

*Return to City Engineers Office  
City Hall, San Diego, Cal.*

TRANSIT

398

**F.B. 374**

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BR. #374

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Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

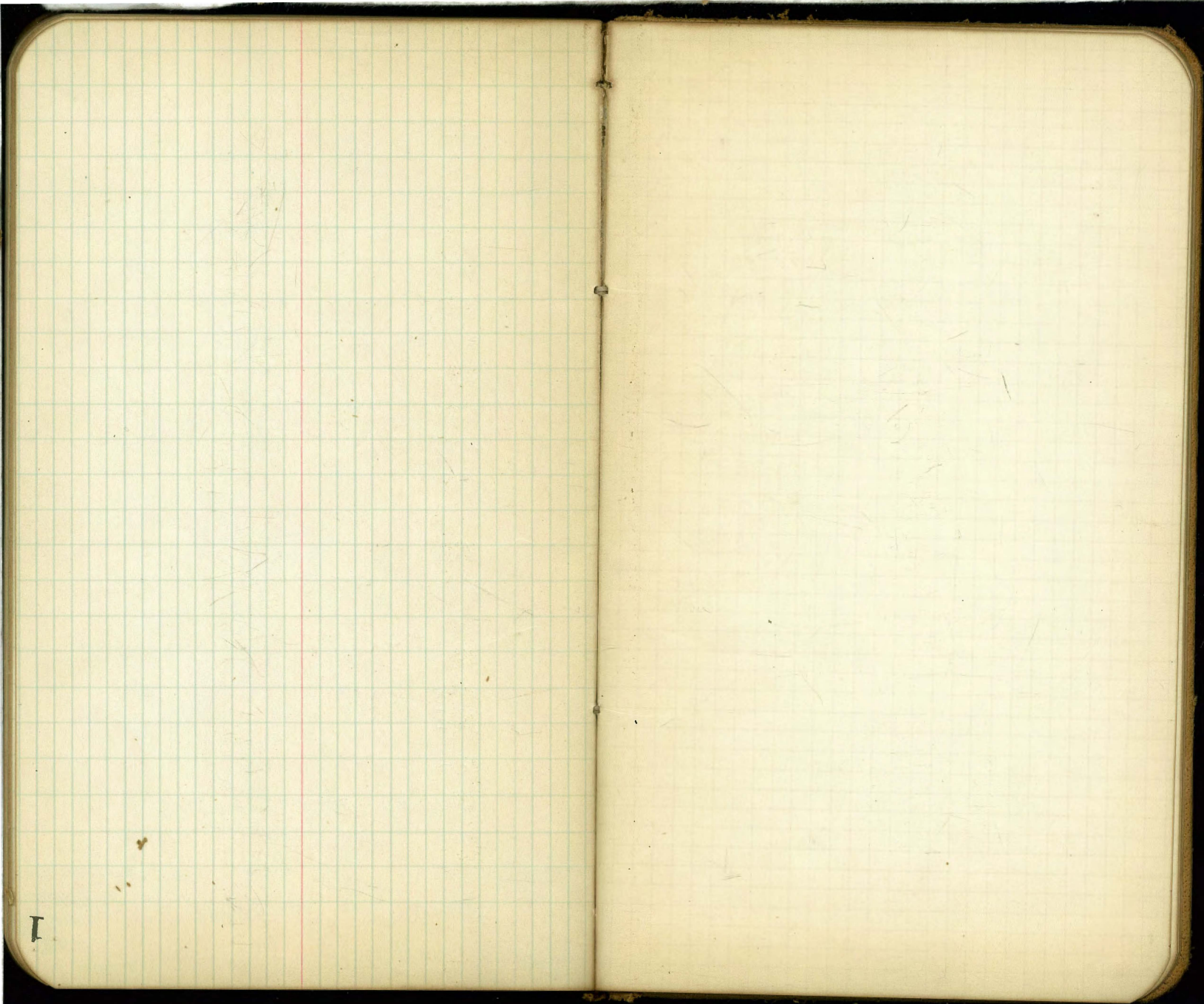
MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1.....	2 $\frac{1}{2}$	21.....	49 $\frac{1}{2}$	41.....	95 $\frac{1}{2}$
2.....	3 $\frac{1}{2}$	22.....	51 $\frac{1}{2}$	42.....	98
3.....	4 $\frac{1}{2}$	23.....	53 $\frac{1}{2}$	43.....	100 $\frac{1}{2}$
4.....	5 $\frac{1}{2}$	24.....	56	44.....	102 $\frac{1}{2}$
5.....	6 $\frac{1}{2}$	25.....	58 $\frac{1}{2}$	45.....	105
6.....	7 $\frac{1}{2}$	26.....	60 $\frac{1}{2}$	46.....	107 $\frac{1}{2}$
7.....	8 $\frac{1}{2}$	27.....	63	47.....	109 $\frac{1}{2}$
8.....	9 $\frac{1}{2}$	28.....	65 $\frac{1}{2}$	48.....	112
9.....	10 $\frac{1}{2}$	29.....	67 $\frac{1}{2}$	49.....	114 $\frac{1}{2}$
10.....	11 $\frac{1}{2}$	30.....	70	50.....	116 $\frac{1}{2}$
11.....	12 $\frac{1}{2}$	31.....	72 $\frac{1}{2}$	51.....	119
12.....	13 $\frac{1}{2}$	32.....	74 $\frac{1}{2}$	52.....	121 $\frac{1}{2}$
13.....	14 $\frac{1}{2}$	33.....	77	53.....	123 $\frac{1}{2}$
14.....	15 $\frac{1}{2}$	34.....	79 $\frac{1}{2}$	54.....	126
15.....	16 $\frac{1}{2}$	35.....	81 $\frac{1}{2}$	55.....	128 $\frac{1}{2}$
16.....	17 $\frac{1}{2}$	36.....	84	56.....	130 $\frac{1}{2}$
17.....	18 $\frac{1}{2}$	37.....	86 $\frac{1}{2}$	57.....	133
18.....	19 $\frac{1}{2}$	38.....	88 $\frac{1}{2}$	58.....	135 $\frac{1}{2}$
19.....	20 $\frac{1}{2}$	39.....	91	59.....	137 $\frac{1}{2}$
20.....	21 $\frac{1}{2}$	40.....	93 $\frac{1}{2}$	60.....	140

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07







Longt cross section of Newport St (80)

Donnan  
Rogers  
5.9.10  
W & L Abbot to Guizot

Brommmer 337	15.64	12.27
417	12.93	8.76

W & L of Abbot St (60)

SL	13.9	-1.0
bl	13.6	-0.7
78	13.0	-0.1
7	10.6	8.9
6	8.2	4.7
7	6.6	6.3
bl	6.5	6.4
SL	7.5	5.4

W & L of Abbot

SL	6.7	6.2
bl	6.7	6.2
7	6.5	6.4
6	6.9	6.0
7	8.9	4.0
bl	10.6	2.3
SL	11.0	1.9

W 1/4 of Abbot

SL	10.3	2.6
bl	9.8	3.1
7	7.4	5.5
6	6.7	6.2
7	6.3	6.6
bl	6.7	6.2
SL	6.5	6.4

1293

Newport St

center of Abbot

SL	6.5	6.4
bl	6.5	6.4
7	6.3	6.6
6	6.7	6.2
7	7.1	5.8
bl	8.9	4.0
SL	9.5	3.4

E 1/4 of Abbot St

SL	9.3	3.6
bl	8.5	4.4
7	6.7	6.2
6	6.5	6.4
7	6.4	6.5
bl	6.6	6.3
SL	6.7	6.2

E 1/4 of Abbot St

SL	7.1	5.8
bl	6.6	6.3
7	8.4	6.5
6	6.3	6.6
7	6.7	6.2
bl	8.3	4.6
SL	9.0	3.9



1293

E 1 of Abbot st

SL	9.1	3.8
H <sup>+3</sup>	7.3	5.1
H	7.0	5.9
Y	6.5	6.4
L	6.2	6.7
Y	6.2	6.7
H	6.8	6.1
SL	7.4	5.5

35' E of Abbot

SL	8.0	4.9
H	6.2	6.7
Y	6.1	6.8
L	5.6	7.3
Y	5.6	7.3
H	6.2	6.7
SL	6.4	6.5

50' E of Abbot

SL	8.9	4.0
H	8.5	4.4
H <sup>36</sup>	8.2	4.7
H <sup>38</sup>	8.8	7.1
Y	5.6	7.3
L	5.2	7.9
Y	6.0	6.9
H	6.3	6.6
SL	7.0	5.9

1293

Newport st

60' E of Abbot st

SL	6.9	6.0
H	6.0	6.9
Y	5.7	7.2
L	5.0	7.9
Y	5.2	7.3
H <sup>+3</sup>	8.0	4.9
H <sup>77</sup>	8.2	4.7
H <sup>710</sup>	6.5	6.4
H	6.0	6.9
SL	6.4	6.5

100' E of Abbot st

SL	4.4	8.5
H	4.9	8.0
H <sup>71</sup>	7.0	5.9
H <sup>77</sup>	7.4	5.5
H <sup>78</sup>	5.2	7.3
H <sup>14</sup>	5.4	7.5
L	4.5	8.4
Y	5.2	7.7
H	5.2	7.7
SL	4.7	8.2

150' E of Abbot

SL	4.1	8.8
H	5.0	7.9
Y	5.0	7.9
L	4.4	7.5
Y	4.6	8.3
H <sup>73</sup>	4.8	8.1
H <sup>78</sup>	6.3	6.6
H <sup>50</sup>	7.9	7.9
SL	2.2	10.7



1293

156' E of abbot (in Alley brook)

52	4.0	8.9
bl	4.7	8.2
+3'	5.0	7.9
+4'	6.2	6.7
+9'	4.9	8.0
1/4	4.6	8.3

200' E of abbot st

52	3.8	9.1
bl	4.6	8.3
+4'	5.4	7.5
4	4.7	8.2
4	4.1	8.8
4	4.8	8.1
bl	4.8	8.1
22	4.8	8.1

250' E of abbot st

22	5.2	7.7
bl	5.2	7.7
4	4.6	8.3
6	4.2	8.7
7	4.5	8.4
bl	4.9	8.0
52	4.4	8.5

1293

Newport st

300' E of Abbot st

52	4.7	8.2
bl	4.5	8.4
4	4.4	8.5
4	4.0	8.9
4	4.6	8.3
bl	5.0	7.9
22	5.1	7.8

350' E of Abbot

22	7.8	8.1
bl	4.6	8.3
4	4.1	8.8
4	3.7	9.2
4	4.1	8.8
bl	4.4	8.5
52	4.3	8.6

672 16.14 375 91.8

400' E of Abbot st

52	6.5	9.6
bl	7.2	8.9
4	6.7	9.4
6	6.6	9.5
4	6.9	9.2
bl	7.2	8.9
22	7.4	8.7



1614

450' E of abbot st

SL	67	9.4
ll	66	9.5
y	62	9.9
h	60	10.1
y	63	9.8
ll	70	9.1
SL	62	9.9

500' E of abbot st

SL	57	10.4
ll	62	9.9
y	54	10.7
h	54	10.7
y	58	10.3
ll	61	10.0
SL	60	10.1

530' E of abbot st

SL	49	11.2
ll	57	10.4
y	50	11.1
h	48	11.3
y	50	11.1
ll	55	10.6
SL	46	11.5

1614

new part st

600' E of NW 2 of Baem st (60')

SL	46	11.5
ll	45	11.6
y	45	11.6
h	42	11.9
y	45	11.6
ll	50	11.1
SL	44	11.7

NW 1/4 of Baem st

SL	46	11.5
ll	44	11.7
y	43	11.8
h	40	12.1
y	43	11.8
ll	44	11.7
SL	45	11.6

NW 1/4 of Baem st

SL	44	11.7
ll	42	11.9
y	42	11.9
h	38	12.3
y	40	12.1
ll	43	11.8
SL	42	11.8



1614

Center of Bacon st

22	40	12.1
22	41	12.0
7	38	12.3
6	38	12.3
7	40	12.1
22	41	12.0
52	42	11.9

Center + 1' = 2' W of RR Rail

52	42	11.9
22	41	12.0
7	40	12.1
6	38	12.3
7	38	12.3
22	41	12.0
22	40	12.1

Elevation of Rail

52	375	12.4
6	380	12.3
22	390	12.2

E 1/4 = 2' E of Rail

22

1614

New part 24

6

E 1/4 = 2' E of Rail

22	42	11.9
22	41	12.0
4	39	12.2
6	38	12.3
7	38	12.3
22	39	12.2
52	40	12.1

E of Bacon st

52	36	12.5
22	37	12.4
7	38	12.3
6	35	12.6
7	38	12.3
22	38	12.3
22	41	12.0

E line of Bacon st

22	35	12.6
22	35	12.6
7	38	12.3
6	34	12.7
7	38	12.3
22	40	12.1
52	37	12.7

TP

738 19.65

389

12.2

72 32



19.65

50' E of Baum st

SL	6.0	13.6
ll	$\begin{matrix} 6.2 \\ 2.1 \end{matrix}$	$\begin{matrix} 13.4 \\ 12.5 \end{matrix}$
y	6.4	13.2
b	6.1	13.5
y	6.5	13.1
ll	$\begin{matrix} 6.2 \\ 6.8 \end{matrix}$	$\begin{matrix} 13.4 \\ 12.8 \end{matrix}$
SL	6.4	13.2

100' E of Baum st

SL	6.0	13.6
ll	$\begin{matrix} 6.2 \\ 7.0 \end{matrix}$	$\begin{matrix} 13.4 \\ 12.6 \end{matrix}$
y	6.0	13.6
b	5.7	13.9
y	5.8	13.8
ll	$\begin{matrix} 6.5 \\ 5.7 \end{matrix}$	$\begin{matrix} 13.1 \\ 13.9 \end{matrix}$
SL	5.6	14.0

150' E of Baum st

SL	5.4	14.2
ll	$\begin{matrix} 5.7 \\ 6.3 \end{matrix}$	$\begin{matrix} 13.9 \\ 13.3 \end{matrix}$
y	5.5	14.1
b	5.3	14.3
y	5.6	14.0
ll	$\begin{matrix} 6.1 \\ 5.5 \end{matrix}$	$\begin{matrix} 13.5 \\ 14.1 \end{matrix}$
SL	5.7	13.9

19.65

Newport st

(200') E of Baum st

SL	5.5	14.1
ll	5.9	13.7
y	5.2	13.4
b	4.9	14.7
y	5.0	14.6
ll	$\begin{matrix} 5.7 \\ 5.1 \end{matrix}$	$\begin{matrix} 13.9 \\ 14.5 \end{matrix}$
SL	5.0	14.6

250' E of Baum st

SL	4.6	15.0
ll	$\begin{matrix} 5.0 \\ 5.3 \end{matrix}$	$\begin{matrix} 14.6 \\ 14.1 \end{matrix}$
y	4.8	14.8
b	4.4	15.2
y	4.8	14.8
ll	$\begin{matrix} 5.5 \\ 4.8 \end{matrix}$	$\begin{matrix} 13.1 \\ 14.8 \end{matrix}$
SL	5.4	14.2

300' E of Baum st

SL	5.0	14.6
ll	$\begin{matrix} 4.6 \\ 5.2 \end{matrix}$	$\begin{matrix} 15.0 \\ 14.4 \end{matrix}$
y	4.4	15.2
b	4.0	15.6
y	4.7	15.2
ll	$\begin{matrix} 5.0 \\ 4.3 \end{matrix}$	$\begin{matrix} 14.6 \\ 15.1 \end{matrix}$
SL	4.5	15.1



1965

	350'	E of	Bacon	W
SL			39	13.7
ll			(42) 46	15.4 15.0
γ			42	15.4
δ			38	13.8
γ			42	15.3
ll			(50) 43	14.6 15.1
nL			47	14.9

	400'	E of	Bacon	W
nL			43	15.3
ll			(41) 47	15.5 14.9
γ			39	15.7
δ			34	15.2
γ			40	15.6
ll			(44) 39	15.2 15.7
SL			38	13.8

	450'	E of	Bacon	W
SL			33	16.3
ll			(30) 40	16.6 15.6
γ			34	16.2
δ			31	16.5
γ			34	16.2
ll			(42) 36	15.4 16.0
nL			38	15.8
TP	633	2299	299	16.66

2299

Newport St

	500'	E of	Bacon	W
nL			68	16.2
ll			(66) 72	16.4 15.8
γ			64	16.6
δ			60	17.0
γ			63	16.7
ll			(70) 64	16.0 16.6
SL			67	16.8

	550'	E of	Bacon	W
SL			55	17.5
ll			(58) 65	17.2 16.5
γ			59	17.1
δ			56	17.4
γ			59	17.1
ll			(66) 58	16.4 17.2
nL			59	17.1

	600'	E = W of	Cabb	W (60')
nL			61	16.9
ll			(57) 62	17.3 16.8
γ			56	17.4
δ			50	18.0
γ			54	17.6
ll			(60) 55	17.0 17.5
SL			56	17.4



22.99

## W 1/4 of ball st

S2	55	17.5
bl	(55) 54	17.5 17.2
4	54	17.6
6	50	18.0
7	54	17.6
ll	(61) 53	16.9 17.5
N2	53	17.5

## W 1/4 of ball st

N2	57	17.4
bl	(57) 60	17.4 17.0
4	53	17.1
6	50	18.0
7	54	17.6
ll	(58) 52	17.2 17.8
S2	51	17.9

## center of ball st

S2	50	18.0
bl	(53) 55	17.7 17.5
4	53	17.7
6	49	18.1
7	52	17.8
ll	(60) 52	17.0 17.4
N2	53	17.5

22.99

New part

9

## E 1/4 of ball st

N2	54	17.6
bl	(48) 58	18.2 17.2
4	51	17.9
6	48	18.2
7	52	17.8
ll	(57) 48	17.3 18.2
S2	49	18.1

## E 1/4 of ball st

S2	50	18.0
bl	(50) 55	18.0 17.5
4	52	17.8
6	47	18.3
7	50	18.0
ll	(57) 52	17.3 17.8
N2	53	17.7

## E line of ball st

N2	54	17.6
bl	(51) 56	17.9 17.4
4	47	18.1
6	46	18.4
7	50	18.0
ll	(54) 46	17.6 18.4
S2	50	18.0



2299

	50	E of	babb st	
SL			4.5	18.5
lh			(4.4)	18.6
			(3.0)	18.0
y			4.6	18.4
b			4.2	18.2
y			4.6	18.4
lh			(5.1)	17.9
			(4.4)	18.4
nl			4.7	18.3

	100	E of	babb st	
nl			4.2	18.8
lh			(4.3)	18.7
			(4.2)	18.4
y			4.1	18.9
b			3.5	19.5
y			4.1	18.9
lh			(4.6)	18.4
			(3.3)	19.5
SL			4.0	19.0

	150	E of	babb st	
SL			3.8	19.2
lh			(3.7)	19.3
			(4.1)	18.9
y			3.4	19.6
b			3.0	20
y			3.5	19.5
lh			(4.1)	18.9
			(3.4)	19.6
nl			3.7	19.6

2299

New part of

10

	200	E of	babb st	
SL			3.0	20.0
lh			(2.7)	20.3
			(3.5)	19.5
y			2.8	20.2
b			2.4	20.6
y			3.0	20.0
lh			(3.5)	19.5
			(2.8)	20.2
nl			3.1	19.9

	250	E of	babb st	
nl			2.6	20.4
lh			(2.4)	20.6
			(3.0)	20.0
y			2.3	20.7
b			1.8	21.2
y			2.3	20.7
lh			(2.7)	20.3
			(2.4)	20.6
SL			2.3	20.7

	TP	7.31	28.98	1.82	21.17

	300	E of	babb st	
SL			7.1	21.4
lh			(7.0)	21.5
			(7.6)	20.9
y			7.0	21.5
b			6.7	21.8
y			6.8	21.7
lh			(7.7)	20.8
			(7.2)	21.3
nl			7.2	21.3



2848

	350	E of	babb st	
nl			65	22.0
lh			(63) 72	22.2 21.3
y			62	22.2
b			58	22.7
y			64	22.1
lh			(70) 62	21.5 22.3
sl			62	22.3

	400	E of	babb st	
sl			57	22.8
lh			(56) 62	22.9 22.3
y			58	22.1
b			51	23.4
y			57	22.8
lh			(63) 57	22.2 22.8
nd			61	22.4

	450	E of	babb st	
nl			53	23.2
lh			(52) 58	23.3 22.7
y			51	23.4
b			46	23.9
y			51	23.4
lh			(57) 48	22.8 23.7
sl			50	23.5
TP	689	<u>3196</u>	341	25.07

39.96

Newport: 25

11

	500	E of	babb st	
nl			82	23.8
lh			(82) 87	23.8 23.3
y			82	23.8
b			75	24.5
y			80	24.0
lh			(85) 88	23.5 24.2
sl			79	24.1

	550'	E of	babb st	
sl			73	24.7
lh			(72) 79	24.8 24.1
y			74	24.6
b			68	25.2
y			73	24.7
lh			(80) 74	24.0 24.6
nl			74	24.6

	600	E = W of	D. J. st (60')	
nl			69	25.1
lh			(70) 74	25.0 24.6
y			66	25.4
b			60	26.0
y			66	25.4
sl			71	24.9
sl			66	25.4
			66	25.4



31.96

W. 1/4 of D. 7 or 11

SE	63	25.7
SW	(62) 70	25.8 25.0
4	64	25.6
6	59	26.1
7	66	25.4
8	(72) 65	24.8 25.5
9	67	25.3

W. 1/4 of D. 7 or 11

12	67	25.3
13	(65) 71	25.5 24.9
4	64	25.6
6	57	26.3
7	63	25.7
8	(67) 61	25.3 25.9
9	58	26.2

Center of D. 7 or 11

SE	61	25.9
SW	(62) 62	25.8 25.4
4	61	25.9
6	56	26.4
7	62	25.8
8	(69) 65	25.1 25.5
9	67	25.3

31.96

Newport 11

12

E. 1/4 of D. 7 or 11

12	63	25.7
13	(65) 67	25.5 25.3
4	61	25.9
6	55	26.5
7	60	26.0
8	(65) 59	25.5 26.1
9	58	26.2

E. 1/4 of D. 7 or 11

SE	56	26.4
SW	(56) 63	26.4 25.7
4	58	26.2
6	53	26.7
7	59	26.1
8	(66) 52	25.4 26.4
9	60	26.0

E. line of D. 7 or 11

12	60	26.0
13	(58) 64	26.2 25.6
4	52	26.8
6	57	26.3
7	(61) 56	25.9 26.8
8	55	26.5



31.96

	50' E of	De	Fae	at
SL		48		27.2
hh		44		27.6
γ		(55)		26.5
γ		49		27.1
b		45		27.5
γ		51		26.9
hh		(55)		26.5
ηλ		(50)		27.0
		50		27.0

	100' E of	De	Fae	at
ηλ		38		28.2
hh		40		28.0
γ		(46)		27.4
γ		40		28.0
b		35		28.5
γ		40		28.0
hh		46		27.4
		(38)		28.2
SL		41		27.9

	150' E of	De	Fae	at
SL		26		29.4
hh		(31)		28.9
γ		(37)		28.3
γ		30		29.0
b		25		29.5
γ		29		29.1
hh		(36)		28.4
		(27)		29.3
ηλ		31		28.9

31.96

Newport st

	200' E of	De	Fae	at
ηλ		20		30.0
hh		(18)		30.2
γ		(24)		29.6
γ		18		30.2
b		13		30.7
γ		18		30.2
hh		26		29.4
		(19)		30.1
SL		22		29.8

	TP	1203	42.25	
		174		30.22

	250' E of	De	Fae	at
SL		112		31.1
hh		(110)		31.3
γ		(117)		30.6
γ		108		31.5
b		103		32.0
γ		106		31.7
hh		(115)		30.8
		(107)		31.6
ηλ		110		31.3

	300' E of	De	Fae	at
ηλ		94		32.9
hh		96		32.7
		(102)		32.1
γ		94		32.9
b		90		33.3
γ		97		32.6
hh		(105)		31.8
		(99)		32.4
SL		102		32.1

13



42.25

	350'	EJ	De	7m	21
SL			87		33.6
hh			(84)		33.9
			(90)		33.0
y			86		33.7
b			80		34.3
y			82		34.1
hh			(87)		33.6
			(76)		34.7
nl			82		34.1

	400'	EJ	De	7m	21
nl			67		35.6
hh			(67)		35.6
			(73)		35.0
y			70		35.3
b			67		35.6
y			70		35.3
hh			(78)		34.5
			(70)		35.3
SL			74		34.9

	450'	EJ	De	7m	21
SL			59		36.4
hh			(53)		36.8
			(60)		36.3
y			52		37.1
b			47		37.6
y			50		37.3
hh			(56)		36.7
			(52)		37.1
nl			50		37.3

42.25

New part 11

14

	500'	E	De	7m	21
nl			25		39.8
hh			(27)		39.6
			(38)		38.5
y			28		39.5
b			24		39.9
y			31		39.2
hh			40		38.3
			32		39.1
SL			37		38.6

11.88 53.60 053 4172

	550'	EJ	De	7m	21
SL			124		41.2
hh			(119)		41.7
			(130)		40.6
y			119		41.7
b			110		42.6
y			117		41.9
hh			(132)		40.4
			(121)		41.5
nl			112		42.4

600' E = W line of Eberste et (60)

nl			89		44.7
hh			(95)		44.1
			(109)		43.7
y			92		44.4
b			86		45.0
y			93		44.3
hh			(104)		43.2
			(97)		43.9
SL			96		44.0



5360

W 1/4 of Eber st

SL	9.0	44.6
ll	(8.7)	44.9
γ	8.7	43.6
δ	8.0	44.9
ε	8.0	45.6
ζ	8.6	45.0
η	9.0	44.6
θ	10.2	43.4
ι	9.0	44.6
κ	8.3	45.3

W 1/4 of Eber st

κ	7.9	45.7
ll	(8.5)	45.1
γ	(9.5)	44.1
δ	8.0	45.6
ε	7.5	46.1
ζ	8.2	45.4
η	(9.2)	44.4
θ	(8.3)	45.1
SL	8.4	45.2

Center of Eber st

SL	7.7	45.9
ll	(7.7)	45.9
γ	(8.9)	44.7
δ	7.5	46.1
ε	6.9	46.9
ζ	7.5	46.1
η	(8.7)	44.9
θ	(8.0)	45.6
ι	7.3	46.3

5360

Newport st

15

E 1/4 of

Eber st

κ	6.7	46.9
ll	(7.3)	46.3
γ	(8.0)	45.6
δ	6.7	46.7
ε	6.4	47.2
ζ	7.0	46.6
η	(8.3)	45.3
θ	(7.5)	46.1
SL	7.4	46.2

E 1/4 of

Eber st

SL	6.6	47.0
ll	(6.8)	46.8
γ	(7.7)	45.9
δ	6.3	47.3
ε	5.7	47.9
ζ	6.3	47.3
η	(7.2)	46.4
θ	(6.4)	47.2
ι	6.2	47.4

E line of

Eber st

κ	5.7	47.9
ll	6.0	47.6
γ	(6.7)	46.9
δ	5.7	47.9
ε	5.1	48.5
ζ	5.8	47.8
η	(7.0)	46.6
θ	(6.0)	47.6
SL	6.0	47.6



53.6

	50	E of	Eber	
SL			2.7	50.9
hh			(2.6)	51.0
f			(5.3)	50.3
b			2.2	51.4
y			1.6	52.0
y			2.2	51.4
hh			(2.9)	50.7
hh			(2.0)	51.0
hh			2.4	51.2
TP	12.44	<u>64.24</u>	1.80	51.80
	100	E of	Eber St	
SL			9.7	54.5
hh			9.4	54.8
y			8.7	55.3
b			8.5	55.4
y			8.9	55.3
hh			9.4	54.8
SL			8.8	55.4
	150	E of	Eber St	
SL			4.9	59.3
hh			4.9	59.3
y			4.1	60.1
b			3.7	60.5
y			4.3	59.9
hh			5.3	58.9
SL			6.1	58.1

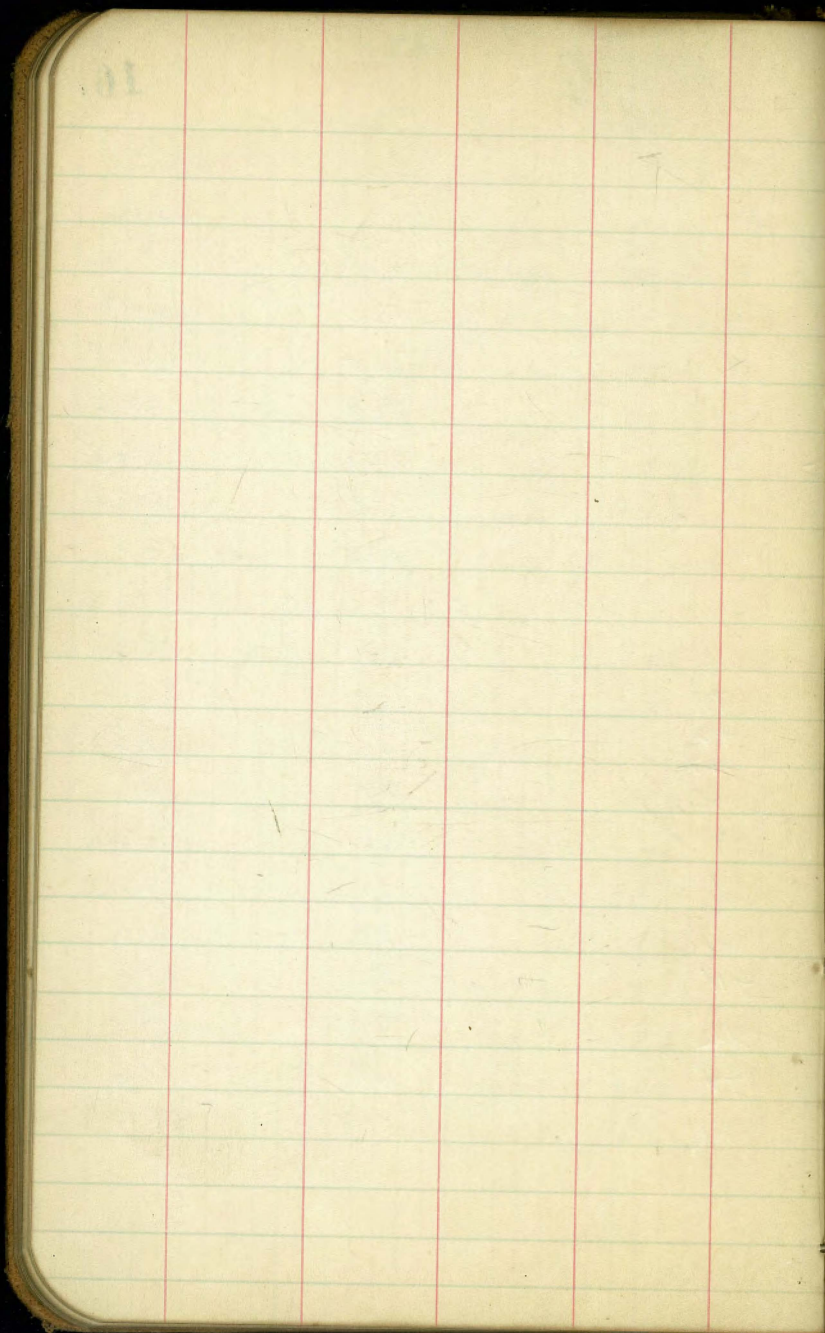
64.24

New part of

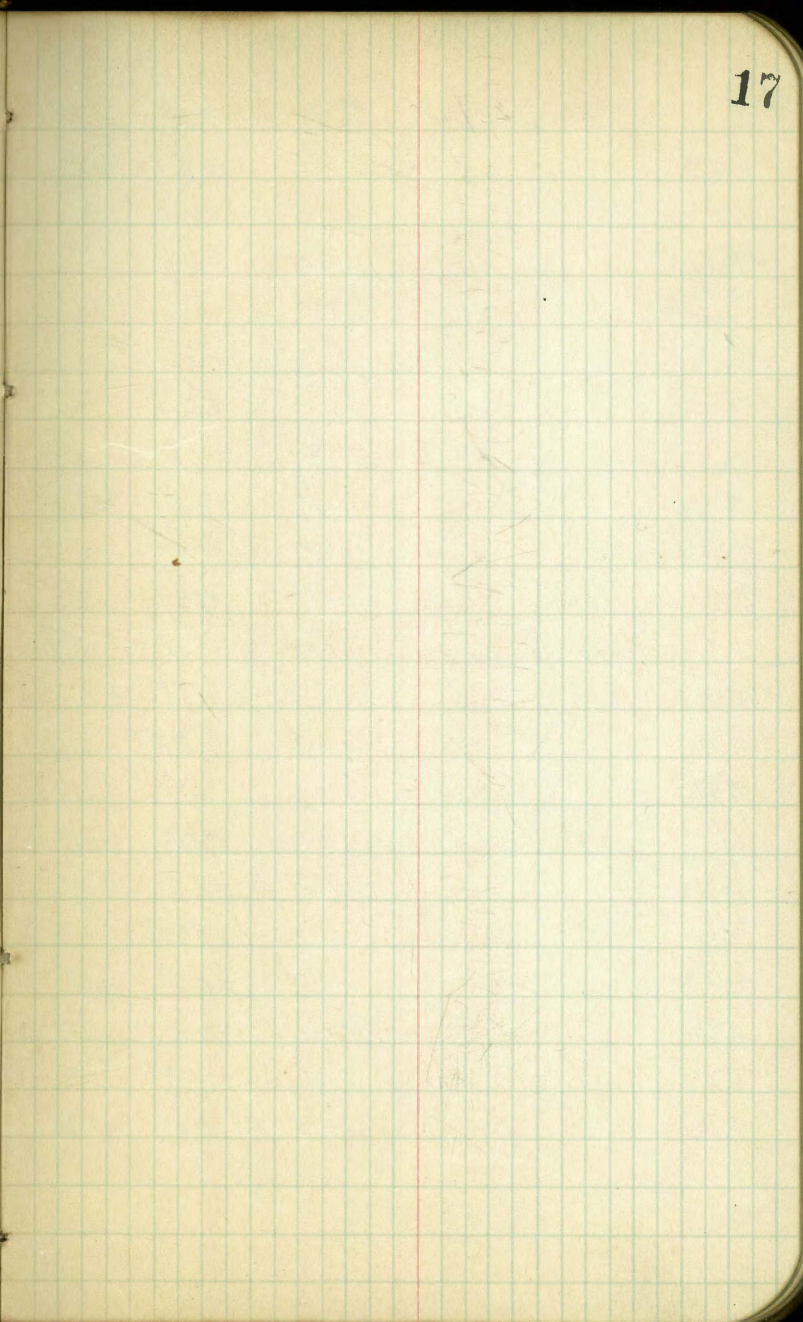
16

	200	E of	Eber St	
SL			2.2	62.0
hh			0.7	63.5
TP	12.77	<u>77.01</u>	0.0	64.24
y			12.3	64.7
b			11.5	65.5
y			11.8	65.2
hh			12.7	64.3
hh			13.2	63.4
SL			13.1	63.9
	250	E of	Eber St	
SL			8.8	68.2
hh			10.2	66.8
+6'			10.0	67.0
+7'			9.0	68.0
hh			7.9	69.1
y			6.6	70.4
b			6.7	70.3
y			7.4	69.6
+11'			8.4	68.6
hh			9.7	67.3
+12'			10.4	66.6
SL			11.8	65.2





16



17



77.01

	300'	E of	Eber St	
nL			75	69.5
+10			6.5	70.5
ll			4.0	73.0
+1'			3.4	73.6
1/4			2.4	74.6
6			1.5	75.5
4			1.8	75.3
ll			2.5	74.5
+4'			4.2	72.8
SL			4.1	72.9

TP	1297	<u>89.61</u>	0.37	76.64
	350	E of	Eber St	
SL			12.1	77.5
+11'			13.3	76.3
ll			10.1	79.5
4			9.5	80.1
6			9.2	80.4
4			10.0	79.6
ll			11.6	78.0
+4'			14.7	74.9
nL			15.5	74.1

89.61

New part

**18**

	400'	E of	Eber St	
nL			10.6	79.0
At 10'			9.4	80.2
ll			6.0	83.6
4			5.2	84.4
6			4.5	85.1
4			4.8	84.8
ll			5.3	84.3
+4'			8.2	81.7
+8'			8.8	80.8
SL			7.7	81.9
	450'	E of	Eber St	
SL			0.1	89.5
ll			1.4	88.2
+2'			0.3	89.3
TP	1273	<u>101.85</u>	0.49	89.12
1/4			12.1	89.8
6			11.8	90.1
4			12.4	89.3
ll			13.3	88.6
+5'			16.4	85.5
nL			16.7	85.2



		16185		
500'	E of	Eber St		
22		9.0	92.9	
62		7.8	94.1	
7		7.5	94.4	
6		6.8	95.1	
7		7.1	94.8	
+11'		8.0	93.9	
66		6.4	95.5	
SR		6.0	95.9	
550'	E of	Eber St		
SR		1.5	100.4	
66		1.8	100.1	
+3'		3.3	98.6	
4		2.5	99.4	
6		2.2	99.7	
4		2.5	99.4	
66		3.0	98.9	
+3'		1.6	100.3	
22		1.9	100	
TR	11.47	<u>113.15</u>	0.17	101.68

		113.15	New part of	
600'	E =	W side of	Fraude St	(60)
22		8.6	104.6	
112'		8.8	104.4	
66		9.7	103.5	
+4'		10.1	103.1	
114		9.5	103.7	
6		8.7	104.3	
7		9.4	103.8	
66		9.7	103.3	
+2'		8.0	105.2	
SR		7.3	105.9	
	W side of	Fraude St		
SR		6.5	106.7	
+2'		7.0	106.2	
66		8.4	104.8	
+2'		9.4	103.8	
7		8.8	104.4	
6		8.3	104.9	
7		8.7	104.3	
+9'		9.5	103.7	
66		8.8	104.4	
SR		7.5	105.7	



113.15

W 1/4 of Franck St

SL	6.8	106.4
tlr	6.8	106.4
tl	8.6	104.6
7	8.3	104.9
l	7.8	105.4
7	8.2	105.1
711	8.6	104.6
tl	6.5	106.7
tr	5.5	107.7
SL	4.9	108.3
center of Franck		
SL	4.0	109.2
tl	(5.0)	108.2
7	(7.8)	105.4
7	7.6	105.6
l	7.2	106.0
7	7.8	105.4
tl	8.1	105.1
tr	5.6	107.6
SL	6.3	106.9

113.15

Newport St

20

E 1/4 of Franck St

SL	6.0	107.2
tlr	5.3	107.9
tl	7.4	105.8
7	7.4	106.0
l	6.7	106.5
7	7.0	106.2
71r	7.2	106.0
tl	4.2	109.0
SL	3.2	110.0
E tl of Franck St		
SL	1.8	111.4
tl	3.2	110.0
tl	6.8	106.4
7	6.5	106.7
l	6.2	107.0
7	6.7	106.5
tl	7.0	106.0
7r	5.1	108.1
SL	5.2	107.6



11315

	E Line of		Fraude st	
nl			5.2	108.0
+iv			4.0	109.2
bb			6.3	106.9
4			6.0	107.2
6			5.6	107.6
4			5.9	107.3
+iv			6.2	107.1
bb			2.4	110.8
SP	862	<u>121.77</u>	0.0	113.15
SA			9.0	112.8
	50'	E of	Fraude	
SA			3.9	117.9
bb			5.9	115.9
+v			11.6	110.2
4			11.0	110.8
6			11.9	110.9
4			11.4	110.4
bb			(11.9)	109.9
Adin			7.0	114.8
			7.4	114.4

12177

Newport st

21

	100'	E of	Fraude st	
nl			1.1	120.7
ll			0.5	121.3
+i			8.2	113.6
4			7.0	114.8
6			6.3	115.5
4			6.4	115.4
+9			7.0	114.8
+iii			5.9	116.1
	11.60	<u>132.67</u>	0.70	121.07
bb			9.4	123.3
SA			8.4	124.3
	150'	E of	Fraude st	
SA			2.4	130.3
ll			3.5	129.2
+v			12.6	120.1
4			12.4	120.3
6			12.4	120.5
4			13.0	119.7
bb			13.4	119.3
+6			7.0	125.7
nl			7.4	125.3



132.67

175'	E of	Traverse	St
72		5.1	127.6
bb		(5.0)	125.7
		(11.0)	121.7
74		11.7	122.0
6		10.0	122.8
7		10.2	122.5
+10'		10.7	122.0
bb		8.0	124.7
+1'		1.0	131.7
SL		+0.4	132.6

185'	E of	Traverse	St
BL		+2.6	135.3
ll		9.7	123.0
7		9.2	123.5
6		8.9	123.8
7		9.6	123.1
ll		(10.0)	122.7
		(4.0)	128.7
72		4.5	128.2

132.67

Newport St

22

200'	E of	Traverse	St
72		3.0	129.7
bb		(3.0)	129.7
		(8.6)	124.1
7		8.0	124.7
6		7.3	125.5
7		7.7	125.0
bb		8.2	124.5
+8'		6.8	125.9
TP	1244	14348	1.63
			131.04
+11'		7.0	136.5
SL		6.8	136.7

250'	E of	Traverse	St
SL		1.1	142.4
+2'		1.1	142.4
+6'		13.6	130.0
ll		13.7	129.8
76		13.2	130.3
7		13.0	130.5
6		12.7	130.8
7		13.3	130.2
ll		(14.1)	129.4
		(5.2)	138.3
72		4.6	138.9
TP	583	14832	0.99
			142.79



SS

		<u>148.02</u>	
300' E of		Fraude St	
SL		2.0	146.3
+2'		2.2	146.1
+5'		13.4	134.7
bb		13.4	134.9
y		12.7	135.6
b		12.6	135.7
y		13.3	135.0
bb		14.4	133.9
+1'		4.5	143.8
nl		5.0	143.3
TP	5.95	<u>152.64</u>	1.63 146.69
350' E of		Fraude St	
SL		1.9	150.7
+2'		1.9	150.7
+5'		12.2	140.4
bb		12.8	139.8
y		12.3	140.3
b		12.0	140.6
y		12.7	139.9
+11'		13.3	139.3
bb		5.7	146.9
+4'		4.4	148.2
		4.6	148.0

152.64

Newport St

23

		<u>152.64</u>	
400' E of		Fraude St	
nl		2.4	150.2
bb		1.5	151.1
+1'		2.0	143.6
y		8.1	144.5
b		7.4	144.2
y		7.8	144.8
bb		7.8	144.8
+7'		7.7	144.9
TP	6.53	<u>158.24</u>	0.93 151.71
+11'		2.2	156.0
SL		2.1	156.1
410' E of		Fraude St	
SL		1.5	156.7
bb		2.5	155.7
+2'		13.2	145.0
y		12.5	145.7
b		12.1	146.1
y		12.7	145.5
+12'		13.2	144.3
bb		7.4	150.8
nl		8.5	149.7



		158.24		
		425'	E of	Fraude St
nl			9.0	149.2
bh			(7.6)	150.4
			(11.9)	146.3
y			11.2	147.0
b			10.6	147.6
y			11.1	147.1
+11'			11.7	146.5
bh			2.0	156.0
SL			0.7	157.5
TP	480	161.44	1.60	152.64
		445'	E of	Fraude St
SL			2.0	157.4
bh			3.3	158.1
+1'			3.3	158.1
+3'			12.9	148.5
y			12.8	148.6
b			12.1	149.3
y			12.7	148.7
bh			13.3	148.1
+2'			9.2	152.2
nl			10.5	150.9

		161.44	Newport St	
		450'	E of	Fraude St
nl			9.9	157.5
bh			(8.7)	152.7
			(12.7)	148.7
y			12.3	149.1
b			11.6	149.8
y			12.0	149.4
+11'			12.3	149.1
bh			11.0	150.4
+7'			1.8	160.6
SL			1.4	160.0
TP	751	167.27	1.68	159.76
		500'	E of	Fraude St
SL			0.0	167.3
+6'			12.8	154.5
bh			13.3	154.0
y			13.0	154.3
b			12.7	154.6
y			13.2	154.1
nl			14.0	153.3
			8.6	158.7
+1'				
nl			10.3	157.0



		167.27		
	550	E of	Tronde	st
R2			94	157.9
bb			57	161.6
+1'			84	158.9
y			81	159.2
b			80	159.3
y			82	159.1
bb			88	158.5
+8'			3.1	164.2
TP	9.61	<u>174.82</u>	006	167.21
+12'			2.8	174.0
SA			2.8	174.0
	575	E of	Tronde	
SR			2.0	174.8
+12'			4.5	172.3
TP	0.60	<u>174.57</u>	2.85	173.97
bb			122	162.4
+4			141	160.5
1/4			136	161.0
b			130	161.6
y			132	161.4
bb			136	161.0
+2'			130	161.6
R2			16.9	157.7

		174.57		
	600'	E = W in	Gungot	(60)
				25
				(Diameter offsets 2 1/2" to 3 1/2")
R2			17.3	157.3
bb			122	162.4
+2'			117	162.9
y			117	162.9
b			11.5	163.1
y			11.9	162.7
+11'			123	162.3
bb			3.9	170.7
SR			0.8	173.8
				W side of
				Gungot st
SR			1.9	172.7
+12'			4.7	
bb			5.6	
+3'			11.8	
y			11.4	
b			11.1	173.5
y			11.3	
+12'			11.6	
bb			12.0	
R2			16.2	158.4



174.57

E 1/4 of Gungot st

nl	142	
lh	11.6	
1/4	11.1	
b	10.9	
1/4	11.0	
+11	11.5	
lh	5.9	
sl	2.4	
center of Gungot st		
sl	2.8	171.8
lh	7.0	
+1	11.2	
1/4	10.6	
b	10.5	164.1
1/4	10.9	
lh	11.2	
nl	13.0	161.6

174.57

Newport st

E 1/4 of Gungot st

26

nl	12.7
lh	11.0
1/4	10.7
b	10.3
1/4	10.4
+10	10.8
lh	7.6
sl	3.5
E 1/4 of Gungot st	
sl	4.1
lh	9.2
+2	10.3
1/4	10.0
b	10.1
1/4	10.6
lh	10.9
nl	12.5



17457

✓ to man Santa Barbara

E line of Surget st

32	104	164.2
bl	105	
4	105	
6	100	164.6
4	9.6	
+10'	100	
bl	9.1	
52	5.4	169.2

27







6191

75°E 2<sup>d</sup>

No Gutr	5.2	56.7
Cl	4.7	57.2
No	3.9	58.0

100°E 2<sup>d</sup>

No	3.5	58.4
Cl	4.1	57.8
Gutr	4.8	57.1
5'	4.5	57.4
$\frac{1}{2}$	4.1	
0	3.9	58.0
$\frac{1}{4}$	4.4	
5'	4.9	57.0
Gutr	5.2	56.7
Cl	4.7	57.2
So	4.5	57.4

120°E 2<sup>d</sup>

So	3.7	58.2
Cl	4.0	57.9
Gutr	4.5	57.4
5'	4.3	57.6
$\frac{1}{2}$	3.8	
0	3.2	58.7
$\frac{1}{4}$	3.6	
5'	3.9	58.0
Gutr	4.3	57.6
Cl	3.7	58.5
No	3.1	58.8

29

150°E 2<sup>d</sup>

No	2.2	59.7
Cl	2.8	59.1
Gutr	2.6	58.3
5'	3.1	58.8
$\frac{1}{2}$	2.1	59.1
0	2.7	59.2
$\frac{1}{4}$	3.2	
5'	2.6	58.3
Gutr	3.8	58.1
Cl	3.3	58.6
So	3.1	58.8

175°E 2<sup>d</sup>

So	2.4	59.5
Cl	2.6	59.3
Gutr	3.1	58.8
5'	2.9	59.0
$\frac{1}{2}$	2.5	
0	2.2	59.7
$\frac{1}{4}$	2.3	
5'	2.4	59.5
Gutr	2.7	59.2
Cl	2.1	59.8
No	1.4	60.5



6191  
 300' E 2d - W.L. 3d

No.	1.2	60.7
Ch	1.5	60.4
Center	2.1	59.8
5'	1.9	60.0
2	1.7	
6	1.8	60.1
2	2.1	
5'	2.5	59.4
Center	2.5	59.4
Ch	1.9	60.0
So.	1.8	60.1

5.05      64.78      2.18      59.73

E.L. 3d

So.	4.2	60.6
Ch	4.4	60.4
Center	5.0	59.8
5'	4.9	59.9
2	4.7	
6	4.3	60.5
2	4.2	
5	4.2	60.6
Center	4.1	60.7
Ch	3.8	61.0
No.	3.5	61.3

25' E 3d

No.	3.5	61.3
Ch	3.9	60.9
Center	4.4	60.4
5'	4.1	60.4
2	4.4	
6	4.3	60.5
2	4.6	
5	5.2	59.6
Center	5.3	59.5
Ch	4.7	60.1
So.	4.7	60.1

53' E 3d

So.	4.6	60.2
Ch	4.9	59.9
Center	5.4	59.4
5'	5.3	59.5
2	4.8	
6	4.5	60.3
2	4.5	
5'	4.5	60.3
Center	4.5	60.3
Ch	4.2	60.8
No.	3.5	61.3



28

60.70

75° E 30°

No.	38	61.0
ct	41	60.7
Center	46	60.2
5'	47	60.1
4'	47	
0	47	60.1
1/4	50	
5'	55	59.3
Center	57	59.1
ct	52	59.6
S.	48	60.0
100° E 30°		
S.	50	59.8
ct	53	59.5
Center	57	58.9
5'	57	59.1
1/4	51	
0	49	59.9
1/4	47	
5'	47	60.1
Center	48	60.0
ct	47	60.7
N.	36	61.2

31

125° E 30°

N.	2.2	62.6
ct	3.9	60.9
ct	4.2	60.6
Center	4.9	59.9
5'	4.9	59.9
1/2	4.8	
0	5.0	59.8
1/4	5.6	
5'	6.0	59.8
Center	6.2	58.6
ct	5.5	59.3
S.	5.2	59.6
150° E 30°		
S.	5.4	59.4
ct	5.7	59.1
Center	6.5	58.3
5'	6.2	58.6
1/2	5.6	
0	5.2	59.6
1/4	5.0	
5'	5.0	59.8
Center	4.9	59.9
ct	4.4	60.4
N.	4.0	60.8



60.78

175' E 39

No	2.8	62.0
14	7.1	60.7
14	4.3	60.5
Center	5.7	59.6
5'	5.1	59.7
1/2	5.3	
0	5.3	59.5
1/2	5.9	
5'	4.3	58.5
Center	6.7	58.1
14	6.0	
5.	5.8	

200' E = W.L. 4th

5.	6.0	
14	6.3	
Center	6.7	58.1
8'	4.5	58.3
1/2	6.0	
0	5.5	59.3
1/4	5.2	
5'	4.8	60.0
Center	4.6	60.2
14	4.3	60.5
No	4.0	60.8
	4.84	60.44 ✓

BM. N. W 4th

60.44







74.10

100' 50" Ash

W.	6.7	67.4
ct	6.6	67.5
Centre	7.2	66.9
5'	7.0	67.1
$\frac{1}{2}$	6.4	
2'	6.3	67.8
2'	6.3	67.8
$\frac{1}{2}$	6.4	
5'	6.6	67.5
Centre	7.0	67.1
ct	6.3	67.8
E	6.1	68.0
115' 50"		
E	6.6	67.5
ct	7.2	66.9
Centre	8.2	65.9
5'	7.5	66.6
$\frac{1}{2}$	7.3	
2'	7.2	66.9
2'	7.0	67.1
$\frac{1}{2}$	7.3	66.8
5'	7.8	66.3
Centre	7.9	66.2
ct	7.4	66.7
W	7.3	66.8

T.P.

1.52

14.1  
67.40

8.52

65.88

34

167' 50"

W	1.5	65.9
ct	1.5	65.9
Centre	2.0	65.4
5'	1.9	65.5
$\frac{1}{2}$	1.4	
2'	1.2	66.2
2'	1.3	66.1
$\frac{1}{2}$	1.7	
Centre	2.4	65.0
ct	1.4	66.0
E	1.0	66.4
175' 50"		
E	1.8	65.6
ct	2.3	65.1
Centre	3.4	64.0
5'	2.5	64.9
$\frac{1}{2}$	2.3	65.1
2'	2.2	65.2
2'	2.1	65.3
$\frac{1}{2}$	1.9	
5'	2.6	64.8
Centre	3.0	64.4
ct	2.4	65.0
W	2.2	65.2



67.40

200' So Ash St

W	30	64.4
Ch	33	64.1
Grtr	39	63.5
5'	37	63.7
1/2	22	
1'	29	64.5
2'	31	64.3
1/4	32	
5'	34	64.0
Grtr	44	63.0
Ch	31	64.3
E	26	64.8

225' S.

E	38	63.6
Ch	39	63.5
Grtr	50	62.4
5'	43	63.1
1/4	41	
2'	39	63.5
2'	38	63.6
1/4	40	
5'	44	63.0
Grtr	49	62.5
Ch	42	63.2
W	41	63.3

150' S.

W	49	62.5
Ch	52	62.2
Grtr	58	61.6
5'	55	61.9
1/2	49	
2'	45	62.9
2'	47	62.7
1/4	48	
5'	50	62.4
Grtr	55	61.9
Ch	47	62.7
E	45	62.9

275' S.

E	54	62.0
Ch	55	61.9
Grtr	61	61.3
5'	58	61.6
1/4	56	
2'	55	61.9
2'	55	61.9
1/4	59	
5'	63	61.1
Grtr	68	60.9
Ch	61	61.3
W	56	61.8



67.40

300' Si. Ash - No. 111A

W.		6.7	60.7
ct		6.9	60.5
Entr		7.1	60.3
5'		6.9	60.5
4'		6.1	
2'		6.2	61.2
2'		6.1	61.3
1/2'		6.1	
5'		6.5	60.9
Entr		6.6	60.8
ct		6.3	61.1
E		6.1	61.3
	0.59	61.03	6.94
		No. Cl. A	
E		0.1	60.9
		0.3	60.7
ct		0.6	60.4
+5		0.5	60.5
1/4'		0.0	
2'		0.0	61.0
2'		0.0	61.0
1/2'		0.1	
5'		0.7	60.3
ct		1.1	59.9
		0.6	60.4
W		1.2	59.8

No. 5' line

W	1.0	60.0
ct	0.9	60.1
+5	0.6	60.4
1/4'	0.1	60.9
2'	0.0	61.0
2'	0.0	61.0
1/2'	0.1	
5'	0.5	60.5
ct	0.8	60.2
E	0.5	60.5
	No. 1/2	
E	0.4	
	1.0	
5'	0.4	
1/4'	0.2	
2'	0.2	
1'	0.2	
1/2'	0.2	
5'	0.6	
ct	0.6	
W	0.8	



61.03

Chr A

N	0.9	60.1
Ch	1.1	59.9
5'	1.0	60.0
7'	0.7	
2'	0.2	60.8
2'	0.4	60.6
7'	0.5	60.5
5'	1.0	60.0
Ch	1.2	59.8
E	0.5	60.5

So 7 A

E	0.9	
Ch	1.3	
5'	1.1	
4'	0.7	
2'	0.5	
2'	0.2	
7'	0.9	
5'	1.2	
Ch	1.0	
N	1.2	

So 5' line A

N	1.6	59.4
Ch	1.5	59.5
5'	1.4	59.6
7'	1.0	60.0
2'	0.4	60.6
2'	0.6	60.4
7'	0.8	
5'	1.3	59.7
Ch	1.3	59.7
E	1.2	59.8

S. Ch A

E	1.2	59.8
	0.6	60.4
Ch	1.5	59.5
5'	1.2	59.8
4'	0.9	
2'	0.6	60.4
2'	0.6	60.4
7'	1.2	
5'	1.5	59.5
Ch	1.8	59.2
	1.5	59.5
	1.0	60.0
N		

37



61.23

## Saline A

W	0.9	60.1
Cl	1.1	59.9
Center	1.8	59.2
5'	2.0	59.0
4'	1.6	59.4
2'	1.1	59.9
2'	1.0	60.0
4'	1.2	
5'	1.7	59.3
Center	1.7	59.3
Cl	0.7	60.3
E	0.4	60.6

25'So

E	2.5	58.5
Cl	2.8	58.2
Center	3.3	57.7
5'	3.1	57.9
7'	2.9	
2'	2.7	58.3
2'	2.6	58.4
4'	3.2	
5'	3.7	57.3
Center	4.0	57.0
Cl	3.3	57.7
W	3.3	57.7

38

## 50'So A

W	5.5	55.5
Cl	5.4	55.6
Center	5.9	55.1
5'	5.7	55.3
4'	5.4	
2'	5.0	56.0
2'	5.0	56.0
4'	5.1	
5'	5.2	55.8
Center	5.3	55.7
Cl	4.8	56.2
E	4.6	56.4

75'So A

E	6.5	54.5
Cl	6.9	54.1
Center	7.7	53.3
5'	7.3	53.7
4'	7.3	
2'	7.1	53.9
2'	7.1	53.9
4'	7.6	
5'	7.8	53.2
Center	8.2	52.8
Cl	7.6	53.4
W	7.6	53.4

T.P. 170

52.67

10.04

50.99



5269

100' S. A

W	1.7	51.0
Cl	1.6	51.1
Grtr	2.1	50.6
5'	1.8	50.9
$\frac{1}{2}$	1.6	
2'	1.0	51.7
2'	0.8	51.9
$\frac{1}{2}$	1.0	51.7
5'	1.4	51.3
Grtr	1.5	51.2
Cl	0.6	52.1
E	0.5	52.2

125' S. A

E	2.6	50.1
Cl	2.7	50.0
Grtr	3.4	49.3
5'	3.0	49.7
$\frac{1}{2}$	2.8	
2'	3.0	49.7
2'	3.0	49.7
$\frac{1}{2}$	3.5	49.2
5'	3.9	48.8
Grtr	4.2	48.5
Cl	3.7	49.0
W	3.9	48.8

150' S

W	0.7	47.0
Cl	0.7	47.0
Grtr	0.7	47.0
5'	0.1	47.6
$\frac{1}{2}$	4.8	
2'	4.7	48.0
2'	4.6	48.1
$\frac{1}{2}$	4.3	
5'	4.5	48.2
Grtr	5.1	47.6
Cl	4.6	48.1
E	4.4	48.3

175' S.

E	5.1	47.6
Cl	5.2	47.5
Grtr	5.6	47.1
5'	5.4	47.3
$\frac{1}{2}$	5.2	
2'	5.4	47.3
2'	5.5	47.2
$\frac{1}{2}$	5.7	
5'	6.0	46.7
Grtr	6.2	46.5
Cl	6.2	46.5
W	6.1	46.6



57-69

200' S. A.

W	6.6	46.1
d	6.6	46.1
Gtr	6.6	46.1
5'	6.3	46.4
4'	6.2	
3'		
2'	6.1	46.6
1'	6.0	46.7
1/2'	5.9	
5'	6.3	46.4
Gtr	6.1	46.6
d	5.6	47.1
E	5.7	47.3

225' S.

E	5.8	46.9
d	6.1	46.6
Gtr	6.6	46.1
5'	6.5	46.2
4'	6.3	
3'	6.5	46.2
2'	6.5	46.2
1'	6.8	
5'	7.0	45.7
Gtr	7.3	45.4
d	7.0	45.7
W	7.2	45.5

40

250' S.

W	7.4	45.3
d	7.4	45.3
Gtr	7.5	45.2
5'	7.5	45.2
4'	7.4	
3'		
2'	7.1	45.6
1'	6.9	45.8
1/2'	6.9	
5'	6.7	46.0
Gtr	6.9	45.8
d	6.4	46.3
E	6.1	46.6

275' S.

E	6.8	45.9
d	6.8	45.9
Gtr	7.5	45.2
5'	7.1	45.6
4'	7.1	
3'	7.3	45.4
2'	7.5	45.2
1'	7.5	
5'	7.9	44.8
Gtr	7.9	44.8
d	7.7	45.0
W	8.0	44.7



5-69

300'S. = NL B

W	8.0	44.7
U	8.2	44.5
Gtr	8.8	43.9
5'	8.4	44.3
7	8.1	
2'	7.9	44.8
2'	7.8	44.9
7	7.7	
5'	7.9	44.8
Gtr	8.0	44.7
CA	7.3	45.4
E	7.2	45.5



Cross-Section 15<sup>th</sup> St E to G

5 Days  
15 Williams  
10 Hancock

	1.66	4.1 44.50	42.19 BM NW 1/4 F	
		No line "F"		
E		1.2	43.3	
Cl		1.2	43.3	
1/4		1.3	43.2	
C		2.0	42.5	
1/2		1.9	42.6	
Cl		1.4	43.1	
W		1.0	43.5	
		10' N.		
W		0.9	43.6	
Cl		1.4	43.1	
1/4		2.1	42.4	
C		1.9	42.6	
1/2		3.4	41.1	
+9		6.1	39.4	
Cl		4.7	39.8	
+4		3.0	41.5	
E		3.0	41.5	

25' N.

E	4.3	40.2
Cl	7.0	37.5
1/2	4.0	40.5
C	3.0	41.5
1/4	2.6	41.9
Cl	1.3	43.2
W	0.8	43.7

50' N.

W	0.8	43.7
Cl	1.5	43.0
1/4	0.5	41.0
1/2	3.6	40.9
C	3.9	40.6
+5	4.4	40.1
1/4	8.3	36.2
+5	9.7	34.8
Cl	10.4	34.1
+7	10.2	34.3
E	5.5	39.0
+3	4.4	40.1
+10	4.5	40.0



49.50  
75' N.

NE	57	38.8
E	57.2	37.3
Cl	59.6	34.9
	10.4	34.1
+7	9.5	35.0
$\frac{1}{4}$	7.7	36.8
+6	5.3	39.2
C	4.4	40.1
$\frac{1}{4}$	5.0	39.5
+4	6.0	38.5
+7	2.7	41.8
Cl	1.9	42.6
W.	1.5	43.0
	100' N.	
W	1.5	43.0
Cl	1.7	42.8
$\frac{1}{4}$	2.7	41.8
+4	3.3	41.2
C	5.1	39.4
+8	4.5	40.0
$\frac{1}{4}$	7.0	37.5
+7	9.7	34.8
Cl	10.4	34.1
E	10.6	33.9
+3	7.5	37.0
+15	6.0	38.5

43

125' N.

15E	6.1	38.4
11E	7.0	37.5
4E	8.1	36.4
	9.7	34.8
E	9.8	34.7
+4	9.1	35.4
Cl	9.4	35.1
+7	8.8	35.7
$\frac{1}{4}$	6.9	37.6
+9	6.3	38.2
C	3.6	40.9
+3	3.0	41.5
$\frac{1}{4}$	2.4	42.1
Cl	1.7	42.8
W.	1.5	43.0
	150' N.	
W	1.4	43.1
Cl	1.8	42.7
$\frac{1}{4}$	2.0	42.5
C	2.6	42.0
+4	2.8	41.7
+9	7.6	36.9
$\frac{1}{4}$	7.7	36.8
+6	8.1	36.4
Cl	8.9	35.6
E	8.9	35.6



		44.5°			
		150' N <sub>0</sub>			
7'E. + EL		8.8	35.7		
25' . . .		6.2	38.2		
		175' N <sub>0</sub>			
25'E		7.0	37.5		
E		{ 7.7	36.8		
		{ 9.4	35.1		
CL		6.2	36.3		
+8		9.3	36.2		
1/2		7.9	36.6		
+4		7.5	37.0		
+10		2.2	42.3		
C		1.2	43.3		
1/2		1.3	43.2		
d.		1.0	43.5		
W.		0.8	43.7		
TR	6.72	50.28	0.95	43.50	
		200' N <sub>0</sub>			
W.		5.4	44.9		
d.		5.8	44.5		
1/2		6.0	44.3		
+7		6.0	44.3		
C		9.4	40.9		
+8		13.4	36.9		
1/2		13.1	37.2		
d.		13.2	36.9		
E		{ 14.2	36.1		
		{ 12.0	38.3		

		44	
		200' N <sub>0</sub>	
25'E.		11.8	38.5
		225' N <sub>0</sub>	
25'E		11.1	39.2
4'E		11.5	38.8
E		12.8	37.5
CL		13.1	37.2
1/2		12.9	37.4
+7		12.2	37.1
C		2.3	42.0
+6		5.2	45.0
1/2		5.2	45.1
CL		5.3	45.0
W.		6.0	45.3
		250' N <sub>0</sub>	
W.		4.7	45.6
CL		4.6	45.7
1/2		4.6	45.7
+8		4.3	46.0
C		8.0	42.3
+5		9.3	41.0
+10		12.8	37.5
1/2		12.7	37.6
CL		13.4	36.9
E		13.1	37.2
+2		11.2	39.1
25'E		12.5	



50.2P  
240' N. of F

25'E	10.0	40.3
3'E	16.0	39.3
E	12.1	38.2
Ch	12.9	37.5
4	12.3	38.0
C	2.1	42.2
16	4.6	45.7
4	9.2	46.1
Ch	3.3	47.0
W	2.7	46.6
295' N.		
W	3.8	46.5
17	2.2	48.1
Ch	1.4	48.9
4	3.4	46.9
C	5.6	44.7
4	5.7	44.6
Ch	5.5	44.8
E	4.5	45.8
10'E	4.0	46.3

300' No = 50 line F St

45

E	0.2	50.3
Ch	0.2	50.1
4	0.1	50.2
C	0.1	50.2
4	0.1	50.2
Ch	0.5	49.8
W	0.1	50.2
0.52      43.36		
50 line "F" St.		
W	0.1	43.3
Ch	0.5	42.9
4	0.6	42.8
C	0.4	43.0
4	0.7	42.7
Ch	1.3	42.1
E	0.4	43.0
9' 5.		
E	1.2	42.2
Ch	1.5	41.9
Ch	2.6	40.8
4	6.4	37.0
C	6.1	36.7
4	4.5	36.9
+14	8.5	34.9
Ch	7.2	36.2



43-36

9'S.

W.L.	{ 3.9 1.6	39.5 41.8
10'W	4.3	42.1
	17'S.	
10'W	2.0	41.4
W	{ 2.6 3.2	40.7 36.0
Cl.	2.7	34.7
7	1.9	34.5
C	1.9	34.5
4	5.4	38.0
Cl.	3.2	40.2
+3	2.1	41.3
E	1.8	41.6
	20'S.	
E	2.6	40.8
+11	2.6	40.8
Cl.	3.7	39.7
+4	4.8	38.6
4	5.3	38.1
C	9.2	34.2
2	9.2	34.2
Cl.	9.3	34.1
W	{ 9.1 4.2	34.2 39.1
10'W	3.4	40.0

46

50'S.

10'W	6.4	37.0
W	{ 7.0 7.5	36.4 39.8
Cl.	9.8	33.4
2	10.2	33.1
C	9.8	33.6
+7	6.6	36.8
2	5.8	37.6
Cl.	4.5	38.9
E	3.6	39.8
	75'S.	
E	3.7	39.7
Cl.	4.0	39.4
4	5.9	37.5
+8	6.2	37.2
C	8.1	35.3
+2	10.1	33.3
Cl.	10.6	32.8
Cl.	10.3	33.1
W	{ 9.7 7.8	33.7 35.6
10'W	7.6	35.8



43-36

100' So F

W - No Slope	10.5	32.9
Ch	10.5	32.9
$\frac{1}{2}$	11.0	32.4
+10	10.4	33.0
C	8.9	34.5
+12	7.6	35.8
$\frac{1}{4}$	5.9	37.5
Ch	4.9	38.5
E	4.0	39.4

125' So F

E	3.9	39.5
Ch	4.6	38.8
$\frac{1}{4}$	5.9	37.5
+2	7.6	35.8
+10	10.7	32.7
C	10.7	32.7
$\frac{1}{2}$	11.1	32.3
Ch	11.4	32.0
W - No Slope	11.0	32.4
T.P.	8.29	40.11
	11.54	31.82

47

150' So F

10 W	8.7	31.4
W	8.6	31.5
Ch	8.4	31.7
$\frac{1}{2}$	9.0	31.6
+3	8.1	32.0
+6	9.2	30.9
C	7.7	32.4
+7	6.6	33.5
$\frac{1}{4}$	3.0	37.1
Ch	1.8	38.3
E	0.6	39.5

175' So

E	1.1	39.0
Ch	1.8	38.3
+7	2.0	38.1
$\frac{1}{2}$	3.8	36.3
+4	7.0	33.1
C	8.2	31.9
+7	9.5	30.6
+10	8.4	31.7
$\frac{1}{4}$	9.8	30.3
Ch	9.5	30.6
W	9.1	31.0
	8.1	32.0
10 W	8.0	32.1



4011  
200' S. 1/2'

11W	8.0	32.1
W	{ 8.0 8.8	{ 32.1 31.3
Cl	9.6	30.5
1/2	9.9	30.2
+3	8.8	31.3
+6	9.4	30.7
+8	8.8	31.3
C	7.9	32.2
+4	7.6	32.5
1/2	2.6	37.5
Cl	1.9	38.2
E	1.6	38.5
225' S.		
E	2.0	38.1
Cl	2.2	37.9
1/2	2.6	37.5
+8	7.3	32.8
C	7.7	32.4
+3	8.0	32.1
+8	9.7	30.4
+11	9.2	30.9
1/2	9.9	30.2
Cl	9.6	30.5
W	{ 9.6 9.2 8.2	{ 31.9 31.9
10W		

48

257' S.

11W	8.7	31.4
W	{ 8.7 9.4	{ 31.4 30.7
Cl	9.8	30.3
1/2	9.3	30.8
C	8.6	31.5
+10	7.6	36.5
1/2	3.2	36.9
Cl	3.0	37.1
E	2.6	37.5
275' S.		
E	3.0T	36.6
Cl	3.6	36.5
1/2	3.8	36.3
+6	4.0	36.1
+8	6.8	33.3
C	8.4	31.7
1/2	10.0	30.1
Cl	10.4	29.7
W	{ 8.6 8.7	{ 30.5 31.4
10W	8.7	31.4



40.11

293 S.F

10'W	6.5	33.6
W	{ 8.7	31.4
	{ 9.5	30.6
Ch	9.3	30.8
$\frac{1}{2}$	9.3	30.8
+8	9.2	30.9
C	6.5	34.6
$\frac{1}{4}$	4.6	35.5
Ch	4.9	35.7
E	4.2	35.9
	300 S. 17 N. L. C. 51	
E	4.2	35.9
Ch	4.6	35.5
$\frac{1}{4}$	4.6	35.5
C	6.0	35.1
+6	6.0	35.1
+7	6.2	33.9
$\frac{1}{4}$	5.6	34.5
Ch	6.1	34.0
+10	6.4	33.7
W	5.6	34.5



5 Hatch  
 20 Mine  
 10 Patrick  
 X Rec Falcon St from  
 St Arnold - Choate To Alley  
 of Blk 283 Northern Extension

W	6.10	271.902	265.502	Falcon Washington
	5.22	270.40	6.72	265.18
		Pueblo line		
W		4.6	265.8	
cb		4.9	265.5	
1/2		4.9	265.5	
c		4.9	265.5	
1/2		5.1	265.3	
cb		5.1	265.3	
E		5.5	264.9	
		25' S.		
E		5.5	264.9	
cb		5.5	264.9	
1/2		5.2	265.2	
c		5.1	265.3	
1/2		5.2	265.2	
cb		5.2	265.2	
W		4.6	265.8	
		50' S.		
W		4.8	265.6	
cb		4.8	265.6	
1/2		4.8	265.6	
c		5.0	265.4	
W		5.1	265.3	

15' street  
 14' Curb on West  
 10' " " East

270.40

cb	5.3	265.1
E	5.5	264.9
	75' S.	
E	5.4	265.0
cb	5.3	265.1
1/2	5.0	265.4
c	5.1	265.3
1/2	5.0	265.4
cb	5.0	265.4
W	5.5	264.9
	100' S.	
W	6.3	264.1
cb	6.0	264.4
1/2	6.0	264.4
c	6.2	264.2
1/2	6.2	264.2
cb	6.2	264.2
E	6.5	263.9
	125' S.	
E	7.2	263.2
cb	7.2	263.2
1/2	7.4	263.0
c	7.3	263.1
1/2	7.3	263.1



	370.40		
cb		7.4	263.0
W		7.5	262.9
	135.5	E	
	137.0	W to Alleyhine	
W		8.4	262.0
cb		8.1	262.3
1/2		8.2	262.2
C		8.2	262.2
1/2		7.9	262.5
cb		7.9	262.5
E		7.5	262.9



51

52







53

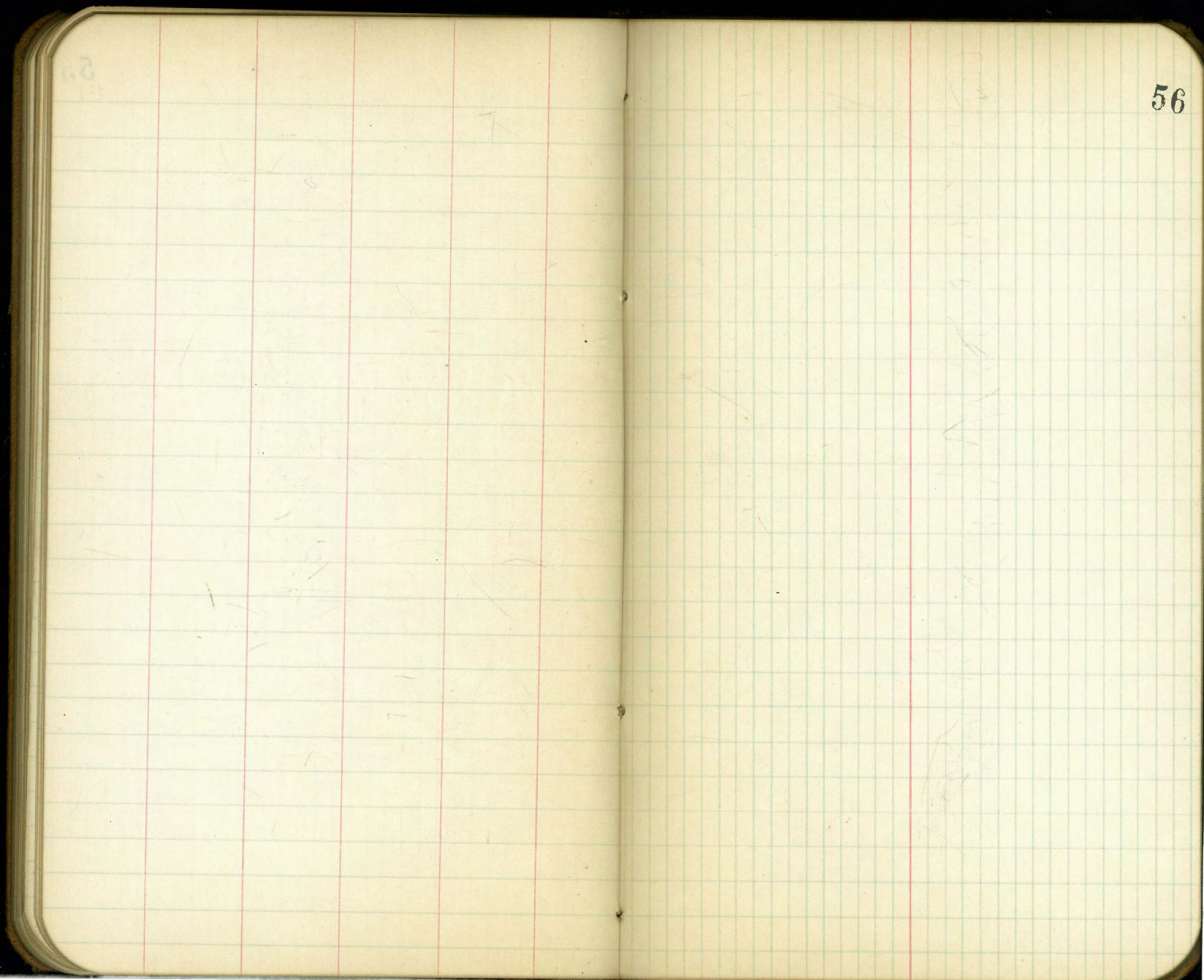
54



54

55

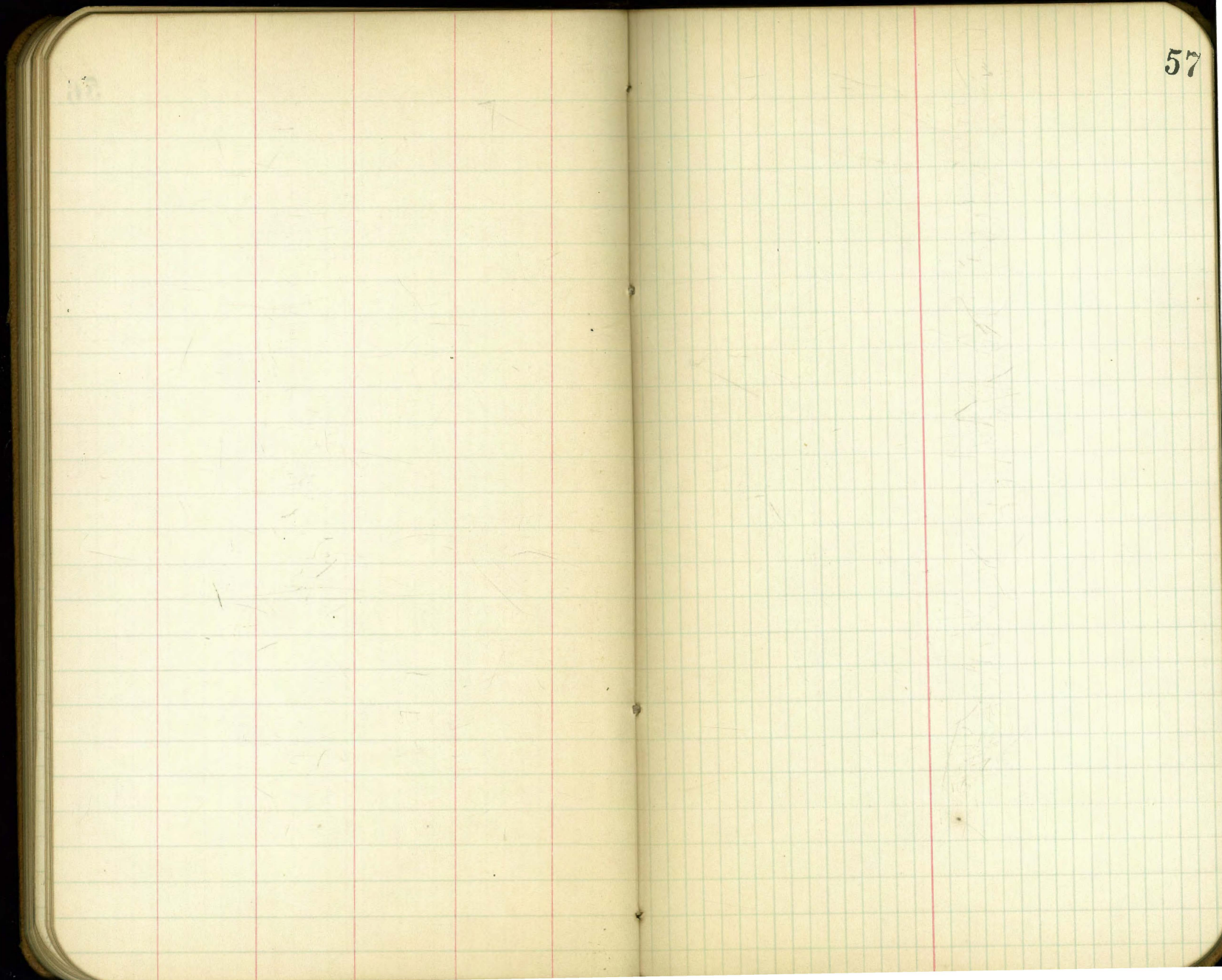




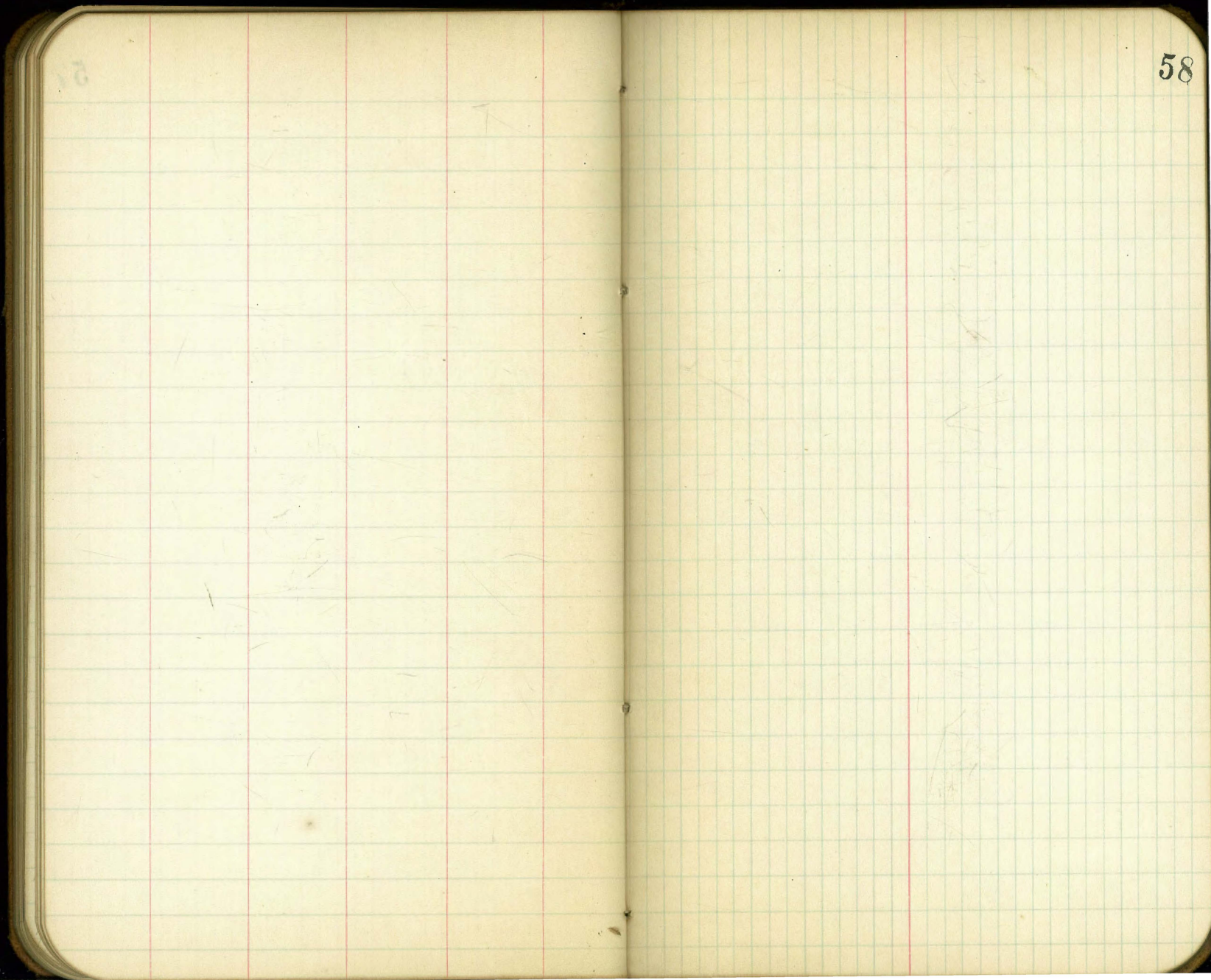
53

56









58



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63



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66



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68



68

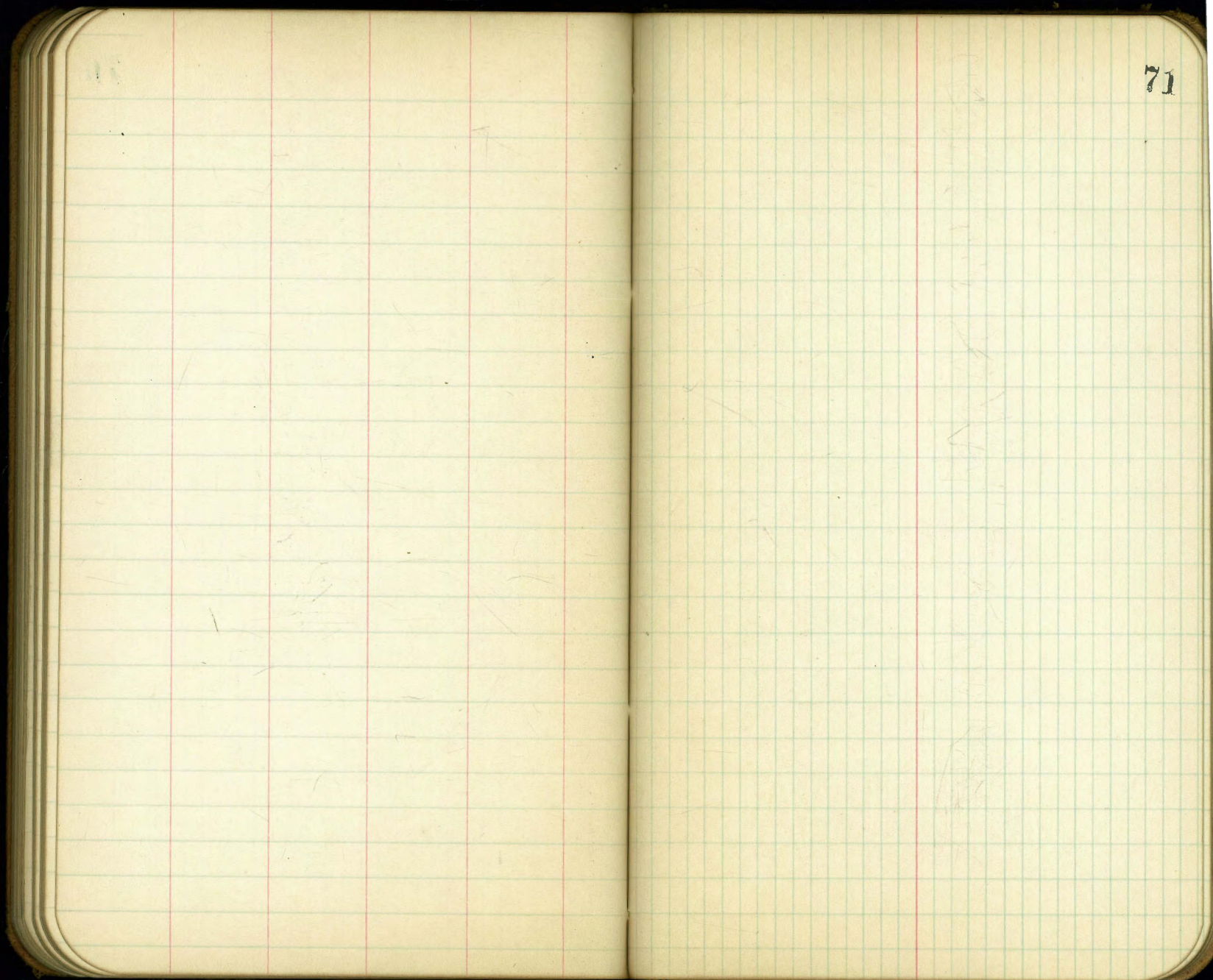
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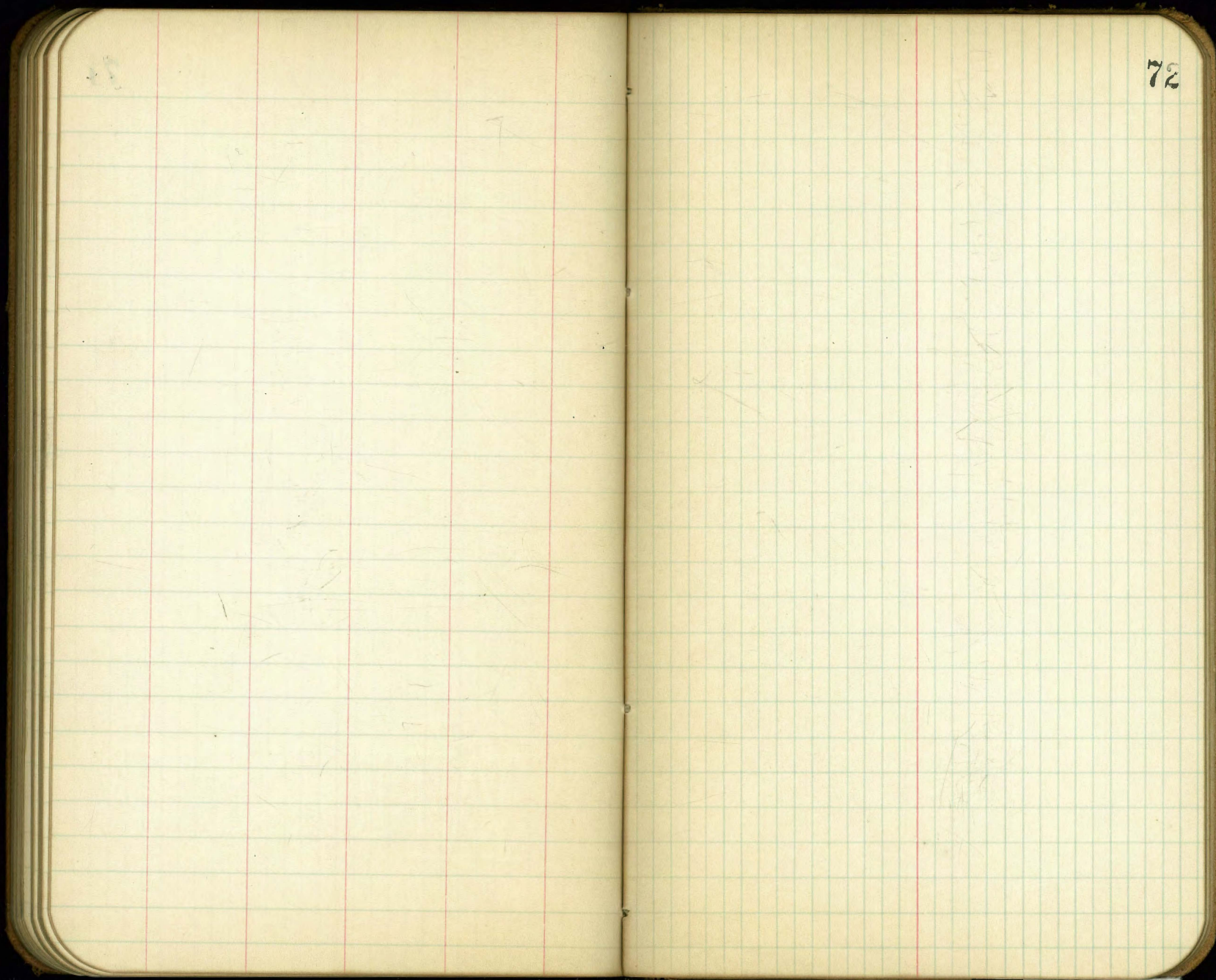
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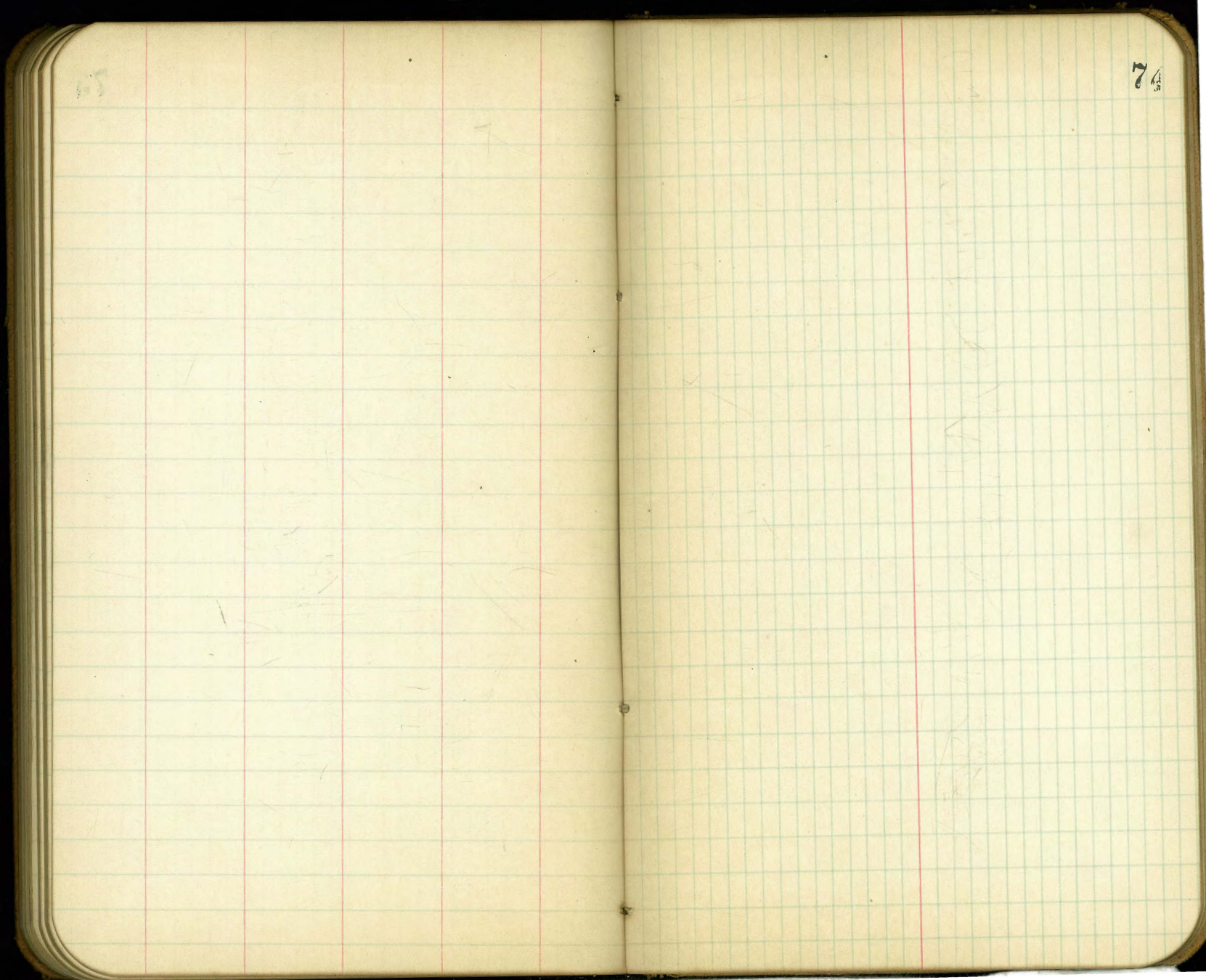
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57

73





65

74







85

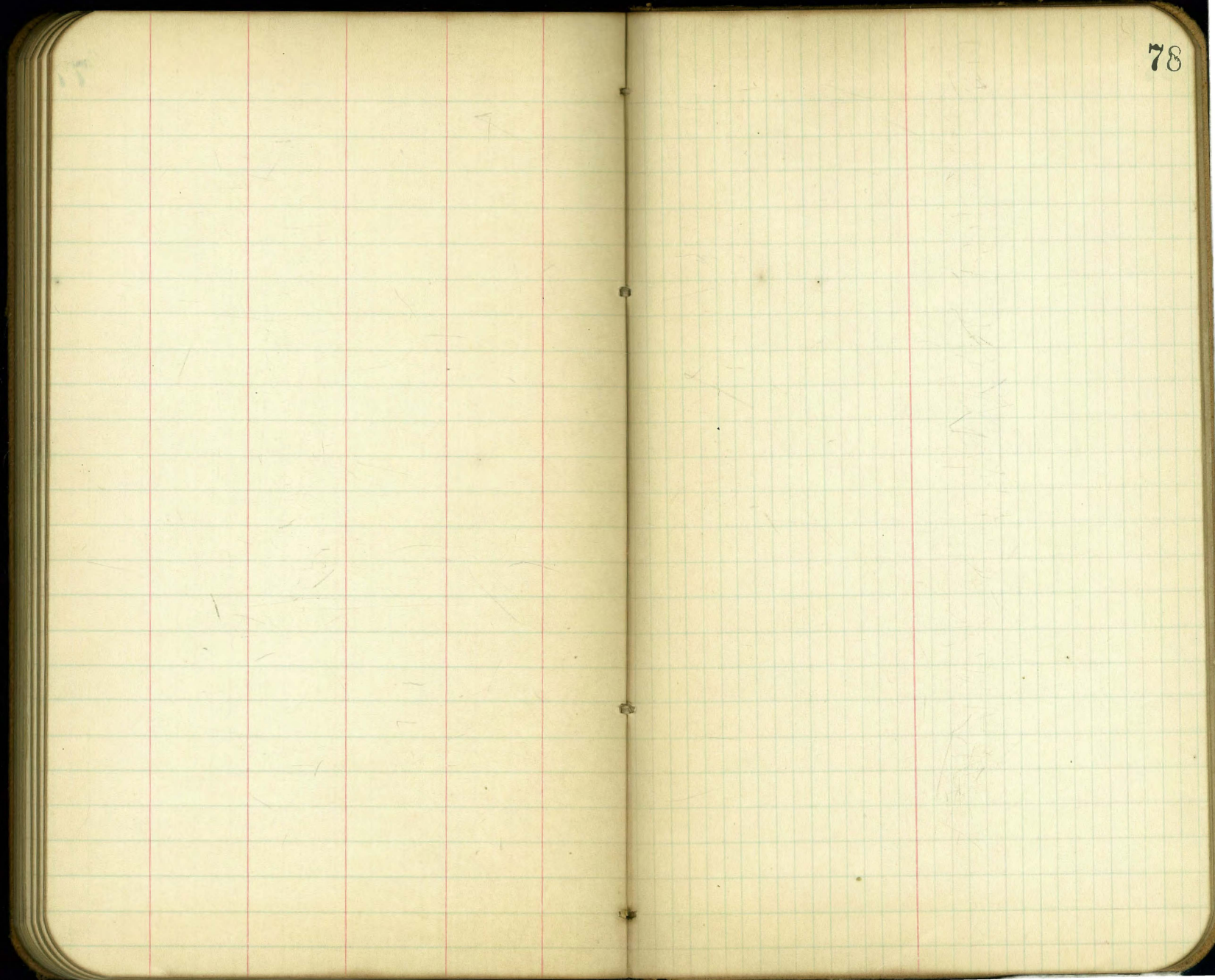
76



76

77







65

79



60.44 - N.W. 3<sup>rd</sup> & A. pl ght  
 70.41 B.M. S.W. Ash. 2<sup>d</sup>  
 55.51 - B.M. N.W. 2<sup>d</sup> & A  
 60.44 N.W. 4<sup>th</sup> and A.  
 4284 N.W. 15<sup>th</sup> & F. pl ght.

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 From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		½ DEGREE.		¼ DEGREE.		¼ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
Degrees.	DEGREES		½ DEGREE.		¼ DEGREE.		¼ DEGREE.		Degrees