

B Street Condit.

214

TRANSIT

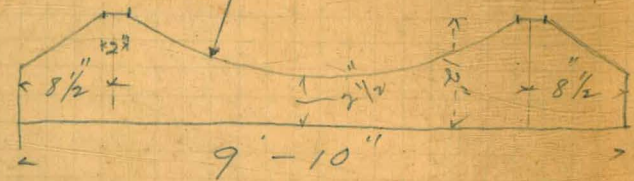
F.B. 214

23
 7.52
 15.17 | 13.45
 13.95 | 11.78 1.13%
 1720
 1345
 3750
 2690
 10600

2105 8816
 418 129
 25.78 36.87
 15.63
 7.10

Sec E.

R = 10' - 11"



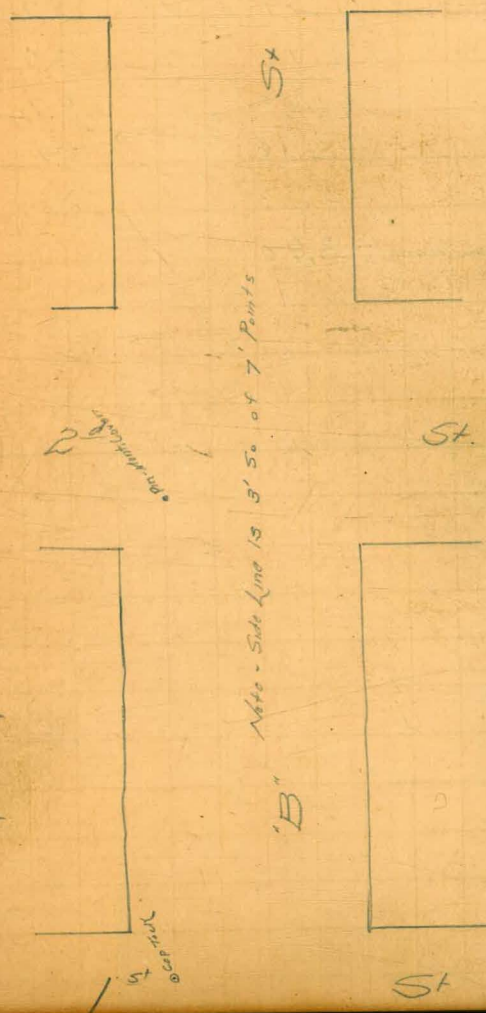
49.89 NE com. Hyd. nozzle. 4" C
 49.27 SE " " " " "

7.52
 2250
 8.056
 8.282
 8.238
 8.664
 8.920
 9.146
 9.372
 9.598
 9.824
 10.050

B.M. 18.63 N.E. cor. B + India
no. of Hyd.

B Street Sewer line

Sta		Grade	H.I.	Rod	Elev.	Out	3' ^{at 100'}	St
0.0	C. Columbia	14.97	23.71					
0+37.5		14.40		2.7	21.0	6.6		
+87.5		13.63		3.5	20.2	6.6		
1+37.5		12.87		4.5	19.2	6.3		
+97.5		12.11		5.3	18.4	6.3		
2+37.5		11.35		6.0	17.7	6.4		
+75	C. India	10.78						
3+12.5		9.95	19.58	2.8	16.8	6.9		
+62.5		8.83		4.1	15.5	6.7		
4+12.5		7.72		5.1	14.5	6.8		
+62.5		6.61		6.2	13.4	6.8		
5+12.5		5.50		7.1	12.5	7.0		
+50.0	C. Artic	4.67						
+87.5		4.33		8.3	11.3	7.0		
6+37.5		3.88		8.9	10.7	6.8		
+87.5		3.43		9.7	9.9	6.5		
7+37.5		2.99		10.6	9.0	6.0		
+87.5		2.54		11.53	8.05	5.5		
8+21.5	3/4 East of C. Calif.	2.24						



Note - Side Line is 3' 5" or 7' Points

B

15'

Sta.		Grade	H.I.	Rod	Elev.	cut
8+62.5		1.29	10.11	2.7	7.4	6.1
9+12.5		0.14		3.8	6.3	6.2
+62.5		-1.02		4.7	5.4	6.4
10+12.5		-2.18		5.9	4.2	6.4
+62.5		-3.33		6.8	3.3	6.6
+87	Main sewer at Atlantic	-3.90				

Grades for Sewer in "B" St bet
Columbia & India. $\frac{4}{16}$ } Saws 3
86 } Ropes
Thimble

	Hi.				Sta	Rod	Ground	Grade	±
	443	<u>23.06</u>							
				BM					
				18.63	0=Ctr India			10.78	
					+50			11.52	
					1			12.26	
					+50			13.00	
					2			13.75	
					+50			14.49	
					+75 Ctr Col.			<u>14.86</u>	

$\frac{11.52}{11.54}$ ✓
 $\frac{12.26}{10.80}$ ✓
 $\frac{13.00}{10.06}$ ✓
 $\frac{14.75}{9.34}$ ✓
 $\frac{14.49}{8.57}$ ✓
 $\frac{9.95}{13.11}$ ✓

Line Stakes from Union to India
set 18.95' S. of N. 7' Line ^{5/12/06}

Line Stakes from Union - E. set
18.45' S of N 7' Line -

Line Stakes from First - 3^d
set 3' S of N 7' Line

Line Stakes from India - Arctic
= 25.95' S. of N Property line

Cr. Stakes India - Arctic
6.75' N. of 18" line

Cr. Stakes Arctic - Atlantic
11.75' S of 4' line

Section "F" Cr. line 12.27 from
N 4' line of "B" St in favor E. Union

Section "E" Cr. Line 12' from N 7' ^{line}
Cr. line 6.42' N of side line

Grades for Conduit
 5/17/66 ^{Slaty} _{Woods} Cut Stakes

	7.04	25.67	Red.	Elev	Grade
B.M. NE. India				18.63	
E.L. India			8.37	17.30	7.83
			7.97	17.70	8.06
			7.90	17.77	8.29
			7.50	18.17	8.51
			7.26	18.41	8.74
			6.87	18.80	8.97
			6.48	19.19	9.20
			6.06	19.61	9.42
			5.77	19.99	9.65
			5.42	20.25	9.88
W.L. Columbia			5.01	20.66	10.10
19			4.37	21.30	10.82
41			3.89	21.87	10.57
64			3.55	22.12	10.83
86			3.17	22.50	11.08
108			2.62	23.05	11.33
130			2.20	23.47	11.58
153			1.56	24.11	11.83
175			0.93	24.74	12.09

0.86
 (add 0.42 for Cr.)
 " " " Side
 1.66

cut	R	el.	R	el.	R	el.
	cr.		North		South	
9.47						
9.64		2.35		20.98		18.63
9.49		3.82		13.02		11.75
9.73						9.10
9.75						
9.88						
10.04						
10.24						
10.30						
10.43						
10.61						
11.04						
11.36						
11.35						
11.48						
11.78						
11.95						
12.33						
12.71						

		38.16					
199	1275	38.16	826	25.41	12.35		13.12
219			1217	25.99	12.59		13.46
242			1159	26.57	12.75		13.79
264			1095	27.21	13.10		14.18
286			1020	27.96	13.35		14.68
308			926	28.90	13.60		15.37
329			873	29.43	13.84		15.66
350	E. L. State		851	29.65	14.08	75.65	15.57
365			829	29.92	14.25	15.75	15.67
386			780	30.36	14.49	15.95	15.87
406			711	31.05	14.71	16.41	16.34
427			650	31.66	14.95	16.79	16.71
448			577	32.39	15.19	17.28	17.20
469			523	32.93	15.43	17.58	17.50
489			455	33.61	15.66	18.04	17.95
510			388	34.28	15.90	18.47	18.38
530			334	34.82	16.12	18.79	18.70
550	W. L. Union				16.35		

Cont. P 61

5/29/16
6/23/16

Grade Stakes

				Bottom Grade	
	235	20.98		1863	
	382	13.02	11.78	9.20	
E Line India				7.83	
10				7.94	
20	3.97	12.96	352	8.06	9.49
30	380	12.95		8.17	9.15
40				8.29	
50				8.40	
60				8.51	
70				8.62	
80				8.74	
90				8.85	
100				8.97	
110				9.08	
120				9.20	
130				9.31	
140				9.42	
150				9.53	
160				9.65	
170				9.76	
180				9.88	

Rate - 1.136%

NI = 12.65

cu	Side
4086	1857 166
	1131
	13.16 NI
Red	Red
Original	Sidegrade
3.96	8.69
3.85	8.80
4.10	8.92
3.99	9.03
3.87	9.15
3.76	9.26
3.65	9.37
3.54	9.48
3.42	9.60
3.31	9.71
3.19	9.83
3.08	9.94
2.96	10.06
2.85	10.17
2.74	10.28
2.63	10.39
2.51	10.51
2.40	10.62
2.28	10.74
	3.16
	3.05
	3.44
	3.33
	3.00
	2.99
	2.78
	2.67
	2.55
	2.44
	2.32
	2.21
	2.09
	1.98
	1.87
	1.76
	1.64
	1.74
	1.62
	9.49
	9.60
	9.72
	9.83
	9.95
	10.06
	10.17
	10.28
	10.40
	10.51
	10.63
	10.74
	10.86
	10.97
	11.08
	11.19
	11.31
	11.42
	11.54

	13.02	
190	9.99	
200	10.10	
W L Columbia	10.21	
270	10.33	
220	10.44	
230	10.55	
240	10.67	
250	10.75	
260	10.95	
E. L. Columbia	11.07	
275	11.18	
10	11.29	
20	11.41	
30	11.52	
40	11.63	
50	11.75	
60	11.86	
70	11.97	
80	12.09	
90	12.20	
100	12.32	
110		
120		

Rate 11.26

$$\begin{array}{r} 11.76 \\ 45 \\ \hline 16.28 \text{ HI} \\ 913 \\ \hline 12.15 \\ 372 \\ \hline 15.87 \text{ HI} \\ 292 \\ \hline 12.95 \\ 322 \\ \hline 12.17 \text{ HI} \\ 5.09/06 \\ \hline 11.81 \\ 292 \\ \hline 19.73 \text{ HI} \end{array}$$

		452	
	+86	+166	8
Cr			Side
			13.16 HI
2.17	10.85	1.51	11.65
2.06	10.96	1.40	11.76
5.21	11.07	1.473	11.87
5.09	11.19	2.86	11.99
4.98	11.30	2.74	12.10
4.87	11.41	2.63	12.21
4.75	11.53	2.52	12.33
4.64	11.64	2.40	12.44
4.47	11.81	2.29	12.61
4.35	11.93	3.56	12.73
4.24	12.04	3.44	12.84
4.13	12.15	3.33	12.95
3.60	12.27	15.87 HI	13.07
3.49	12.38	2.92	13.18
3.38	12.49	2.80	13.29
3.26	12.61	2.69	13.41
3.15	12.72	2.58	13.52
3.04	12.83	2.46	13.63
2.92	12.95	2.35	13.75
2.81	13.06	2.24	13.86
2.69	13.18	2.12	13.98

$\left\langle \begin{array}{c} 4.48 \times 4.48 \\ \hline 8.96 \\ +.86 \end{array} \right\rangle$

9
+1.66

Bottom grade

130	12.73
140	12.57
150	12.66
160	12.77
170	12.88
180	13.00
200	
W.L. State	12.71
10	13.22
20	13.34
30	13.45
40	13.56
50	13.68
60	13.79
75 E.H. State	13.96
10	14.07
20	14.19
30	14.30
40	14.41
50	14.53
60	14.64
70	14.75

	Cr.	Grade	Side grade
15.87 HI	2.58	13.29	1.78 14.09
4.00	2.47	13.40	1.67 14.20
17.40 HI	3.88	13.52	3.08 14.32
	3.77	13.63	2.97 14.43
	3.66	13.74	2.86 14.54
	3.54	13.86	2.74 14.66
	3.43	13.97	2.63 14.77
	3.32	14.08	2.52 14.88
	3.20	14.20	2.40 15.00
18.20 HI	3.81	14.39	3.01 15.19
	3.09	14.31	2.29 15.11
	3.73	14.47	2.93 15.27
	3.78	14.42	2.98 15.22
	3.66	14.54	2.86 15.34
	3.55	14.65	2.75 15.45
	3.38	14.82	2.58 15.62
18.51 HI	3.58	14.93	2.78 15.73
	3.29	14.93	2.47 15.73
15.73	3.29	15.05	2.49 15.85
2.61	3.18	15.16	2.38 15.96
18.24 HI	3.07	15.27	2.27 16.07
16.19	2.96	15.39	2.15 16.19
3.71	4.40	15.50	3.60 16.30
18.90	4.29	15.61	3.49 16.41

cr.
+1.86

side
+1.66

80	14.87
90	14.98
100	15.10
110	15.21
120	15.34
130	15.47
140	15.69
150	15.72
160	15.84
170	15.97
180	16.10
190	16.22
200 W.L. Union	16.35
10	16.46
20	16.58
30	16.69
40	16.80
50	16.92
60	17.03
67 E.L. Union	17.11
15	17.28
30	17.45
40	17.57

A - Corrupted

19.90	4.17	15.73	5.37	16.53
<u>20.64</u> 147	4.06	15.84	5.26	16.64
	4.68	15.96	<u>20.564</u>	16.76
	4.57	16.07	3.8.0	16.87
	4.44	16.20	3.56	17.00
	4.31	16.33	3.43	17.13
	4.19	16.45	3.31	17.25
20.32	4.06	16.58	3.26	17.38
	3.62	16.70	3.06	17.50
	3.49	16.83	2.93	17.63
	3.68	16.96	2.80	17.76
	3.56	17.08	<u>20.70</u>	17.88
	3.43	17.21	2.82	18.01
	3.32	17.32		18.12
147				
<u>20.70</u>	3.26	17.44	2.46	18.24
	3.15	17.55	2.35	18.35
1776				
315				
<u>20.93</u> 147	3.04	17.66	2.24	18.46
19.26				
<u>20.91</u>	2.92	17.78	2.12	18.58
147				
	3.04	17.89	2.24	18.69
	2.96	17.97	2.16	18.77
0.78 1.58				
<u>20.91</u>	2.85	18.06	2.05	18.86
	2.68	18.23	1.88	19.03
	2.56	18.35	1.76	19.15

Sec E (8' 10" x 6'-0")

492 478
 454 462
 552
 537
 38
 592
 599
 2378
 1846
 532
 2378
 452
 1928
 504
 822
 12

50	17.68
60	17.79
70	17.90
80	18.02
90	18.14
100	18.25
110	18.36
120	18.47
130	18.59
140	18.70
150	18.81
160	18.93
170	19.04
180	19.15
190	19.26
198 W.L. Front	19.36
10	19.47
20	19.59
30	19.70
40	19.81
50	19.92

8 1/2" x 9.20' x 9.20' x
 15 1/2" ⁸⁻⁵ _{4-2 1/2}
 Cr
 add. 0.78
 add. 1.58
 11

Section E (5'-4" x 6'-0")

2091 HT

2.45	18.46	1.65	19.26
5.21	18.57	4.41	19.37
5.10	18.68	4.30	19.48
4.98	18.80	4.18	19.60
4.86	18.92	4.06	19.72
4.75	19.03	3.95	19.83
4.64	19.14	3.84	19.94
4.53	19.25	3.73	20.05
4.41	19.37	3.61	20.17
5.21	19.48	4.41	20.28
5.10	19.59	4.30	20.39
4.07	19.71	3.27	20.51
3.96	19.82	3.16	20.62
3.85	19.93	3.05	20.73
3.74	20.04	2.94	20.84
3.64	20.14	2.84	20.94
	20.25		21.05
4.41	20.37	3.61	21.17
4.30	20.48	3.50	21.28
4.19	20.59	3.39	21.39
4.08	20.70	3.28	21.50

2051
 418
 74.29
 2051
 427
 24.78 HT

0.78

1.58

60	20.07
70	20.16
80 E Line Front	20.27
10	20.38
20	20.49
30	20.60
40	20.72
50	20.84
60	20.95
70	21.06
80	21.17
90	21.29
100	21.40
110	21.51
120	21.63
130	21.75
140	21.86
150	21.97
160	22.08
170	22.20
180	22.31

252041 ✓
 247841 ✓
 20.82
 474
 25.1141

7.38	20.82	3.49	21.62
3.84	20.94	3.04	21.74
3.73	21.05	2.93	21.85
3.62	21.16	2.82	21.96
3.51	21.27	2.71	22.07
3.73	21.38	2.93	22.18
3.61	21.50	2.81	22.30
3.49	21.62	2.69	22.42
3.38	21.73	2.58	22.53
3.27	21.84	2.47	22.64
3.16	21.95	2.36	22.75
3.04	22.07	2.24	22.87
2.93	22.18	2.13	22.98
2.82	22.29	2.02	23.09
2.70	22.41	1.90	23.21
2.58	22.53	1.78	23.33
2.47	22.64	1.67	23.44
2.36	22.75	1.56	23.55
2.25	22.86	1.45	23.66
2.13	22.98	1.33	23.78
2.02	23.09	1.22	23.89

For Tie Points from E. Line of 1st
to W. Line of 3rd See P. 1

190	22.43
200 W.L. First	22.54
10	22.65
20	22.76
30	22.88
40	23.00
50	23.13
60	23.27
70	23.40
80 E.L. First	23.54

Continued on Page 20

345

923
43

13

0.78

1.58

23.09

9.22

27.31

1.90

3.99

3.76

3.53

3.26

2.99

23.21

23.32

23.43

23.55

23.66

23.78

23.91

24.05

24.18

24.32

24.32

gard

1.10

3.19

2.96

2.73

2.46

2.19

24.01

24.12

24.23

24.35

24.46

24.58

24.71

24.85

24.98

25.12

Grades - India - Arctic

282
932
354

869
382
1261

+86

+1.65

Grade	W of India	W.L. India	W. of W.L. India	869 of Arctic					
				972 301 12.73 HI 949 308 12.52 HI 798 406 12.09 HI 368 836 307 11.43 HI	972 d 296 12.68 HI 1563 11.51 11.24 8.285 3.205 12.190 8.24	4.15	8.58	3.35	938
20				798 406 12.09 HI 368 836 307 11.43 HI	1563 11.51 11.24 8.285 3.205 12.190 8.24	4.22	8.46	3.42	926
20				406 12.09 HI 368 836 307 11.43 HI	11.24 8.285 3.205 12.190 8.24	4.18	8.34	3.38	914
40				368 836 307 11.43 HI	8.285 3.205 12.190 8.24	3.97	8.22	3.17	9.02
50				836 307 11.43 HI	3.205 12.190 8.24	4.09	8.10	3.29	8.90
60				307 11.43 HI	12.190 8.24	4.21	7.98	3.41	8.78
75	W.L. India			512 328 11.43 HI	824 349 11.64	4.24	7.80	3.44	8.60
10	W. of W.L. India			328 11.43 HI	349 11.64	4.36	7.68	3.56	8.48
20				776 32 10.96 HI	788 329 11.17 HI	4.48	7.56	3.68	8.36
30				32 10.96 HI	329 11.17 HI	3.99	7.44	3.19	8.24
40						4.32	7.32	3.52	8.12
50						4.20	7.20	3.40	8.00
60						4.32	7.08	3.52	7.88
70						4.21	6.96	3.41	7.76
80						4.12	6.84	3.32	7.64
90						4.24	6.72	3.44	7.52
100						4.36	6.60	3.56	7.40
110						4.48	6.48	3.68	7.28
120						4.60	6.36	3.80	7.16
130						4.72	6.24	3.92	7.04

1195
03.595

1195
20
23900

5.07
22
483

392
15

+ .86 + 1.66

140		
150		
160		
170	Taper	
185	Beginning of wide section.	
185	" " wide "	
200		
210		
225		
228		
248		
270		
280		
290		
300		
310		
320		
330		
340		
350		

Grade
1.95 %

1

1096 HI
 $\frac{892}{371}$ 784
 $\frac{1081}{577}$ HI
 $\frac{322}{9.64}$ HI
 $\frac{923}{511}$ HI
 $\frac{457}{418}$ HI
 $\frac{970}{459}$ HI
 $\frac{875}{9.70}$ HI

133
 $\frac{559}{237}$ HI
 $\frac{830}{796}$ HI
 $\frac{457}{308}$ HI
 $\frac{965}{751}$ HI

4.84	6.12	4.04	6.92
4.80	6.01	4.00	6.81
4.92	5.89	4.12	6.69
5.04	5.77	4.24	6.57
3.45	5.59	2.65	6.39
3.63	5.41	2.83	6.21
3.94	5.29	3.14	6.09
4.12	5.17	3.32	5.91
4.63	5.07	3.83	5.77
3.92	4.83	3.12	5.63
3.39	4.57		5.37
3.51	4.45		5.25
3.63	4.33		
4.09	4.21		
4.21	4.09		
4.33	3.97	2.88	4.77
4.45	3.85	2.86	4.65
4.57	3.73	2.98	4.53
4.03	3.62	2.23	4.42

32.1
460.1
482.1

Last Stake on E of S Fe

~~3-no 45 E of N.~~

16

+86

+166

360	218 363 581 RT	(482.1 = Sta of. C.R. of E of.)	2.64	
370			2.52	
380			2.40	
390			2.28	
400			2.16	
410			2.04	
420			1.92	
430			1.80	
440			1.68	
450			1.56	0.56
460			1.44	0.44
470			1.32	0.32
480			1.20	0.20

765 HI

Grade drops
1' here -

4.15	3.50	335	430
4.27	3.38	347	418
4.39	3.26	359	406
4.51	3.14	371	394
4.63	3.02	383	382
4.75	2.90	395	370
4.87	2.78	407	358
4.99	2.66		
5.11	2.54		
	1.42		
	1.30		
	1.18		
	1.06		

Continued on P 21

aug. 23^d 1906

17

10.60 KI

Grade Top of	5.86	6.01	6.15	6.29
Cap	2.74	2.59	2.45	2.31

Rod

6.44	6.61	6.79
4.16	4.69	3.81

7				
6	4.11	0.48	single	cl.
5	4.02	0.43	"	6.49
4	3.93	0.38	"	
3	3.72	0.44	"	
2	3.76	0.33	"	
1	3.58	0.23	"	7.02

Cont. 2-2" below stake.

bottom of Column.

for 1" below Top of Column

Grade

+1.15

+5.42

Station	Direction	Track	St. Fe.	Grade	Dist.
482.1		Stay of C.R. (er) of S.T.	1.18		2.33
487.0	W	T.1 Hand track	0.18	1.12	5.27
497.0	E		0.12		
501.9	W	T.2 Main line	0.00	1.00	2.15
512.0	E		-0.06	0.94	2.09
516.9	W	T.3	-0.18	0.82	1.97
524.05	E		-0.28	0.77	1.92
528.95	W	T.4	-0.32	0.68	1.83
536.05	E		-0.38	0.62	1.77
540.95	W	T.5	-0.46	0.54	1.69
548.15	E		-0.52	0.48	1.63
553.05	W	T.6	-0.61	0.39	1.54
560.00	E		-0.66	0.34	1.49
564.90	W	T.7	-0.75	0.25	1.40
			-0.81	0.19	1.34

wharf track
 grade S.R. → 2.64
 of cap. 4.03 =
 3.97 W
 6.93 B.M.
 3.57
 10.60 H.E.
 3.97
 6.63

482.1
 2.36
 484.46

497
 2.36
 499.36
 484.46
 14.9

482.2
 47.5
 7.2
 2.5
 32.2

6.93 B.M.
 = 6'-4"
 2-8 1/2
 9-7 1/2
 2-8 1/2
 6-11 1/4
 7"
 1.8
 2'-3" (4th Trk below
 Grade stake =
 2'-4 1/2" 5th Trk.

84
 15
 99

84
 108
 2-6

27
 67
 94

99
 67
 61

112
 67
 79

218		2.33	2.27	2.15	2.09
246	HI	2.31	2.37	2.49	2.35
4.64		1.97	1.92	1.83	1.77

Continued from Page 13

457
63
3.94
67
27

285
20

24.32
13.8
30.70

+78

+158

EL 1 st	23.54
15	23.74
30	23.94
40	24.08
50	24.21
60	24.35
70	24.48
80	24.62
90	
100	24.89
110	
120	25.16
130	
140	25.43
150	
160	25.70
170	
180	25.97
190	
200	26.24

26.49
286
29.35 HI

24.32	25.12
+0.70	+1.33
6.26 24.44	5.63 25.07
24.64	25.27
5.92 24.78	5.29 25.41
24.91	
4.30 25.05	3.67 25.65
25.32	
4.03 25.32	3.40 25.95
25.59	
3.76 25.59	3.13 26.22
25.86	
4.84 25.86	4.21 26.49
26.13	
4.57 26.13	3.94 26.76
26.40	
4.30 26.40	3.67 27.03
26.67	
457 31.24 HI	
4.03 26.67	3.40 27.30
26.94	
3.76 26.94	3.67 27.57

Continued on P. 23

$\frac{3.29}{54}$ $\frac{3.29}{7.37}$
 Continued from P 16

$\frac{1.08}{4.37}$ $\frac{1.08}{6.58}$ $\frac{1.08}{6.58}$ $\frac{1.08}{1.66}$
 9/11/06 21

430		1.80
440		1.18
450	Beginning of Santa Fe	0.56
460	Nectar - 0.5 East	0.44
470		0.32
480		0.20
490		0.08
500		-0.04
510		-0.16
520		-0.28
530		-0.40
540		-0.51
550		-0.63
560		-0.75
570	End of Santa Fe	-0.88
580	Nectar - 0.5 West	-1.00
590		-1.12
600		-1.24
610		-1.35
620		-1.46
630		-1.58

$\frac{2.66}{1.76}$
 $\frac{1.50}{2.84}$
 $\frac{4.34}{4.34} HI$

	2.66	3.46		
	2.04	2.90		
✓	3.00	1.42	2.20	2.22
✓		1.30		2.10
✓	3.24	1.18	2.44	1.98
✓		1.06		1.86
✓	3.48	0.94	2.68	1.74
✓		0.82		1.62
✓	3.72	0.70	2.92	1.50
✓		0.58		1.38
✓	3.96	0.46	3.08	1.26
✓		0.35		1.15
✓	4.19	0.23	3.31	1.03
✓		0.11		0.91
✓	4.44	-0.02	3.56	0.78
✓		-0.14		0.66
✓	4.68	-0.26	3.80	0.54
✓		-0.38		0.42
✓	4.91	-0.49	4.03	0.31
✓		-0.60		0.20
✓	5.14	-0.72	4.26	0.08

640	-1.70
650	-1.82
660	-1.94
670	-2.06
680	-2.18
690	-2.30
700	-2.42
710	Santa fe section
720	Begin of grade
730	End of
750	Atlantic St line
775	End of Santa fe Ave
Outlet	-3.07
	-4.23

1.09	8.02	6.93
-3.37	2.07	
11.39	10.59	

9/11/06

372	294
210	210
1.62	84

442 HI		
434 HI	-0.84	-0.04
693	538 -0.96	4.50 -0.16
215	-1.08	-0.28
981	562 -1.20	4.74 -0.40
975	-1.32	-0.52
-0.74	5.86 -1.44	4.98 -0.64
284	-1.56	-0.76
+2.10 HI	6.10 -1.68	5.22 -0.88
	3.97 -1.80	3.17 -1.00
	4.13 -1.87	3.33 -1.07
770	4.28 -2.03	3.58 -1.23
	-2.21	-1.41
	3.37	-2.57

693 Spk. in end of 8x8' at South side of Water Tower.

Continued from P 20

WL 2 ^d	26.24
20	26.51
40	26.78
60	27.05
80 EL 2 ^d	27.34
20	27.61
40	27.88
60	28.15
80	28.42
100	28.70
120	28.97
140	29.24
160	29.51
180	29.78
200 WL 3 ^d	30.05
20	30.32
35	30.59
60	30.86
80 EL 3 ^d	31.14
15	31.34
40	31.68

31.24 HI
230

28.94

5.22

34.37 HI

50.53

67

51.10

76.1

42.49

5.54

48.02

12

36.03

0.55

36.58 HI

57.24 HI

4.30 26.94

4.03 27.21

3.76 27.48

3.39 27.75

3.20 28.04

2.93 28.31

5.79 28.58

5.52 28.85

5.25 29.12

4.97 29.40

4.70 29.67

4.43 29.94

4.16 30.21

3.89 30.48

3.62 30.75

5.56 31.02

5.39 31.29

5.02 31.56

4.74 31.84

4.47 32.11

4.21 32.38

+0.70

23
+1.33

3.67 27.57

3.40 27.84

3.13 28.11

2.86 28.38

2.57 28.67

2.30 28.94

5.16 29.21

4.89 29.48

4.62 29.75

4.34 30.03

4.07 30.30

3.80 30.57

3.53 30.84

3.26 31.11

2.99 31.38

4.73 31.65

4.74 31.84

4.39 32.19

4.11 32.47

4.57 32.67

4.21 33.01

+0.60

+L33

	Bottom grade		Rod, Centrigade	Rod	Side grade
60	31.95	36.58 HT 34.9	2.03	32.55	3.96 33.28
80	32.22	33.09 4.15	3.76	32.82	3.69 33.55
100	32.49	37.24 HT	3.49	33.09	3.42 33.82
120	32.76		3.22	33.36	3.15 34.09
140	33.02	35.17 3.54	3.62	33.62	2.89 34.35
160	33.30	38.71 HT	3.34	33.90	2.61 34.63
180	33.57		3.07	34.17	2.34 34.90
200 WLA ¹⁴	33.84		2.80	34.44	2.07 35.17
20	34.11	39.22 HT	4.00	34.71	3.27 35.44
40	34.38	36.53 39.5	3.73	34.98	3.00 35.71
60	34.65	40.48 HT	3.97	35.25	3.24 35.98
80 FLA ¹⁴	34.93		3.69	35.53	2.96 36.26
100	35.20		3.42	35.80	2.69 36.53
120	35.47	37.07 4.30	4.41	36.07	3.68 36.80
140	35.74	41.37 HT	4.14	36.34	3.41 37.07
160	36.02	37.34 4.30	3.86	36.62	3.14 37.34
180	36.29	41.6 HT	4.75	36.89	4.02 37.62
100	36.56		4.48	37.16	3.75 37.89
120	36.83	39.89 3.14	3.60	37.43	2.87 38.16
140	37.10	41.03	3.33	37.70	2.60 38.43
160	37.37		3.06	37.97	2.33 38.70

Side x Stake	2.54	Cr	2.54	Side x Stake	Bottom Grade
200	WL 5 ¹⁴				37.64
220					37.91
240					38.18
260					38.46
280					38.73
15		5948 BM SE.			38.93
40		6.63		6 ¹⁴ B	39.27
60		60.11 K			39.54
80		12.84			39.81
100		47.27			40.08
120		293			40.35
140		50.20			40.62
160					40.90
180					41.17
200	WL 6 ¹⁴				41.44
220					41.71
240					41.98
260					42.25
280					42.52
300	EL 6 ¹⁴				42.79
320					43.06

7.16 ft offset from Centre grade
(side line to Cr line) +0.60

Side grade +1.325

	Prod	Prod
38.70 3.2 41.82	3.58 38.24	2.85 38.97
38.97 3.97 42.94 KI	4.43 38.57	3.70 39.24
39.51 3.57 43.08 KI	4.16 38.78	3.43 39.57
	4.02 39.06	3.29 39.79
	3.75 39.33	3.02 40.06
40.26 3.58 43.84 KI	3.55 39.53	2.82 40.26
	3.97 39.87	3.24 40.60
316 40.87 44.03 KI	3.70 40.14	2.97 40.87
	3.62 40.41	2.89 41.14
41.68 3.43 45.11 KI	3.35 40.68	2.62 41.41
	3.08 40.95	2.35 41.68
50.20 KI 42.50 3.60 46.10	3.89 41.22	3.16 41.95
4304 3.61 46.65	3.68 41.50	2.88 42.23
	3.43 41.77	2.70 42.50
43.31 3.58 46.89 KI	4.06 42.04	3.33 42.77
	3.79 42.31	3.06 43.04
	4.07 42.58	3.34 43.31
	4.04 42.85	3.31 43.58
	3.77 43.12	3.07 43.85
	3.50 43.39	2.77 44.12
	3.23 43.66	2.50 44.39

+60

+1.33

60	43.33
80	43.60
100	43.87
120	44.14
140	44.41
150	44.50
160	44.68
170	44.87
180	44.95
200 W.L. 7 th	45.23
20	45.50
40	45.77
60	46.04
80 E.L. 7 th	46.32
20	46.59
40	46.86
60	47.13
80	47.40
100	47.67
120	47.94
140	48.21
160	48.48
180	48.75

44.29 3.95	3.95	43.93	3.22	44.66
47.88 52.76 H.E.	3.68	44.20	2.95	44.93
45.01 8.03	18.29	44.47	17.56	45.20
53.04	18.02	44.74	17.29	45.47
52.73 H.E.	7.11	45.01		45.74
	17.90	45.14	7.17	45.97
	17.32	45.28		46.01
		45.41	6.59	46.14
		45.55		46.28
	16.90	45.83	16.18	46.55
		46.10		46.83
	16.35	46.37	5.63	47.10
46.87 4.79	4.52	46.64	3.79	47.37
51.16 H.E.	4.24	46.92	3.51	47.65
	3.97	47.19	3.24	47.92
	3.70	47.46	2.97	48.19
	3.43	47.73	2.70	48.46
	3.16	48.00	2.43	48.73
49.00 3.35	2.89	48.27	2.16	49.00
52.35 H.E.	3.51	48.54	3.08	49.27
56.73 H.E.	3.54	48.81	2.81	49.54
	3.27	49.08	2.54	49.81
	1.68	49.35	6.15	50.08

side 0
940

229

side 10
540

229

side 20
540

6.91' from side line to center

40.6

27
1133

200' WL 8th

+20
+40
+60

+80' EL 8th

+10
+40
+50
+60
+80
1+00
+20
+40
+60
+70
+80

2+00' WL 9th

+20
+40
+60

00'+80' EL 9th

+30

49.02
49.29
49.56
49.83
50.11
50.24
50.65
50.92
51.19
51.46
51.73
52.01
52.28
52.55
52.82
53.09
53.36
53.63
53.91
54.31

56.23/47

50.16
42.9
54.45 M

50.84
42.7
55.1.1 M
59.30 M

52.33
3.63
55.96 M

57.24 M

53.69
42.6
57.95 M

6.61 49.62
6.34 49.89
6.07 50.16
4.02 50.43
3.74 50.71
3.61 50.84
3.86 51.25
3.73 51.38
7.51 51.79
7.24 52.06
6.97 52.33
3.25 52.61
3.08 52.88
2.96 53.07
3.82 53.42
3.55 53.69
3.99 53.96
3.72 54.23
3.44 54.51
3.04 54.91

5.88 50.35
5.61 50.62
5.34 50.89
3.29 51.16
3.01 51.44
2.88 51.57
3.13 51.98
3.00 52.11
52.25
16.78 52.52
16.51 52.79
16.24 53.06
2.62 53.34
2.35 53.61
2.21 53.75
53.88
3.09 54.15
2.82 54.42
13.24 54.69
12.99 54.96
2.71 55.24
12.81 55.64

586 = 86' No B

106

126

146

166

186

206

226

246

266

286

300 - SLA

320

340

360

380 - SLA

400

420

440

460

480

57.67

57.99

58.31

58.63

58.95

59.26

59.58

59.90

60.22

60.50

60.77

60.96

61.23

61.50

61.67

61.94

62.21

62.48

62.75

63.02

63.30

$$\begin{array}{r} 6123 \\ 376 \\ \hline 6499 \end{array}$$

$$\begin{array}{r} 6210 \\ 372 \\ \hline 6582 \\ 6137 \\ \hline 6919 \end{array}$$

$$\begin{array}{r} 376 \\ 376 \\ \hline 752 \end{array}$$

62.73 141

$$\begin{array}{r} 57.23 \\ 62.23 \\ \hline 119.46 \end{array}$$

64.99 HI

65.83 HI

67.17 141

	70.6		71.33
	58.27	3.73	59.00
	58.59	3.41	59.32
	58.91	3.09	59.64
3.50	59.23	2.77	59.96
	59.55	1.95	60.28
	59.86	1.64	60.59
	60.18	1.32	60.91
1.73	60.50	1.00	61.23
	60.82	3.44	61.55
	61.10	3.16	61.83
3.62	61.37	2.89	62.10
	61.56	3.54	62.29
	61.83	3.27	62.56
5.11	62.00	4.44	62.73
	62.27	4.17	63.00
	62.54	3.90	63.27
	62.81		63.54
	63.08	3.36	63.81
	63.35	3.09	64.08
	63.62	2.82	64.35
3.27	63.90	2.54	64.63

500

520

540

560

580

600

620 = B.C.

630.5

641.0

651.5

662.0

672.5

683.0

693.5

707.5 = E.C.

727.5

747.5

759.5 = B.C.

770.0

780.5

791.0

63.57

63.84

64.11

64.38

64.65

64.92

65.20

65.44

65.68

65.93

65.87

66.01

66.15

66.29

66.48

66.75

67.02

67.18

67.32

67.46

67.60

$$\begin{array}{r} 63.90 \\ 5.95 \\ \hline 69.85 \text{ M} \end{array}$$

71.91 M

$$\begin{array}{r} 65.90 \\ 4.67 \\ \hline 70.57 \text{ M} \end{array}$$

71.82 M

+06

+1.03

64.17 4.95 64.90

64.44 4.60 65.17

64.71 4.41 65.44

64.98 4.14 65.71

65.25 4.92 65.98

65.52 4.65 66.25

65.90 4.27 66.63

66.04 3.80 66.77

66.18 3.66 66.91

66.33 3.51 67.06

66.47 3.37 67.20

66.61 3.23 67.34

66.75 3.09 67.48

66.89 2.95 67.62

67.08 2.76 67.81

3.74 68.08

3.47 68.35

3.31 68.51

3.17 68.65

3.03 68.79

2.89 68.93

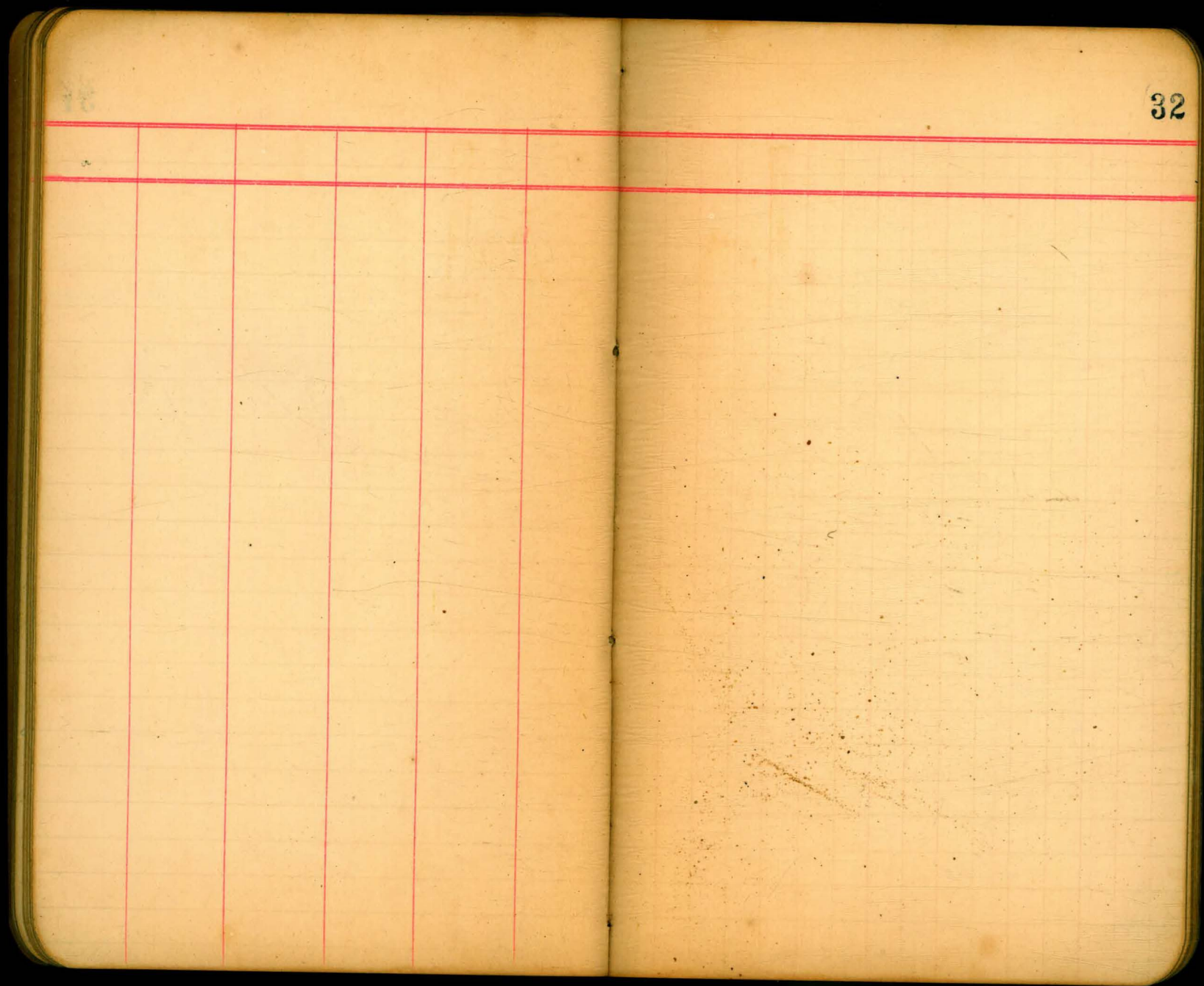
801.5	67.75
812.0	67.89
819 = E.C. Face Inlet.	68.00

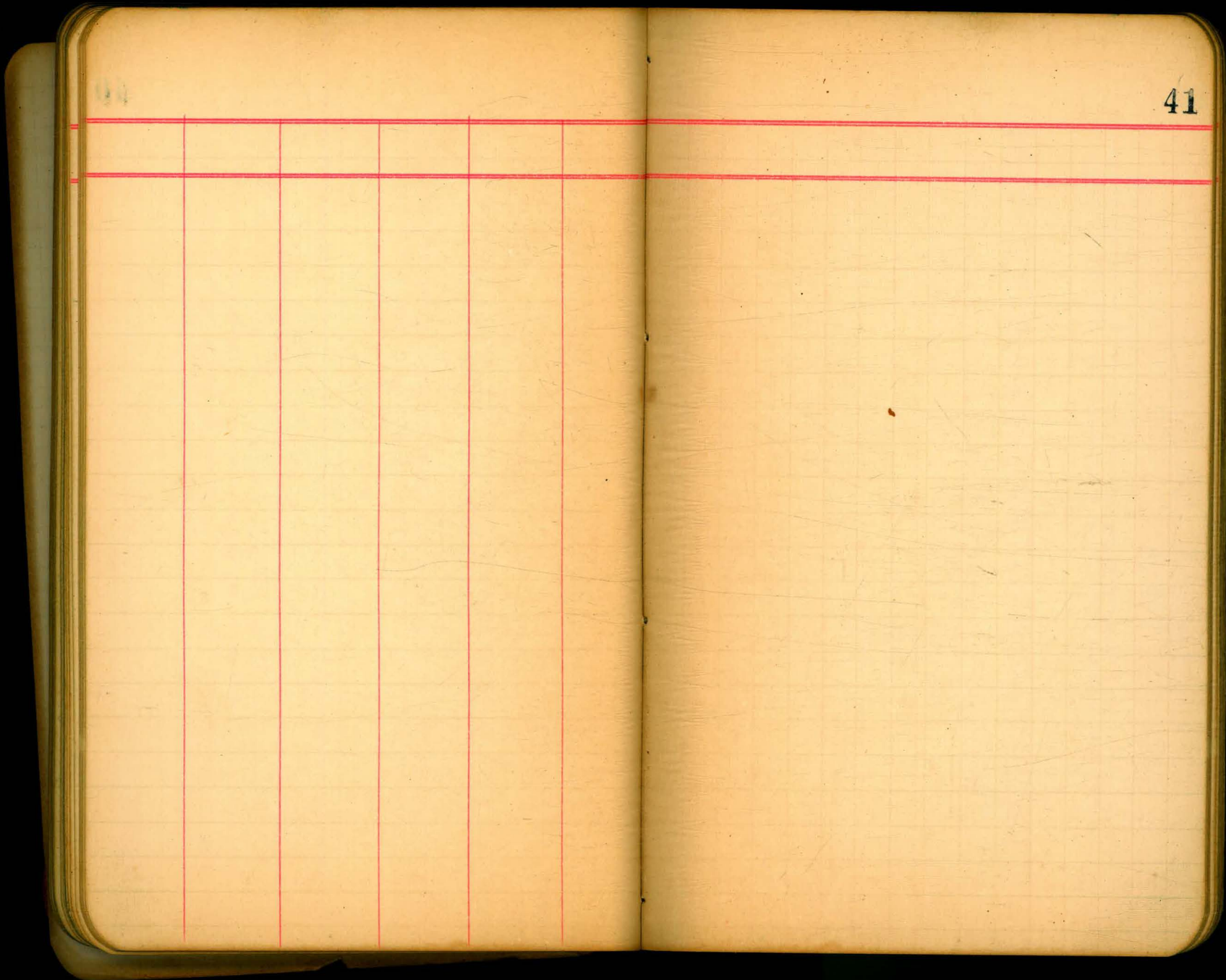
71.82 MG.	3.47	68.35	12.74	69.08
12.05				69.22
0.40				
83.30				
11.21	9.92	68.60	9.19	69.33
72.15				
6.39				
78.52 MG				

+0.6

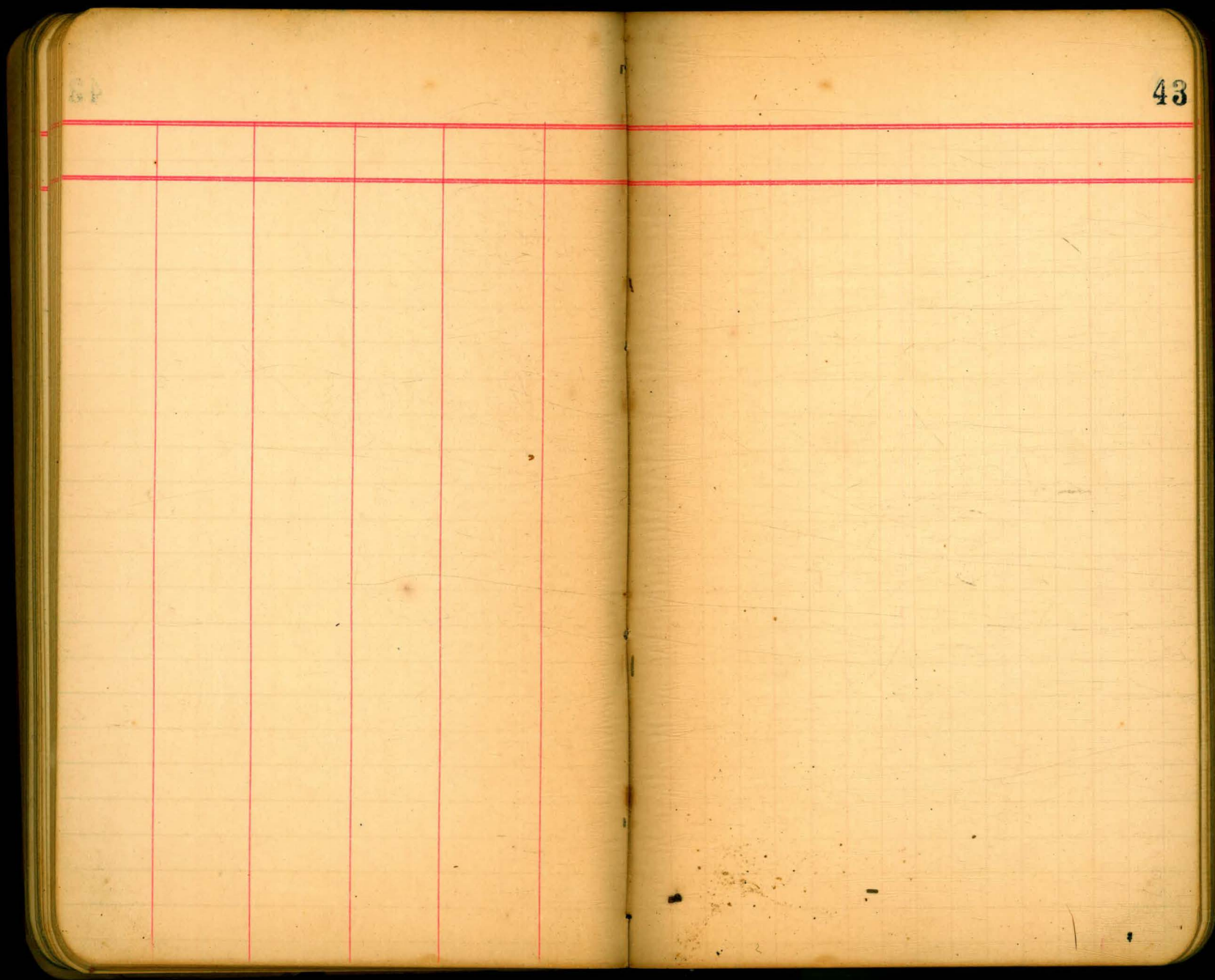
+1.33

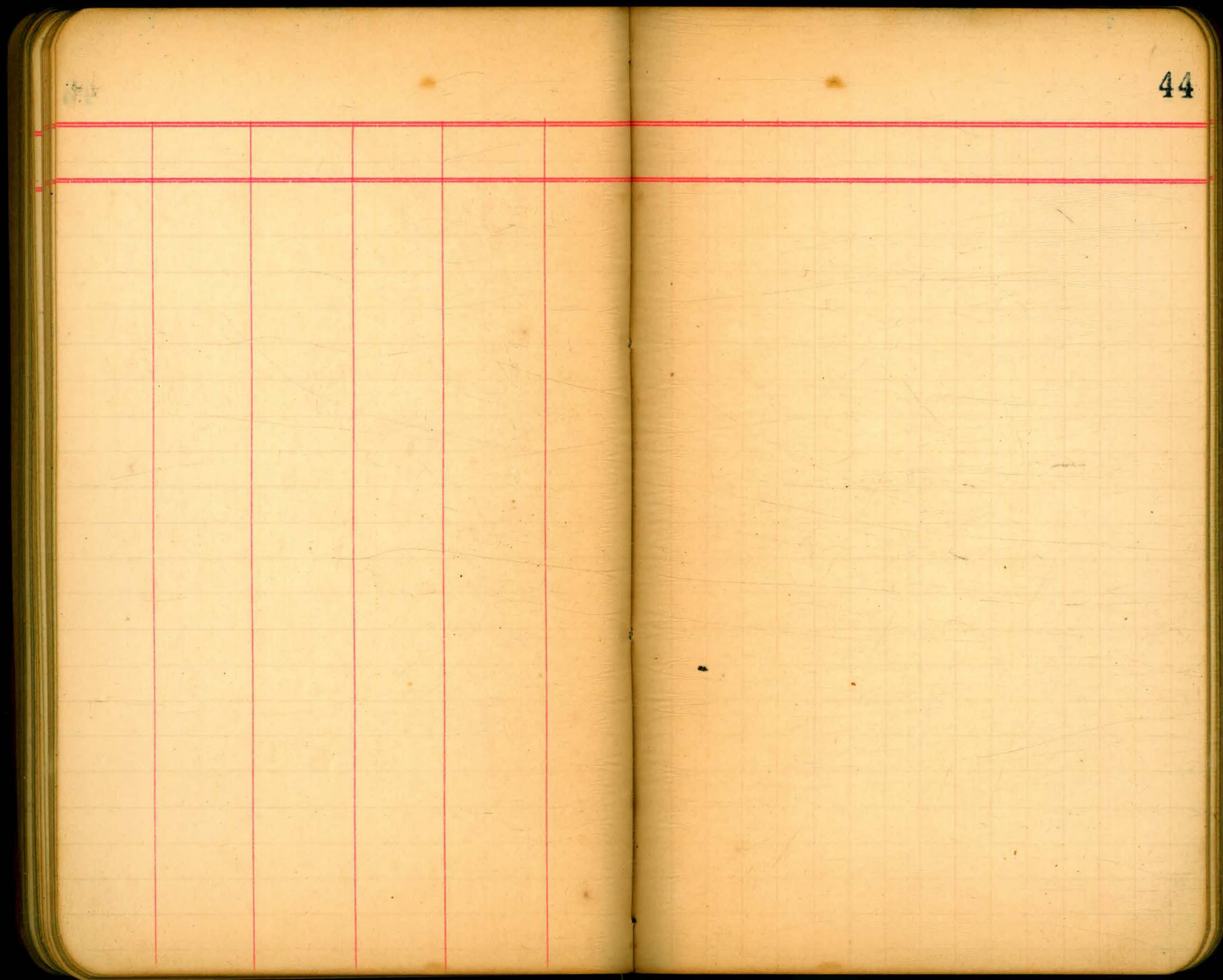
69.23
632
6.12
2.23
4.89

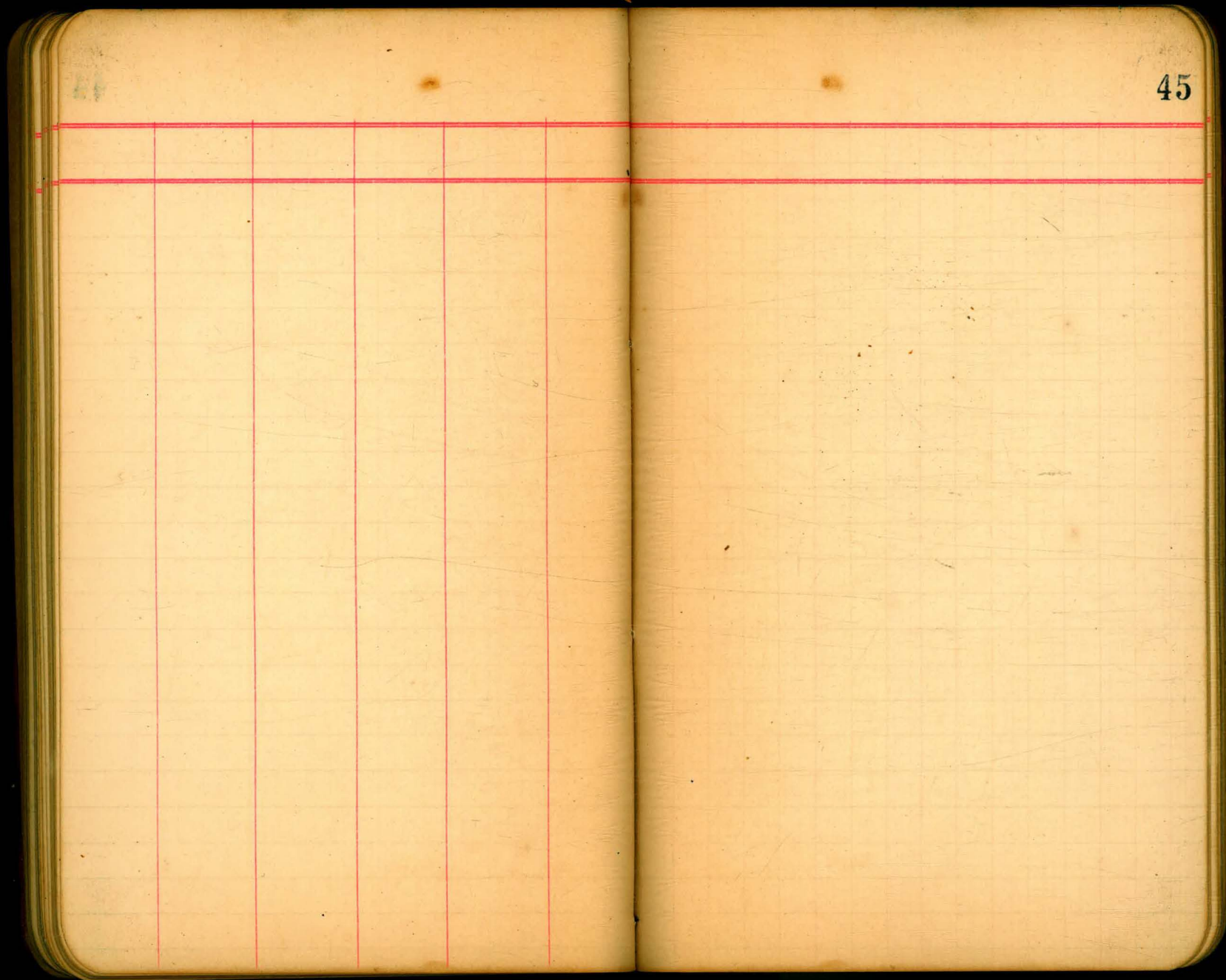


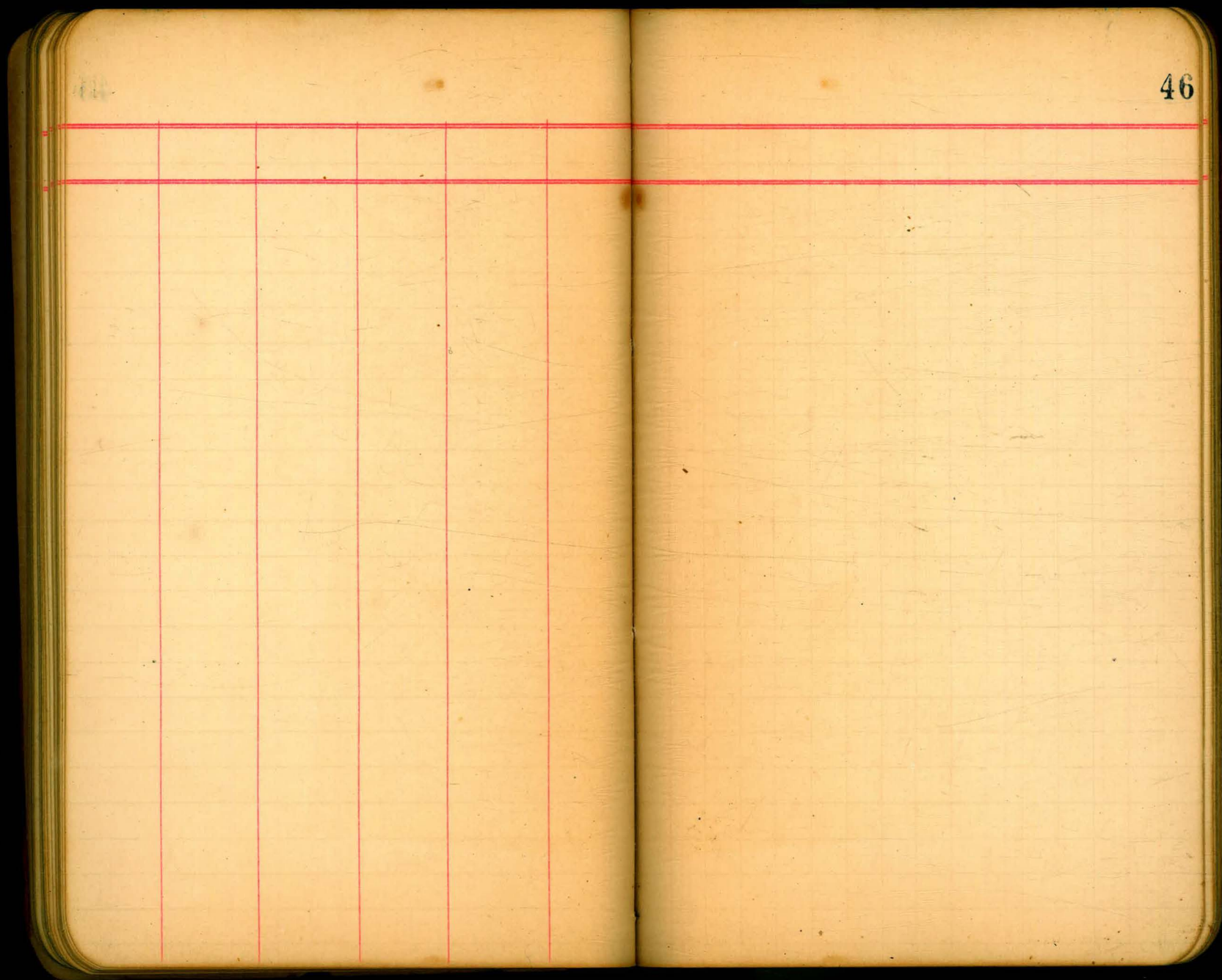


The image shows an open notebook with two pages. The left page is a ledger page with a grid of red lines. It has two horizontal lines near the top, creating a header section. Below these, there are five vertical lines that divide the page into six columns of varying widths. The right page is a grid page with a uniform grid of red lines. The number '42' is printed in the top right corner of the right page. The paper is aged and yellowed, with some minor stains and wear.

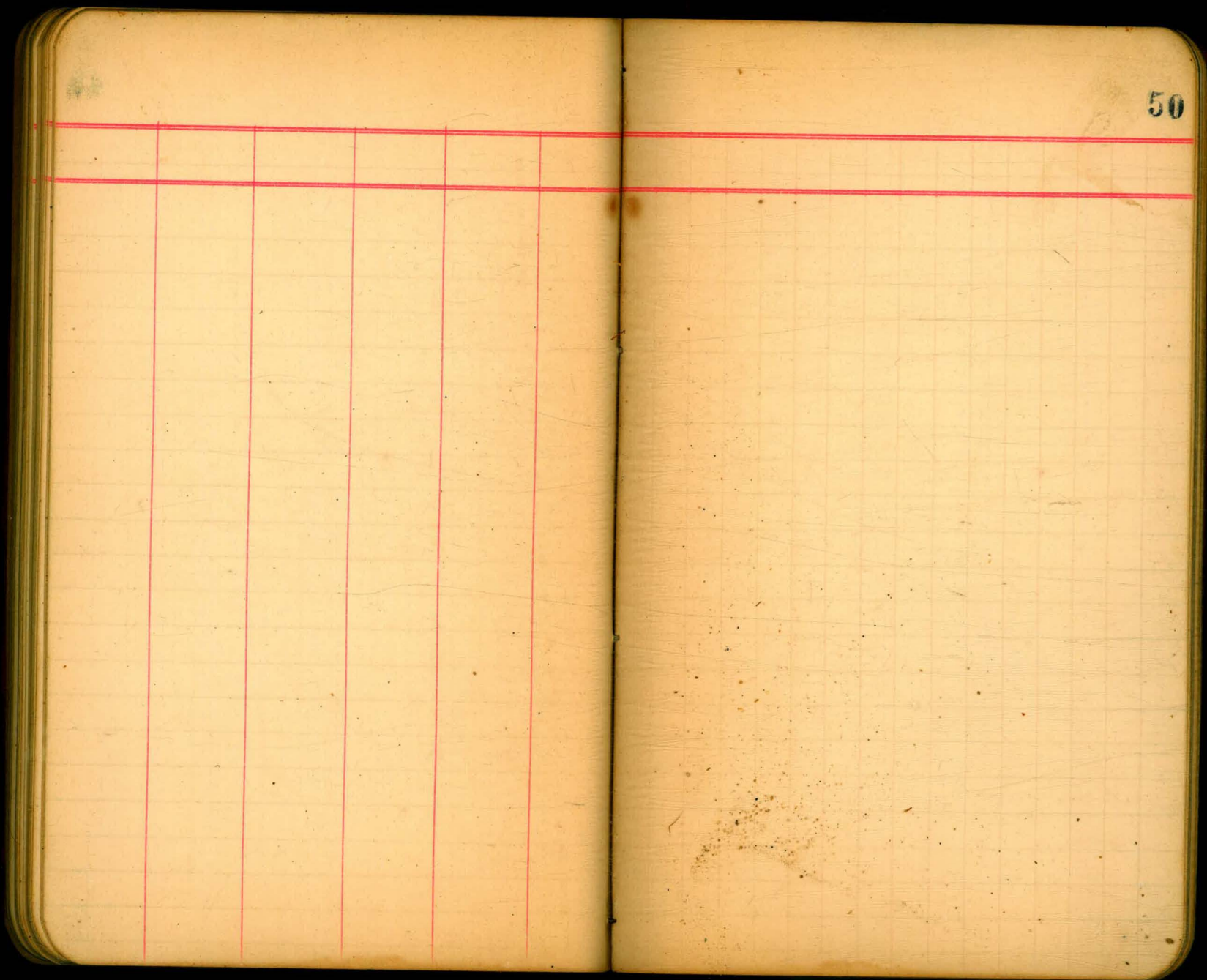








47



The image shows an open notebook with two pages. The left page is a ledger page with a grid of red lines. It has two horizontal lines near the top, creating a header section. Below these are six vertical lines that divide the page into seven columns of varying widths. The right page is a grid page with a uniform grid of red lines. The number '51' is printed in the top right corner of the right page. The notebook has a dark cover, and the pages are a light cream color.

Cuts from spikes on Santa Fe.
tracks to bottom of trench

7/27/06 from
Boston

8.70
- 3.95

8.60
+ 7.05

12.65
6.93
5.72

54

Sta	d.	Sta	Grade	Cut
4+88	3.73 3.92 72.65	4+40 3.95	8.70 + 0.11	8.59
5+04		4.05	8.60 - 0.08	8.68
5+18		3.77	8.88 - 0.25	9.13
5+30		4.00	8.65 - 0.39	9.04
5+42		4.15	8.50 - 0.53	9.03
5+54		4.22	8.43 - 0.67	9.10
5+66		4.48	8.17 - 0.82	8.99

Santa Fe.

$\frac{666}{-081}$
5.85

$\frac{666}{18}$
6.84

55

	10.95				
BE	9.11	1.84	El Cap 6.84	5'	
NV.	10.10	0.85	5.85	5'	
720	+4.55	-2.66	7.21		
740	+3.74	-2.81	6.55		
750.6	+2.45	-2.89	6.34		
70	+2.44	-3.04	5.48		

below top of Cap -

402

693

1095 HI

Base W of E = 7.9

306 grade = $\frac{+0.18}{7.7}$

Base W of W. 7.10

Grade $\frac{-0.81}{7.91}$

$\frac{285}{7.10}$

460 144 0.44

Wharf tracks

E $\frac{6.8}{7.15}$ el.

480 120 0.20

grade 718 $\frac{-2.64}{6.77}$ cut

500 096 -0.04

W $\frac{6.5}{4.45}$ el.
grade 718 $\frac{-2.70}{7.15}$ cut

520 072 -0.28

ER. ET.
el. = 7.9
grade = $\frac{+0.18}{7.7}$ cut.

540 049 -0.51

WR WT
d. = 7.10
grade = $\frac{-0.81}{7.9}$ cut

560 025 -0.75

580 0.01 -1.0

600 -0.22 -1.22

Santa Fe Tracks

Grade to Top of Cap
= 6.67
for 4" Clearance

633

33

6.66

56

620 -0.46 -1.96

$\frac{-0.1195}{20}$
 $\frac{0.23900}{0.3585}$

640 -0.70 -1.70

660 -0.94 -1.94

$\frac{1.22}{0.55}$
1.90

680 -1.18 -2.18

700 -1.42 -2.42

$\frac{2-6}{11}$
 $\frac{6-4}{11}$
0.18
grade to top of wharf $\frac{6.33}{6.51}$

720 -1.66 -2.66

1095 HI

740 -1.90 -2.81

E of E -
W of W -

760 -2.03 -2.89

E -
W -

775 level, V $\frac{+3.07}{1.54\%}$
850.6 outlet V $\frac{+4.23}{1.54\%}$

La Jolla Tracto ¹⁷ 20

		16.505		$\begin{array}{r} 12.64 \\ 3.865 \\ \hline 16.505 \text{ HI} \\ 4.86 \\ \hline 11.645 \end{array}$	
1	2	3	4	5	6
$\frac{9.623}{6.882}$	$\frac{9.567}{6.938}$	$\frac{9.481}{7.027}$	$\frac{9.935}{7.080}$		
12.64 E.L. Arctic					
$\frac{12.64}{3.42}$ HI					
16.06					
ET		CT		WT	
E W		E W		E W	
N. S		N. S		N. S	
$\frac{3.91}{12.15}$	$\frac{4.24}{11.82}$	$\frac{3.89}{12.17}$	$\frac{4.22}{11.84}$	$\frac{3.98}{12.08}$	$\frac{4.32}{11.74}$
$\frac{11.82}{11.52}$	$\frac{11.82}{11.52}$	$\frac{11.84}{11.52}$	$\frac{11.84}{11.52}$	$\frac{11.74}{11.52}$	$\frac{11.74}{11.52}$
$\frac{11.52}{11.985}$	$\frac{11.52}{11.985}$	$\frac{11.52}{11.985}$	$\frac{11.52}{11.985}$	$\frac{11.52}{11.985}$	$\frac{11.52}{11.985}$
$\frac{11.985}{9.623}$	$\frac{11.985}{9.623}$	$\frac{11.985}{9.623}$	$\frac{11.985}{9.623}$	$\frac{11.985}{9.623}$	$\frac{11.985}{9.623}$
$\frac{9.623}{2.362}$	$\frac{9.623}{2.362}$	$\frac{9.623}{2.362}$	$\frac{9.623}{2.362}$	$\frac{9.623}{2.362}$	$\frac{9.623}{2.362}$
$\frac{2.362}{8.67}$	$\frac{2.362}{8.67}$	$\frac{2.362}{8.67}$	$\frac{2.362}{8.67}$	$\frac{2.362}{8.67}$	$\frac{2.362}{8.67}$
$\frac{8.67}{1.69}$	$\frac{8.67}{1.69}$	$\frac{8.67}{1.69}$	$\frac{8.67}{1.69}$	$\frac{8.67}{1.69}$	$\frac{8.67}{1.69}$
$\frac{13.64}{4.25}$ HI		$\frac{9.34}{7.55}$		$\frac{9.28}{7.61}$	
16.59					

St. top of Column

57

4.203 + 5.42 = 9.623 E	} E. Track.
4.147 " = 9.567 W	
4.061 " = 9.481 E	} Cr. "
4.005 " = 9.425 W	
3.919 " = 9.339 E	} YX "
3.863 " = 9.283 W	

From India - Bay -

6/28/06 Hatch
minutes

47.5

58

731
39
9

2.2
1.2
3.4

			elv.	Grade	cut.
	1.42	20.05	18.63		
E. L. India				7.83	9.47
15			30.1	17.04	7.65
35			3.24	16.81	7.42
55			3.90	16.59	7.18
75 W. L. India			3.95	16.10	6.94
20			4.26	15.99	6.70
40			4.72	15.33	6.46
60			5.09	14.96	6.22
80			5.49	14.56	5.98
100			5.88	14.17	5.74
120			6.24	13.81	5.50
140			6.63	13.42	5.26
160			7.01	13.04	5.03
170	5.215	14.95	7.22	12.83	4.91
"	N		1.80	13.18	4.91
185			1.95	13.03	4.75
200	E h. Arctic		2.34	12.64	4.55
220			2.90	12.02	4.31
240			2.74	12.24	4.07
260			3.34	11.64	3.83
280			3.91	11.57	3.59

1.1957 1863 - Bay

11.64
5.50
17.14 HI
5.30
11.84 el
3.95 grade
7.89 cut
7.10 1/2

383
12
3.95 grade

Bottom grades
under rails
of La Jolla
Ry.

E

4.31
4.107
4.203 - 1st R
0.56
4.147 - 2d R
0.16
4.061 - 1st R
0.56
4.005 - 2d R
0.86
3.919 - 1st R
0.56
3.863 - 2d R

W

8' of track
bet tracks
w of tracks

24.6
21.6
3.0

		1498				
300			3.72	11.26	3.35	7.91
350			4.17	10.81	3.11	7.70
400			4.91	10.57	2.87	7.68
360			4.77	10.21	2.64	7.56
380			5.15	9.83	2.41	7.42
400			5.76	9.52	2.16	7.35
420			5.79	9.19	1.92	7.26
440			6.25	8.73	1.68	7.04
460			6.46	8.52	1.44	7.07
480			7.19	7.79	1.20	6.58
T.P.	2.71	10.45	6.94	8.04	0.96	7.07
500			2.41	8.04	0.96	7.07
520			2.54	7.91	0.72	7.18
540			3.02	7.43	0.49	6.93
560	stake beside rail				0.25	
580			3.89	6.56	0.08	6.54
600			4.06	6.39	-0.22	6.61
620			4.39	6.06	-0.46	6.52
640			4.94	5.51	-0.70	6.21
660			5.20	5.25	-0.94	6.19
680			5.42	5.03	-1.18	6.21
800			5.96	4.49	-1.42	5.91

.01195
1.88
9.560
5.975
1.195
0.188810

Grade of bottom at 2" pipe
= 1.22

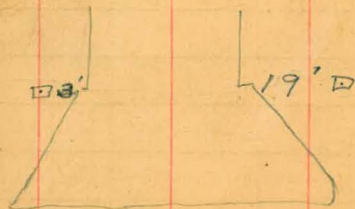
0-11" Invert
4-6" Clear
1" Base I 12"
2 1/2" Photo

4-20 1/2 1.22
5-8 1/2 5.71
5.71 6.93 El bottom 2" Pipe

6.93 B.M.
4.06
10.99
4.02
6.97 El of nails for bottom 2" Pipe

244
 5.37
 7.81 HI

		10.45			
720		5.90	4.55	-1.66	6.21
740		6.71	3.74	-1.90	3.60
750	E.L. Atlantic	7.00	3.45	-2.03	5.98
20	(+24.5 Cr Sewer)	8.01	2.44	-2.27	4.71
B.C.	Spk in Water Tower	3.52	6.93		
T.P.	11.15	17.31	2.29	8.16	
check		0.68	18.63	7.863	
40		7.81		-2.51	
60		6.38	1.43	-2.75	
80				-2.99	
100	W.L. Atlantic			-3.23	



121
 139
 300
 - 3.31
 86
 - 2.45

480
 750
 3000
 705
 2000
 19.50
 20.00
 12.2

15
 64
 7.6
 60

986
 746
 - 240 al of sewer -
 240 - 2.45 grade
 16
 259

2.66 HI

25' E = Sewer

30' 11.2

40' 12.4 N 5.25
 12.8 S 17.95 S 12.8

60' 11.1, 5/3 15.9, S. 10.4

70' Cr. 12.5 S. 10.7 N. 9.8

4.18 80' Cr. 11.0 N. 10.6 S. 13.0

90' 11.8 Cr. 10.3 S. 10.9

100' Cr. 11.6 S. 11.0 S. Wing - 8.6

30 - 7.2 Q. surface - 4.6

50 - 7.2 - 4.6

100 - 7.3 - 4.9

7/30/06
 Bottom Only

5/28/06

from P.C.

61

sta.	+	HI	-	Slev.	Grade	cut
	393	40.82		36.59		
W. L. Union			5.46	35.36	16.35	19.01
27			4.79	36.63	14.66	19.37
47			4.81	36.01	16.88	19.13
67 E. L. Union			5.28	35.54	17.11	19.43
15			5.28	35.54	17.28	19.26
40			5.12	35.70	17.57	18.13
60			5.30	35.52	17.79	17.73
80			5.15	35.67	18.02	17.65
100			5.10	35.72	18.25	17.47
120			5.01	35.81	18.47	17.34
140			4.92	35.90	18.70	17.20
160			4.85	35.94	18.93	17.01
180			4.76	36.06	19.15	16.91
197 W. L. Front (Angle Left)			^{4.68} 4.14	36.14	19.36	16.78
20			4.14	36.68	19.59	17.09
40			4.14	36.68	19.51	16.87
60			4.11	36.71	20.77	16.67
80 E. L. Front			4.57	36.25	20.27	15.98
100			4.67	36.15	20.19	15.76

4052
506
3576 } chub.
3576

3735
23
16

62

	+	HI 40.82	-	Elev.	Grade	Cut.
120			4.65	36.17	20.72	15.45
140			4.65	36.17	20.95	15.22
160			4.60	36.22	21.17	15.05
180		41.02	4.46	36.36	21.20	14.96
200			4.42	36.60	21.63	14.97
220			4.35	36.67	21.86	14.81
240			4.38	36.64	22.05	14.56
260			4.11	36.91	22.31	14.60
280	Wk First		4.15	36.87	22.54	14.33
300			3.52	37.50	22.76	14.74
40 cr. First st.			3.20	37.82	23.00	14.82
60			2.71	38.31	23.27	15.03
80	E L First	44.97	3.07	37.95	23.54	14.40
100			3.07	38.15	23.74	14.41
120			6.59	38.38	24.08	14.30
140			6.10	38.87	24.35	14.52
160			5.86	39.11	24.62	14.49
180			5.49	39.48	24.89	14.59
200			5.21	39.76	25.16	14.60
220			4.71	40.26	25.43	14.83
240			4.26	40.71	25.70	15.01

13.55% Rate of

962
4591

2656
899

22.57
10.97

	N.I. 44.97				
180		4.15	40.82	25.97	14.85
200-W.L. 2d		3.94	41.03	26.24	14.79
220		3.74	41.23	26.51	14.72
240-Cr		3.39	41.58	26.78	14.80
260		3.16	41.81	27.05	14.76
280-E.L. 2 ^d -0+00		2.89	42.08	27.34	14.74 ✓
20		2.66	42.31	27.61	14.70
40		2.35	42.62	27.88	14.74
60		2.08	42.89	28.15	14.74
80		1.92	43.05	28.42	14.63
100		1.57	43.40	28.70	14.70
120		1.25	43.69	28.97	14.72
140		1.13	43.84	29.24	14.60
160		0.70	44.27	29.51	14.75
180 Bm 4 th B.	5135	0.62	44.35	29.78	14.57
200-W.L. 3d	55.49 NI 55.49	0.40	44.57	30.05	14.52
20		10.83	44.66	30.32	14.34
40		10.71	44.78	30.59	14.19
60		11.07	44.98	30.86	13.62
80 = E.L. 3 ^d *		10.01	45.48	31.14	14.34
15		9.75	45.74	31.34	14.40 ✓

8/9/06

B.M. on Hydrant at NW Cor
of 4th & 18th Streets is incorrect

64

5549

40		9.27	46.22	31.68	14.54
60		8.82	46.67	31.95	14.72
80		8.34	47.15	32.22	14.93
100	✓	7.71	47.78	32.49	15.29
120		7.03	48.46	32.76	15.70
140		6.50	48.99	33.02	15.97
160		5.97	49.52	33.30	16.22
180		5.49	50.00	33.57	16.43
200	WL 4 th X	4.96	50.53	33.84	16.69
220		5.66	49.83	34.11	15.72
240		5.34	50.15	34.38	15.76
260		5.66	49.83	34.65	15.18
280	EL 4 th	4.96	50.53	34.93	15.60
300		4.61	50.88	35.20	15.68
320		4.39	51.10	35.47	15.63
340		3.93	51.56	35.74	15.82
360		3.53	51.96	36.02	15.94
380		3.04	52.45	36.29	16.16
400		2.63	52.86	36.56	16.30
420		2.90	52.59	36.83	15.76
440		1.80	53.69	37.10	16.59

5459
0.98

50.53
4.69
55.22
11.64
43.58
0.36
43.94

60.53
5.04
55.57

16.69
7.33
9.36

1	15.60	
4.72	50.85	15.65
4.60	50.97	15.50
3.96	51.61	15.87
3.76	51.81	15.79
3.07	52.50	16.21
2.72	52.85	16.29
2.62	52.95	16.12
1.94	53.53	16.43

5549
5377

8
6327
921
33.79

5554 N.H.
5549 - Davis. Hwy.
5-5557 - SW H.H.
6-5948 - SE N.H.

9.1
59.37

15

5549

5557

460			1.51	53.98	37.37
480	WL 5 th	x	1.03	54.46	37.64
500			1.55	53.94	37.91
520			1.19	54.30	38.18
540	5 th B ^d	5557	1.72	53.77	38.46
560	EL 5 th	63.67 HI	0.90	54.59	38.73
15			9.08	54.59	38.93
40			8.65	55.02	39.27
60			8.26	55.41	39.54
80			7.77	55.90	39.81
100			8.10	55.57	40.38
120			7.18	56.19	40.35
140			6.85	56.82	40.62
160			6.48	57.19	40.90
180			6.24	57.43	41.17
200	WL 6 th		5.67	58.00	41.44
220			5.36	58.31	41.71
240			5.16	58.51	41.98
260			5.16	58.51	42.25
280	on cement. EL 6 th	x	5.16	58.51	42.52
290			5.15	58.52	42.65

16.11	1.65	53.92	16.65
16.82	1.13	54.44	16.80
16.03			
16.12			
15.31			
15.86			
15.66	8.38	54.64	
15.85	7.96	54.96	
15.87	7.56	55.36	
16.09	7.15	55.77	
15.49	7.34	55.58	
15.84	6.71	56.21	
16.20	6.67	56.85	
16.29	5.74	57.18	
16.26	5.51	57.41	
16.56			
16.60			
16.53			
16.26			
15.99			
15.87			

54.59
833
6272

4118

15.5

5

6367

310		5.16	58.51	42.90	15.61
330		4.80	58.89	43.19	15.68
350		4.54	59.13	43.46	15.67
370		4.43	59.24	43.73	15.51
390		4.24	59.43	44.00	15.43
410		4.03	59.64	44.27	15.37
430		3.68	59.99	44.54	15.45
450		3.52	60.15	44.81	15.34
470		3.30	60.37	44.95	15.42
480	WL 7 ^m X	3.18	60.49	45.23	15.26
500		2.28	61.39	45.50	15.89
520		1.59	62.08	45.77	16.31
540		1.80	61.87	46.04	15.83
560	EL 7 ^m 67.75	2.13	61.54	46.32	15.22
580		6.35	61.40	46.59	14.81
600		6.24	61.71	46.86	14.85
620		6.08	61.67	47.13	14.54
640		5.70	62.05	47.40	14.65
660		5.41	62.34	47.67	14.67
680		5.22	62.53	47.94	14.59
700		5.05	62.70	48.21	14.49
720		4.91	62.84	48.48	14.36

54.59
276
57.35
805
49.30
Bulto grande 40
9.30
7.23
2.05
7.9
1.30

El Topo
Luz

Bulto grande

828
69.60
67.75
3.75

67.75

740			4.56	63.19	48.75	14.44
760	WL 8 ^m	X	4.36	63.39	49.02	14.37
780			3.70	64.05	49.29	14.76
800			3.24	64.51	49.56	14.95
820			3.28	64.47	49.83	14.64
840	EL 8 ^m		3.20	64.55	50.11	14.44 ✓
10			3.15	64.60	50.24	14.36
20			3.00	64.75	50.38	14.37
40			2.58	65.17	50.65	14.52
60			2.38	65.37	50.92	14.45
80			1.98	65.77	51.19	14.58
100			1.60	66.15	51.46	14.69
120			1.30	66.45	51.73	14.72
140			1.08	66.67	52.01	14.66
160	577	72.85	0.67	67.08	52.27	14.80
180			5.52	67.33	52.55	14.78
200	WL 9 ^m	X	5.19	67.66	52.82	14.84
220			5.05	67.80	53.09	14.71
240			4.84	68.01	53.36	14.65
260			4.68	68.17	53.63	14.54
280	EL 9 ^m		4.80	68.05	53.91	14.14

70.93
7.27
77.20
1.35
10th = 76.85 club

76.85

LL

72.14

6.54
5

72.85

300	Grades	5.57	67.28	54.18	13.10
310	54.81		³⁺¹⁰ break 54.81		
320		5.76	67.09	54.25	12.64
340	54.65	5.66	67.19	54.72	12.47
360	54.87	5.38	67.47	55.00	12.47
380	55.10	5.18	67.67	55.27	12.40
400	55.32	3.56	69.29	55.54	13.75
420	55.54	3.24	69.61	55.81	13.80
431 BC	55.67	3.58	69.27	55.96	13.31
441.8	55.79	3.25	69.60	56.11	13.49
453.6	55.91	3.32	69.53	56.25	13.28
464.7	56.03	2.57	70.28	56.40	13.88
475.2 7.27	56.15	1.92	70.93	56.54	14.39
486.0	56.27	6.58	71.32	56.69	14.63
496.8	56.40			56.84	
507.6	56.51	7.24	70.96	56.98	13.98
518.4	56.64	7.03	71.17	57.13	14.04
529.2	56.77	6.77	71.43 ^{break}	57.27	14.16
540.0	56.94	6.29	71.91	57.42	14.49
550.8	57.11	6.06	72.14	57.57	14.57
561.6	57.29	5.92	72.28	57.71	14.57

Grade Change cd.
11/28/16
72.39
3.44
75.83
1.18
4.65
4.66
4.88
5.735
6.65
72.39
5.25
77.64
12.7
64.99
64.20
57.33
6.85
5

57.35 grade

Rate = ~~1.38~~ + 0%
1.355

431 431 451
586 5829 142
155 1424 588

9

78.20

592A		590	72.30	59.86	14.44	} 57.46
586 = 86 No of 10's	B	E 598	72.22	58.06	14.16	
		W 591	72.39		14.33	
106		598	72.22	58.33	13.89	57.99
120		605	72.15	58.60	13.55	58.31
146		602	72.18	58.87	13.31	58.63
166		602	72.18	59.14	13.04	58.95
186		613	72.07	59.41	12.66	59.26
206		607	72.13	59.68	12.45	59.58
226		586	72.34	59.95	12.39	59.90
246	1649	79.00 569	72.51	60.22	12.29	60.22
266		643	72.57	60.50	12.07	
286	(10)	635	72.65	60.77	11.88	
300	Sh. A	653	72.47	60.96	11.51	
320		624	72.76	61.23	11.53	
340		629	72.71	61.40	11.31	
360		633	72.67	61.67	11.00	
380	NL A	657	72.43	61.94	10.49	
400		632	72.68	62.21	10.47	
420		612	72.88	62.48	10.40	
440		Fiume		62.75		
460				63.02		
480		51.8	73.82	63.30	10.52	

6.10
7.10
2.00

A.M. 73.14

7900
589
73.11 chub-

620
56
534

620
350
240

70

7900 Prod also grad out.

500		5.02	73.98	63.57	10.41
520		4.57	74.43	63.84	10.59
540		4.12	74.88	64.11	10.77
560		3.72	75.28	64.38	10.90
580		3.39	75.61	64.65	10.96
600		2.85	76.15	64.92	11.23
620	B.C.	W 2.08	76.92	65.30	11.62
		E 2.50	76.50		11.20
630.5		W 5.60	77.40	65.44	12.96
641		W 5.36	77.64	65.58	12.06
651.5		W 5.21	77.79	65.73	12.06
662		W 5.23	77.77	65.87	11.90
672.5				66.01	
683		W 5.08	77.92	66.15	11.77
693.5		E 5.18	77.82	66.29	11.53
707.5	E.C.	E 5.31	77.69	66.48	11.21
759.5	BC	E 4.32	78.68	67.18	11.50
770		4.16	78.54	67.32	11.22
780.5		4.67	79.33	67.46	10.87
791		4.87	78.13	67.60	10.53
801.5		5.20	77.80	67.75	10.05
812				67.89	

8.2
74.1
79.75
5.65

(33' Pacific D.
+ Cr.

78.66
3.17
81.83
7.2

72.90
6.06
80.00

96.15
6.49
82.73
4.07
98.66 TP
1375
82.71 HE

74.1
7.7
81.8
4.2
77.7 cl.

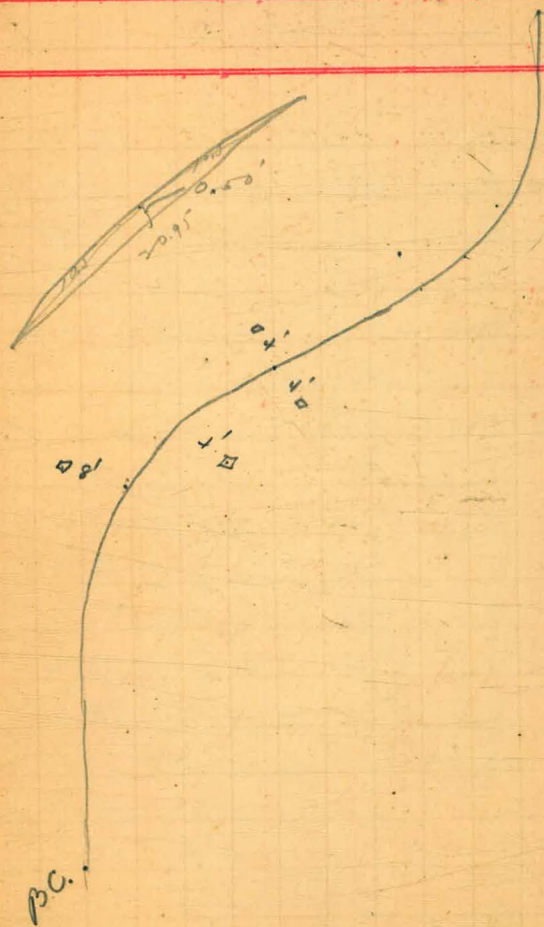
at Cr. in new
plan

78.66
7.9
72.8
73.9
74.7
74.7
5.8
7
3.5
10.5
81.83
4.20
77.63
18M
Dua

	Prod	Elev	Grade	cut
Face of Inlet.				
819 E.C.	E 6.06	76.94	68.00	8.94

$\frac{76}{3}$ $\frac{46}{23}$ <u>69</u>	$\frac{13}{6}$ $\frac{19}{3}$	$\frac{21}{101}$ $\frac{315}{18}$ $\frac{27}{3}$	$\frac{23}{2}$ $\frac{15.5}{3}$ $\frac{125}{5}$	$\frac{175}{57}$ $\frac{261}{3}$ $\frac{56}{28}$ <u>84</u>	$\frac{19}{95}$ $\frac{385}{1}$
$\frac{64}{2}$ $\frac{32}{15}$	$\frac{4}{2}$ $\frac{2}{1}$ $\frac{2}{8}$	$\frac{88}{2}$ $\frac{58}{29}$ $\frac{87}{11}$		$\frac{69.33}{1341}$	
		$\frac{82.94}{1.68}$ $\frac{83.62 Hz}{56}$ $\frac{78.02}{472}$ $\frac{82.74 Hz}{}$	$\frac{79.75}{5.57}$ $\frac{3.00}{}$	$\frac{175}{71.75}$ $\frac{1100}{1100}$	$\frac{175}{1100}$
			$\frac{8.7}{74.0}$	$\frac{7.9}{3}$ $\frac{29}{740}$ <u>3</u>	

76



7/15/06 Lowering of Water
Main Arctic - B.

78

	11.00	16.77		5.77	
N. Top Pipe (-1.2)	7.76		9.0		7.8
N. Side Conduit	7.90		9.4		8.2
S. " "	7.90		9.4		
S. Top Pipe (-1.2)	7.90		9.4		
Topline					
N. from Conduit					
	4.7	12.1			2.2
12	4.7	12.1			2.7
24	4.66	12.1			3.2
36	4.66	12.1			3.7
48	4.6	12.2			4.2
60	4.6	12.2			4.7
72	4.5	12.3			5.2
84	4.5	12.3			5.7
96	4.4	12.4			6.2
108	4.3	12.5			6.7
120	4.2	12.6			7.2
132	4.2	12.6			7.7

S from Conduit					
	4.7	12.1	2.2		9.9
12	4.8	12.0	2.7		9.3
24	4.8	12.0	3.2		8.8
36	4.9	11.9	3.7		8.2
48	4.9	11.9	4.2		7.7
60	4.9	11.9	4.7		7.2
72	5.0	11.8	5.2		6.6
84	5.0	11.8	5.7		6.1
96	5.0	11.8	6.2		5.6
108	5.1	11.7	6.7		5.0
120	5.1	11.7	7.2		4.5
132	5.0	11.8	7.7		4.1
145	5.0	11.8	8.2		3.6
				9.9	
				9.4	
				8.9	
				8.4	
				8.0	
				7.5	
				7.1	
				6.6	
				6.2	
				5.8	
				5.4	
				4.9	

Survey for Drain from
Turn table for L.A. & S.D. B. Ry
to Bst Conduit

281	14.69	12.83	- 6.0
4.25	19.76	4.13	10.51 = 4.51
Base Rail		4.32	
Top of Stake (C. T.T.) = 0+00		4.32	
ground el. "		5.97	
0+50		5.6	
1		5.5	
+50		5.7	
2		5.5	
+20		5.8	
+40 at line		4.4	
+50		4.5	
3		4.7	
grade at 375.7 W of E. India.			3.34
(42.5 W of W Gage L. of W Tract)			
el of bottom -			4.16
(310 Cr T.T. to 4' line)			

4.5
1.5
6.0
10.5
4.5

4.51
4.26
0.25
fall from -
Cr of TT Pit to
Bottom of Invert.

6.92
1.16
8.08
4.04
3.83
0.25

11.95
3.75,7
17.785
38.15
7.57
37.57
4.488.615
7.83
5.84
9.2
4.26
6.01
1.75

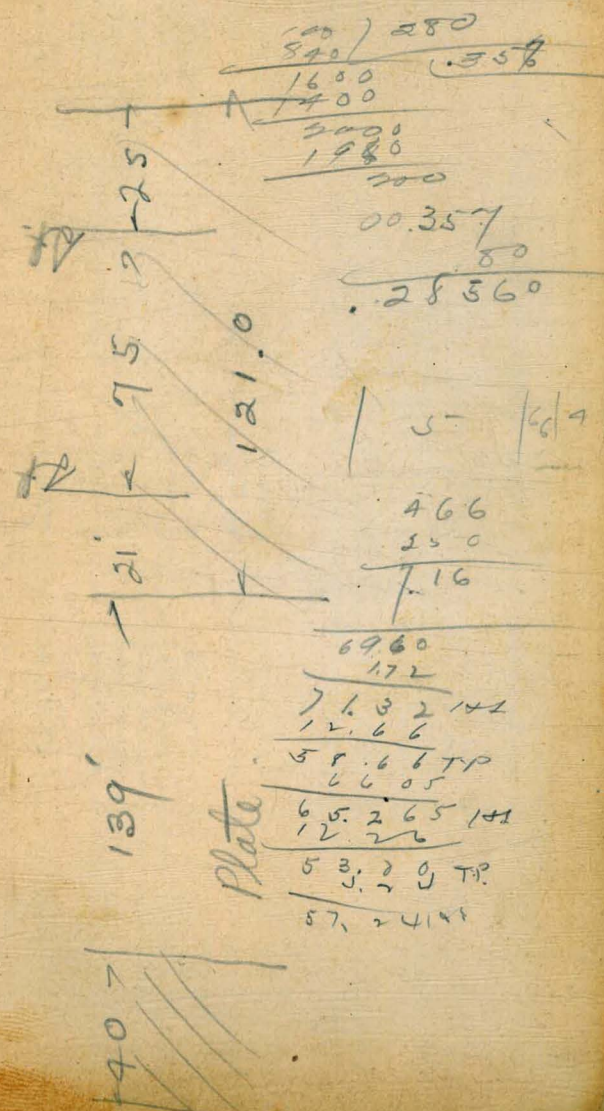
6.01
6.2
4.81
6.01
5.06
9.5

3.46
1.16
4.62
4.2
4.82

10.05
 215 ✓
 10.265 ✓
 249 ✓
 10.514 ✓
 26 ✓
 10.774 ✓
 248 ✓
 11.022 ✓
 249 ✓
 11.271 ✓
 248 ✓
 11.519 ✓
 26 ✓
 11.779 ✓
 249 ✓
 12.028 ✓
 26 ✓
 12.288 ✓
 247 ✓
 12.525 ✓
 26 ✓
 12.775 ✓
 248 ✓
 13.033 ✓
 249 ✓
 13.282 ✓
 248 ✓
 13.530 ✓
 237 ✓
 13.767 ✓
 237 ✓
 14.004 ✓
 169 ✓
 14.173 ✓
 237 ✓
 14.410 ✓
 226 ✓
 14.636 ✓
 237 ✓
 14.878 ✓
 237 ✓
 15.116 ✓
 237 ✓
 15.347 ✓
 236 ✓
 15.578 ✓
 236 ✓

22.52 w/ stars
 0.65 N.O.

6.91
 25
 18.09 11.195
 0.5975



216
 329
 18.4
 Degrees.
 89
 88
 87
 86
 85
 84
 83
 82
 81
 80
 79
 78
 77
 76
 75
 74
 73
 72
 71
 70
 69
 68
 67
 66
 65
 64
 63
 62
 61
 60
 59
 58
 57
 56
 55
 54
 53
 52
 51
 50
 49
 48
 47
 46
 45
 Degrees.
 trials,

1 Land 1859
 8.0529 17.7.3
 3.37
 9-5 11.42
 17.5 1.12
 17.5 12.44
 62 0.14
 1750 11.28
 250 9.0
 4.250 9.0
 10.32
 2.54 266 8.03
 9.88
 1863
 1765
 20.28
 16
 Return to City Engineers Office
 City Hall, San Diego, Cal.
 7.418
 2749-25
 5631
 950
 891
 962
 56
 75.6
 12
 354
 285
 17.5
 34°08'

Return to City Engineers Office
 City Hall, San Diego, Cal.
 TRAVERSE TABLE FOR TRANSIT BOOK
 From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0	99.98	1.75	100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.94	3.49	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.86	5.23	99.92	3.83	99.91	4.36	99.88	4.80	87
3	99.76	6.98	99.84	5.07	99.81	6.10	99.79	6.54	86
4	99.62	8.72	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.45	10.45	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.25	12.19	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.03	13.92	99.30	12.62	99.14	13.05	99.09	13.49	82
8	98.77	15.64	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.48	17.36	98.70	16.07	98.63	16.50	98.56	16.93	80
10			98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	89.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.00	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							

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