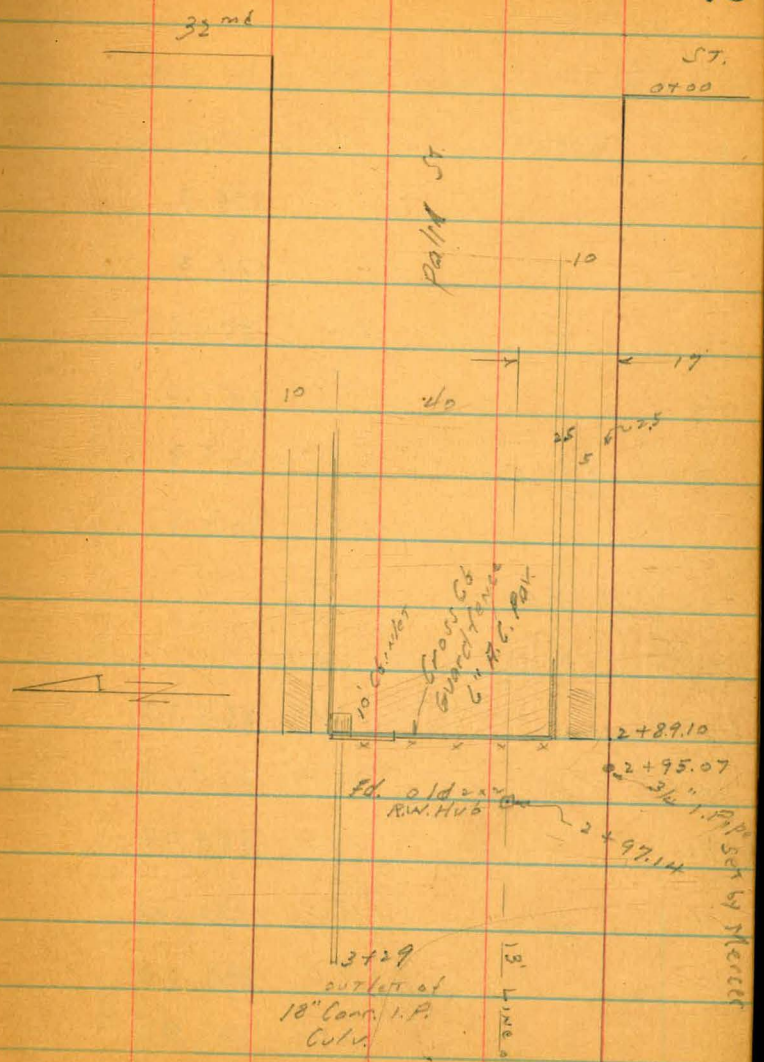
Indexed C.S.K.

Moore 5-19-38.

XSec 30' W of end of Palm St W of 32nd St.

Top B.M. Curb	4+17	300.53	296.06
	7+79.10		
S cb		4.21	296.32
S gut par.		4.88	295.65
C "		5.39	295.14
N gut "		6.15	294.38
N cb		5.28	295.25
	7+89.10 = W'ly end of Paving		
N cb		5.47	295.06
N gut. grate inlet		6.47	294.06
FL. Box of CB inlet		11.18	289.35
C Top cb. cross St		5.02	295.51
C par		5.82	294.71
S cb " gut		5.12	295.41
S cb		4.47	296.06
	7+95.07		
S L. Top 3/4" pipe		4.82	296.21

Top cb S. Side Palm St P 74



3+04.10

S	5.3	295.23
cb	5.5	295.0
C	5.6	294.9
+10	6.0	294.5
cb	8.6	291.9
N	13.5	287.0
+20	24.7	265.8
+40	36.0	264.53

3+19.10

-45	same slope rate as N to -20	
-20	31.8	268.73
N	21.4	279.13
cb	17.1	283.43
+10	10.7	290.33
C	9.8	290.73
cb	7.7	292.83
S	7.4	293.13

300.53

3+29 on N/L Curb line of Palm.

F.L. 18" Corr. I. Pipe Culv. 21.10 279.43
outlet

#400

.85 4.35

3.1
3.88

7.38

280.08 8.38

0.38 HI.
280.46

1,2,86
267.60 J.P.

0,95
268.55 HI.

12,95
255.60 J.P.

0,22
255.82 HI.

12,82
243.00 J.P.

0,65
243.65 HI.

1,45
237.20 J.P.

0,34
231.54 HI.

8,20
223.34 J.P.

1.57
224.91 HI.

10,72
214.19 J.P.

1,49
215.68 HI.

12,43
203.25 J.P.

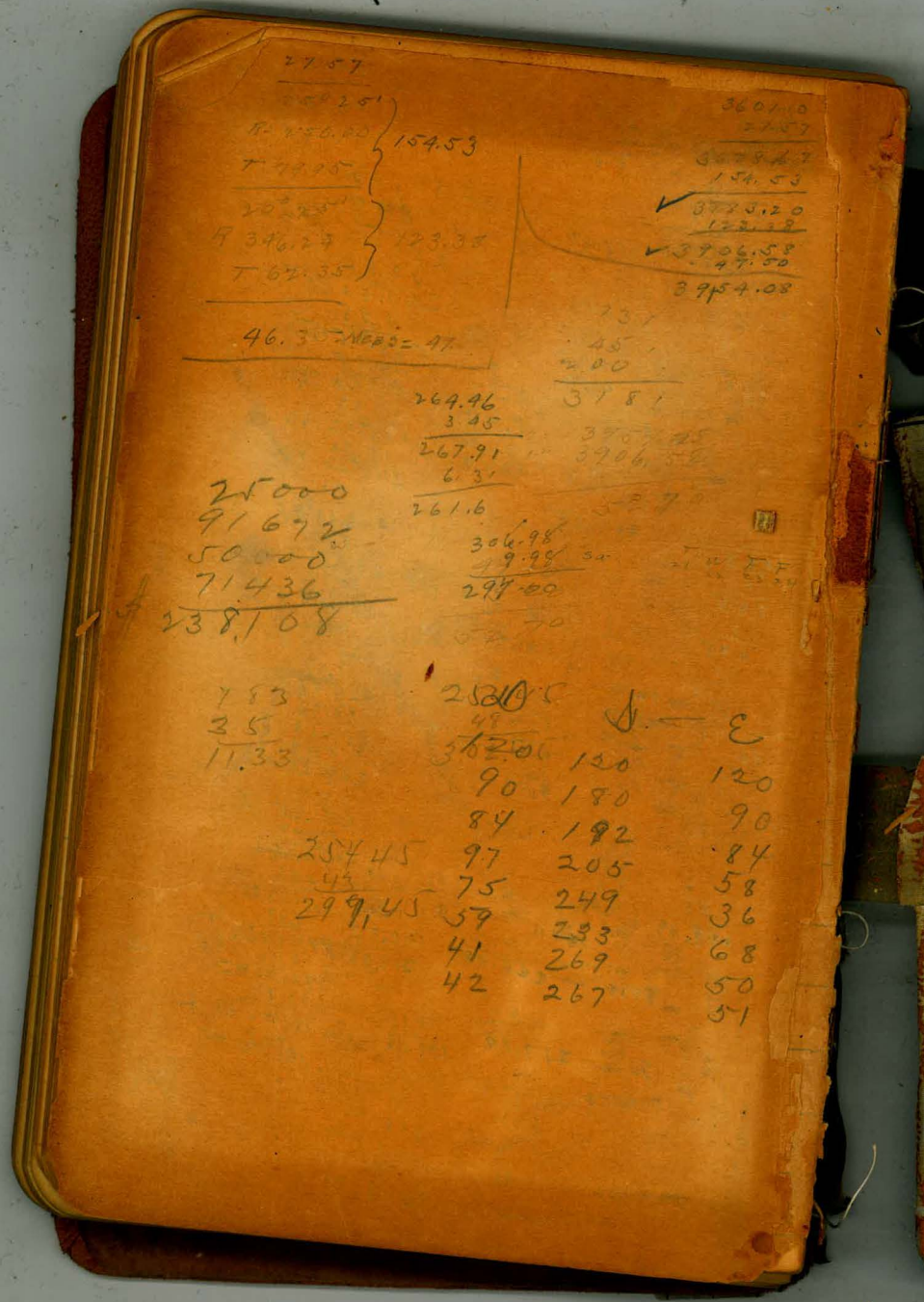
2,88
205.63 HI.

12,97
192.66 J.P.

0,40
193.06 HI.

11,83
181,93 J.P.

4,22
186.56 HI.



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TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							

Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
	DEGREES		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		